AMCP-706-177

AMC PAMPHLET

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ENGINEERING DESIGN HANDBOOK



EXPLOSIVES SERIES

PROPERTIES OF EXPLOSIVES

OF MILITARY INTEREST

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HEADQUARTERS, U.S. ARMY MATERIEL COMMAND

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HEADQUARTERS UNITED STATES ARMY MATERIEL COMMAND WASHINGTON. D. C. 20315

29 January 1971

AMC PAMPHLET No. 706-177*

ENGINEERING DESIGN HANDBOOK PROPERTIES OF EXPLOSIVES OF MILITARY INTEREST

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PREFACE

The Engineering Design Handbook Series of the Army Materiel Command is a coordinated series of handbooks containing basic information and fundamental data useful in the design and development of Army materiel and systems. The handbooks are authoritative reference books of practical information and quantitative facts helpful in the design and development of Army materiel so that it will meet the tactical and technical needs of the Armed Forces.

AMCP 706-177, Properties of Explosives of Military Interest, is one of a series on Explosives. One hundred and ten explosive compounds or mixtures are listed herein, alphabetically, with their properties, including composition variations. These explosives were selected because of their current or probable application to military use.

The tabulated data reflect the results of tests, and were first compiled for publication at Picatinny Arsenal, Dover, New Jersey, by W. R. Tomlinson, Jr. These data were later revised by Oliver E. Sheffield, also of Picatinny Arsenal, for the Engineering Handbook Office of Duke University, prime contractor to the Army Materiel Command.

The Handbooks are readily available to all elements of AMC, including personnel and contractors having a need and/or requirement. The Amy Materiel Command policy is to release these Engineering Design Handbooks to other D0D activities and their contractors and to other Government agencies in accordance with current Amy Regulation 70-31, dated 9 September 1966. Procedures for acquiring these Handbooks follow:

a. Activities within AMC and other DOD agencies order direct on an official form from:

Commanding Officer Letterkenny Amy Depot, ATTN: AMXLE-ATD Chambersburg, Pennsylvania 17201

b. Contractors who have Department of Defense contracts should submit their requests through their contracting officer with proper justification to the address listed in par. a.

c. Government agencies other than DOD having need for the Handbooks may submit their requests directly to the address listed in par. a or to:

Commanding General U. S. Amy Materiel Command ATTN: AMCAM-ABS Washington, D. C. 20315

d. Industries not having Government contracts (this includes colleges and Universities) must forward their requests to:

Commanding General U. S. Amy Materiel Command ATTN: AMCRD-TV Washington, D. C. 20315

e. All foreign requests must be submitted through the Washington, D. C. Embassy to:

Assistant Chief of Staff for Intelligence Foreign Liaison Office Department of the Amy Washington, D. C. 20310

All requests, other than those originating within DOD, must be accompanied by a valid justification.

Comments and suggestions on this handbook are welcomed and should be addressed to Army Research Office-Durham, Box CM, Duke Station, Durham, North Carolina 27706.

ABBREVIATIONS AND SYMBOLS

| ~ | approximately. This symbol is used before numbers. |
|-----------------------------|---|
| AC | Advisory Council on Scientific Research and Develop- ment, Great Britain. |
| AC S | American Chemical Society. |
| AISI | American Iron and Steel Institute. |
| Ann | Liebig's Annalen der Chemie. |
| Ann chim phys | Annales de chimie et de physique. |
| AP | armor-piercing. |
| APG | Aberdeen Proving Ground. |
| atm | atmosphere; atmospheric pressure. |
| Beil | Beilstein Organische Chemie, 4th Edition. |
| Ber | Berichte der Deutschen Chemischen Gesellschaft. |
| BIOS GP2-HEC | British Intelligence Overseas Service or Objective |
| | Subcommittee, Group 2, Halstead Exploiting Center. |
| BM | Bureau of Mines, United States Department of Interior. |
| Bull Soc chim | Bulletin de la societe'chimique de France. |
| CA | Chemical Abstracts. |
| calc | calculated. |
| Chem Met Eng | Chemical and Metallurgical Engineering. |
| Chim et Ind | Chimie et Industrie. Comptes rendus hebdomadaires des seances de |
| Comp rend | l'Academie des Sciences (Paris). |
| C D | centipoise. |
| ср CR | Comptes rendus hebdomadaires des seances de |
| CIX | l'Academie des Sciences (Paris). |
| dec | decomposes. |
| AH | difference in heat (i.e., heat evolved) by decomposition. |
| DRP | Deutsches Reichspatent. |
| E | modulus of elasticity or "Young's modulus"; longitudinal |
| | stress/change in length; (force/area)/(elongation/ |
| | length); expressed in lb/inch ² . |
| E | same as E, but expressed in dynes/cm ² . |
| Gazz chim ítal | Gazzetta Chimica Italiana. |
| GP | general purpose. |
| HE | high explosive. |
| HEAT | high explosive antitank. |
| Ind Eng Chem | Industrial & Engineering Chemistry. |
| J Am Chem Soc J Chem Ind | Journal of the American Chemical Society The Journal of the Society of Chemical Industry (London). |
| J Chem Ind J Chem Soc | Journal of the Chemical Society (London). |
| J Frank Inst | Journal of the Franklin Institute. |
| J Ind Explo- | oodinal of the flanklin institute. |
| sives Soc | Journal of the Industrial Explosives Society (Japan). |
| J prakt Chem | Journal für praktische Chemie. |
| LA | lead azide |
| Land-Bornst | Landolt-Bornstein Physikalish-Chemische Tabellen, |
| | 5th Edition (Berlin). |
| М | molar. |
| | Monatshefte fur Chemie (Wein). |
| Mem poudr | Mémorial des poudres et salpêtres (Paris). |
| mg | milligram. |
| | |

ABBREVIATIONS AND SYMBOLS (cont'd)

| min ml m/s MW NAVORD NC | minimum. milliliter. meters per second. molecular weight. Bureau of Ordnance (U. S. Navy) nitrocellulose. |
|--|--|
| $n \frac{D}{20}$ | index of refraction, with D band of sodium as light source, at twenty degrees centigrade. |
| NDRC | National Defense Research Committee. |
| NFOC | National Fireworks Ordnance Corporation. |
| NG NOL | nitroglycerin. U. S. Naval Ordnance Laboratory, White Oak, Silver |
| NOL | Spring, Maryland. |
| NOTS | U. S. Naval Ordnance Test Station, China Lake, Calif. |
| NRC | National Research Council. |
| OB | oxygen balance. |
| OCM | Ordnance Committee Minutes. |
| OSRD | Office of Scientific Research and Development |
| PA | Picatinny Arsenal. |
| PATR | Picatinny Arsenal Technical Report. |
| Phil Trans | Philosophical Transactions of the Royal Society of London. |
| Pogg Ann | Poggendorf's Annalen der Physik. |
| Proc Roy Soc | Proceedings of the Royal Society of London. |
| Rec trav chim | Recueil des travaux chimiques des Pays-Bas. |
| RH | relative humidity. |
| RI | Report of Investigation. |
| SAE | Society of Automotive Engineers. |
| SAP | semi-armor-piercing. |
| sol | solution. |
| Spec | Specifications. |
| std dev | standard deviation. |
| ТМ ТМ/ТО | Technical Manual, Department of the Army. |
| 1 11/10 | joint publication, as a TM and as a Department of the Air Force Technical Order. |
| Trans Farad Soc | Transactions of the Faraday Society |
| vac stab | vacuum stability. |
| Z angew Chem | Zeitschrift fur angewandte Chemie. |
| Z anorg Chem | Zeitschrift für anorganische und allgemeine Chemie. |
| Z ges Schiess- | Zeitschrift fur das gesamte Schiess und Sprengstoff- |
| Sprengstoffw | wessen (Munchen). |
| Z/sec | atoms of oxygen per second. |
| | |

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PROPERTIES OF EXPLOSIVES OF MILITARY INTEREST

INTRODUCTION

1. PREDOMINANTLY A REPORT OF STANDARD TESTS. No effort was made to cover all the existing literature, either open or classified security information, on any explosive. Rather, the main resource has been reports from facilities using standard or well-known test procedures.

2. ORIGIN. Compilation of data resulting in this handbook was undertaken by Picatinny Arsenal personnel who desired to provide a manual tabulating the characteristics of explosives, based on tests, with regard to current, and possible future, interest. The first resulting Picatinny Arsenal publication was dated 20 June 1949. Revision 1, PA Technical Report No. 1740, dated April 1958, with revisions, provides the data used herein.

<u>3. SCOPE</u> Tabulated data of tests on one hundred and ten explosive compounds or mixtures include sensitivity to friction, impact, heat; performance characteristics or effectiveness in weapons; physical and chemical properties; and method of preparation, synthesis or manufacture, with comments on historical origin, and supplementary references.

4. REFERENCE NOTATIONS AND SOURCES. The references, as to sources of data or for more details in methods of testing, have been listed, when available, at the end of each section devoted to a given explosive compound, explosive mixture, or explosive ingredient. Where no reference is given, it can be assumed that these data represent typical values obtained by standard procedures. When evailable any reference should be consulted for more details in interpreting test data.

Also there are listed Picatinny Arsenal Technical Reports which contain additional information on the particular explosive. These report numbers are given in ascending order, in columns corresponding to their terminal digits, and in accordance with the "Uniterm Index" prepared for Picatinny Arsenal by Documentation Incorporated under Contract RAI-36-034-501-ORD-(P)-42 (1955).

5. EXPLANATION OF TERMS AND METHODS OF TESTING. Data are tabulated herein on three form-type pages, in the following sequence of headings. Many of these terms are self-explanatory.

a. First tabular page.

(1) Name of the explosive in each instance.

- (2) "Composition."
- (3) "Impact Sensitivity, 2 Kg Wt."
 - (a) Impact sensitivity test for solids. (a)*

A sample (approximately 0.02 gram) of explosive is subjected to the action of a falling weight, usually 2 kilograms. A 20-milligram sample of explosive is always used in the Bureau of Mines (BM) apparatus when testing solid explosives. The weight of sample used in the Pica-tinny Arsenal (PA) apparatus is indicated in each case. The <u>impact test value</u> is the minimum

^{*}Reference publications (a through q), applying to this introduction, are listed at the end of the introduction.

height at which at least one of 10 trials results in <u>explosion</u>. For the BM apparatus, the unit of height is the centimeter; for the PA apparatus, it is the inch. In the former, the explosive is held between two flat, parallel hardened (C 63 ± 2) steel surfaces; in the latter case, it is placed in the depression of a small steel die-cup, capped by a thin brass cover, in the center of which is placed a slotted-vented-cylindrical steel plug, slotted side down. In the BM apparatus, the impact impulse is transmitted to the sample by the upper flat surface, in the PA, by the vented plug. The main differences between the two tests are that the PA test (1) involves greater confinement, (2) distributes the translational impulse over a smaller area (due to the inclined sides of the die-cup cavity), and (3) involves a frictional component (against the inclined sides).

The test value obtained with the PA apparatus depends, to a marked degree, on the sample density. This value indicates the hazard to be expected on subjecting the particular sample to an impact blow, but is of value in assessing a material's inherent sensitivity only if the apparent density (charge weight) is recorded along with the impact test value. The values tabulated herein were obtained on material screened between 50 and 100 mesh, U. S. Standard Screens where single component explosives are involved, and through 50 mesh for the mixtures.

(b) Impact sensitivity test for liquids. (b)

The PA Impact Test for liquids is run in the same way as for solids. The die-cup is filled and the top of the liquid meniscus adjusted to coincide with the plane of the top rim of the die-cup. To date, this visual observation has been found adequate to assure that the liquid does not wet the die-cup rim after the brass cap has been set in place. Thus far the reproducibility of data obtained in this way indicate that variations in sample size obtained are not significant.

In the case of the EM apparatus, the procedure that was described for solids is used with the following variations:

1. The weight of explosive tested is 0.007-gm.

<u>2.</u> A disc of desiccated filter paper (Whatman No. 1)9.5-millimeter diameter, is laid on each drop, on the anvil, and then the plunger is lowered on the sample absorbed in the filter paper.

(4) "Friction Pendulum Test." (c)

A 7.0-gm sample of explosive, 50-100 mesh, is exposed to the action of a steel, or fiber, shoe swinging as a pendulum at the end of a long steel rod. The behavior of the sample is described qualitatively to indicate its reaction to this experience, i.e., the most energetic reaction is explosion, and in decreasing order of severity of reaction: snaps, cracks, and unaffected.

(5) "Rifle Bullet Impact Test." (d)

Approximately 0.5-pound of explosive is loaded in the same manner as it is loaded for actual use: that is, cast, pressed, or liquid in a 3-inch pipe nipple (2-inch inside diameter, 1/16-inch wall) closed on each end by a cap. The loaded item, in the standard test, contains a small air space which can, if desired, be filled by inserting a wax plug. The loaded item is subjected to the impact of a caliber .30 bullet fired perpendicularly to the long axis of the pipe nipple, from a distance of 90 feet.

(6) "Explosion Temperature." (a)

A 0.02-gm sample (0.01-gm in the case of initiators) of explosive, loose loaded in a No. 8 blasting cap, is immersed for a short period in a <u>Wood's metal</u> bath. The temperature determined is that which produces explosion, ignition or decomposition of the sample in 5 seconds, and the behavior of the sample is indicated by "Explodes" or "Ignites" or "Decomposes" placed beside the value. Where values were available for times other than 5 seconds, these have been included. For 0.1-second values, no cap was used, but the explosive was placed directly on <u>Wood's metal</u> bath, immediately after cleaning. The value 0.1 second is estimated, not determined, and represents an interval regarded as instantaneous to the observer's eye. Dashes indicate no action.

(7) "75°C International Heat Test." (a)

A 10-gm sample is heated for 48 hours at 75° C. The sample after this exposure is observed for signs of decomposition or volatility.

(8) "100°C Heat Test." (a)

A 0.6-gm sample is heated for two 48-hour periods at 100° C. It is also noted whether exposure at 100° C for 100 hours results in explosion.

(9) "Flammability Index." (h)

The measure of the likelihood that a bare charge will catch fire when exposed to flames is the index of flammability. The test is made by bringing an oxyhydrogen flame to bear on the explosive. The maximum time of exposure which gives no ignition in 10 trials and the minimum exposure which gives ignition in each of 10 trials are determined. The index of flammability is 100 divided by the mean of the two times in seconds. The most flammable substances have high indices, e.g., 250.

(10) "Hygroscopicity."

A 5- to 10-gm sample is exposed for hygroscopicity under the stated conditions, until equilibrium is attained, or in cases where either the rate is extremely low, or very large amounts of water are picked up, for the stated time. The sample, if solid, is prepared by sieving through a 50 and on a 100 mesh screen.

(11) "Volatility."

A 10-gm sample is exposed for volatility under the stated conditions. The sample if solid is prepared by sieving through a 50 and on a 100 mesh sieve.

(12) "Molecular Weight."

The molecular weight (MW) of a mixture can be calculated from the equation

MW of mixture =
$$\frac{100}{\frac{a}{mw_1} + \frac{b}{mw_2} + \frac{c}{mw_3} + \frac{n}{mw_n}}$$

where a, b, c and n are the weight percents of the components, and mw_1 , mw_2 , mw_3 and mw_n their corresponding molecular weights.

(13) "Oxygen Balance."

The oxygen balance (OB) is calculated from the empirical formula of a compound in percentage of oxygen required for complete conversion of carbon to carbon dioxide (or carbon monoxide) and hydrogen to water. When metal is present the reactions are assumed to occur in the following order:

Metal + 0 \longrightarrow Metal Oxide C + H₂0 \longrightarrow CO + H₂ CO2 + H₂ \longrightarrow CO + H20 2CO + O₂ \longrightarrow 2CO₂

Procedure for calculating oxygenbalance is to determine the number of gramatoms of oxygen which are excess or deficient for 100 grams of a compound. This number multiplied by the atomic weight of oxygen gives

the oxygen balance: 1600 (2X + $\frac{Y}{Z}$ - Z)

 \div molecular weight of compound = oxygen balance to C02 and H₂O, where X = atoms of carbon, Y = atoms of hydrogen, Z = atoms of oxygen. The oxygen balance of a mixture is equal to the sum of the percent composition times the oxygen balance for each component.

The carbon/hydrogen (C/H) ratio is calculated as follows:

 $\frac{\text{Number of } C \text{ atoms } (\%C + \%H)}{\text{Number of } H \text{ atoms } (100)} = C/H \text{ ratio}$

- (14) "Density."
- (15) "Melting Point."
- (16) "Freezing Point."
- (17) "Boiling Point."
- (18) "Refractive Index."
- (19) "Vacuum. Stability Test." (a)

A 5.0-gm sample (1.0 gm for initiators), after having been carefully dried, is heated for 40 hours, in vacuo at the desired temperature.

- (20) "200 Gram Bomb Sand Test."
 - (a) Sand test for solids. (a)

A 0.4-gm sample of explosive, pressed at 3000 pounds per square inch into a No. 6 cap, is initiated by lead azide, or mercury fulminate (or, if necessary, by lead azide and tetryl), in a sand test bomb containing 200 gm of "on 30 mesh" Ottawa sand. The amount of azide, or of tetryl, that must be used, to insure that the sample crushes the maximum net weight of sand, is designated as its sensitivity to initiation and the net weight of sand crushed, finer than

•

30 mesh, is termed the <u>sand test value</u>. The net weight of sand crushed is obtained by subtracting from the total the amount crushed by the initiator when shot alone.

(b) Sand test for liquids. (b)

The sand test for liquids is made in accordance with the procedure given for solids except that the following procedure for loading the test samples is substituted:

Cut the closed end from a No. 6 blasting cap and load one end of the resulting cylinder with 0.20 gm of lead azide and 0.25 gm of tetryl, using a pressure of 3000 psi for consoli-dating each charge. With a pin, prick the powder train in one end of a piece of miner's black powder fuse 8 or 9 inches long. Crimp to the pricked end a loaded cylinder, taking care that the end of the fuse is held firmly against the charge in the cap. Crimp near the mouth of the cap so as to avoid squeezing the charge. Transfer a weighed portion of 0.400 gm of the test explosive to an aluminum cap, taking precautions when the explosive is liquid to insert the sample in such a manner that as little as possible adheres to the side walls of the cap, and when a solid material is being tested use material fine enough to pass through a No. 100 U. S. Standard Sieve. The caps used shall be of the following dimensions: length 2.00 inches, internal diameter 0.248-inch, wall thickness 0.025-inch. Press solid explosives, after insertion into the aluminum cap, by means of hand pressure to an apparent density of approximately 1.2 gn per cubic centimeter. This was done by exerting hand pressure on a wooden plunger until the plunger had entered the cap to a depth of 3.93 centimeters. Following are the dimensions of the interior of the cap: height 5.00 cm, area of cross section 0.312 square centimeters. Insert the cylinder containing the fuse and explosive charge of tetryl and lead azide into the aluminum cap containing the test explosive for the determination of sand crushed.

(21) "Sensitivity to Initiation."

This is <u>sensitivity to initiation</u> as described under the preceding heading. The minimum detonating charge, in grams, required to detonate the explosive sample, is given.

(22) "Ballistic Mortar, % TNT." (e)

The amount of sample under test which is necessary to raise the heavy ballistic mortar to the same height to which it is raised by 10 gm of trinitrotoluene (TNT) is determined. The sample is then rated, on a proportionate basis, as having a certain TNT value, i.e., as being a certain percent as effective as TNT in this respect. The formula is

TNT value =
$$\frac{10}{\text{sample weight}}$$
 x 100.

The ballistic mortar consists of a long compound supporting rod, at the end of which is supported a heavy short-nosed mortar. The mortar contains a chamber about 6 inches in diameter and 1 foot long. A projectile occupies about 7 inches of the chamber and the sample to be tested occupies a small portion of the remainder of the chamber. When the sample is detonated, the projectile is driven into a sand bank, and the mortar swings through an angle which is marked on paper by a pencil attached to the mortar. The angle thus indicates the height to which the pendulum is raised by the explosion, and this latter represents the energy measured by this test procedure.

(23) "Trauzl Test, % INT." (d)

A sample of the explosive to be tested (of the order of 10 gm) is exploded in a cavity, or borehole, 25-mm in diameter and 125-mm deep, in a lead block 200-mm in diameter and 200-mm in height. The borehole is made centrally in the upper face of each block, which is cast in a mold from desilverized lead of the best quality. Although these tests have been made under a variety of conditions, where possible the data have been taken from or related to those of Reference f (Naoum). Here a No. 8 blasting cap was used for initiation of the sample contained in glass. The weight of sample used was adjusted to give, with the initiator, a total expansion of 250 to 300 cc, since within this range expansion and sample weight were linearly related under the conditions of Naoum's test. Thus expansions for equivalent weights were readily calculated, and the test value expressed in percent of the expansion of an equivalent weight of TNT.

(24) "Plate Dent Test." (d)

Two methods were used for plate dent tests.

(a) Method A - The charge is contained in a copper tube, having an internal diameter of 3/4-inch and 1/16-inch wall. This loaded tube is placed vertically on a square piece of cold-rolled steel plate, 5/8-inch thick; 4-inch and 3-1/4-inch square plate gave the same results. The steel plate is in a horizontal position and rests in turn on a short length of heavy steel tubing 1-1/2 inches ID and 3 inches OD. The charge rests on the center of the plate, and the centers of the charge, plate, and supporting tube are in the same line. A 20-gm charge of the explosive under test is boostered by a 5-gm pellet of tetryl, in turn initiated by a No. 8 detonator.

(b) Method B - A 1-5/8-inch diameter, 5-inch long uncased charge is fired on a 1-3/4-inch thick, 5-square inch cold-rolled steel plate, with one or more similar plates as backing. The charge is initiated with a No. 8 detonator and two 1-5/8-inch diameter, 30-gm tetryl boosters.

Plate dent test value, or relative brisance = $\frac{\text{Sample Dent Depth}}{\text{Dent Depth for TNT at 1.61 gm/cc}} \times 100.$

(25) "Detonation Rate." (g)

The detonation rates reported in the tables contained herein were determined principally by using the rotating drum camera, under the conditions stated, e.g., usually charges 1 inch in diameter, 20 inches long, wrapped in cellulose acetate sheet, and initiated by a system designed to produce high order stable detonation at the maximum rate under the particular conditions. A typical initiating system for this consisted of four tetryl pellets 0.995 inch in diameter, 0.75 inch long, pressed to 1.50 gm/cc, with a Corps of Engineers special blasting cap placed in a central hole in the end pellet.

b. Second tabular page.

(1) "Booster Sensitivity Test." (p)

The booster sensitivity test procedure is a scaled up modification of the Bruceton method (unconfined charge). The source of the shock consists of two tetryl pellets, each 1.57 inches diameter by 1.60 inches high, of approximately 100 gm total weight. The initial shock is degraded through wax spacers of cast Acrawax B, 1-5/8 inches diameter. The test charges are 1-5/8 inches diameter by 5 inches long. The value given is the thickness of wax in inches at the 50% detonation point. The weight of tetryl pellet noted is the minimum which will produce detonation with the spacer indicated.

(2) "Heat of" (calorimetric tests). (i)

Heats of combustion and explosion are generally determined on samples weighing of the order of 1 to 2 gm, in standard calorimeter bombs such as the Parr or Emerson, approximately 400 cc (for low loading density), or the Boas, approximately 45 cc (for high loading density). For

heats of combustion the sample is burned under about 40 atmospheres or oxygen; for heats of explosion, nitrogen, or one atmosphere of air is used.

- (3) "Specific Heat."
- (4) "Burning Rate."
- (5) "Thermal Conductivity."
- (6) "Coefficient of Expansion."
- (7) "Hardness, Mohs' Scale."
- (8) "Young's Modulus."
- (9) "Compressive Strength."
- (10) "Vapor Pressure."
- (11) "Decomposition Equation."
- (12) "Armor Plate Impact Test." (j)
 - (a) 60-mm Mortar Projectile.

A modified 60-mm, M49A2, mortar projectile is loaded with the explosive to be tested, drilled to the proper depth (about 1/2 inch), and a flat-based steel plug screwed into the projectile to give a smooth close-fit between the plug base and the charge. The part of the plug outside the projectile is rounded off in the form of a spherical section. The loaded projectile with fins attached is fired from a five foot length of 2-3/8 inches ID x 3-3/8 inches 0D Shelby steel tubing. The igniter and propelling charge, consisting of an igniter for a 2.36-inch rocket (bazooka), 5 gm of 4F black power, and a quantity of shotgun propellant sufficient to give the desired velocity (read from a calibration chart) are conveniently loaded into the "gun" through a simple breech plug. The velocities are measured electronically, and the reaction, inert or affected, is determined by observation (e.g., whether or not flash occurs on impact). Within the range of flight stability of the projectile, 200-1100 ft/sec, the 50% point is located.

- (b) 500-lb General Purpose Bombs.
- (13) "Bomb Drop Test."

Bomb drops are made using bombs assembled in the conventional manner, as for service usage, but containing either inert or simulated fuzes. The target is usually reinforced concrete.

- c. Third tabular page.
 - (1) "Fragmentation Test." (1)

The weight of each empty projectile and weight of water displaced by the explosive charge is determined, and from this the specific gravity of the charge is calculated. All 3-inch and 90-mm projectiles are initiated by M20 Booster pellets, and those used with 3-inch HE, M42Al, Lot KC-5 and 90-mm HE, M71, Lot WC-91 projectiles are controlled in weight and height as follows: 22.50 ± 0.10 gm, and 0.480 to 0.485 inch.

The projectile assembled with fuze, actuated by a Blasting Cap, Special, Type II (Spec 49-20) placed directly on a lead of comparable diameter, and booster, are placed in boxes constructed of half-inch pine. The 90-mm projectiles are fragmented in boxes $21 \times 10-1/2 \times 10-1/2$ inches and the 3-inch projectiles in boxes $15 \times 9 \times 9$ inches outside dimensions. The box with projectile is placed on about 4 feet of sand in a steel fragmentation tub, the detonator wires are connected, and the box covered with approximately 4 feet more of sand. The projectile is fired and the sand run onto a gyrating 4-mesh screen on which the fragments are recovered.

(2) "Fragment Velocity."

Charges 10-1/8 inches long and 2 inches in diameter, containing a booster cavity, filled by a 72-gm tetryl pellet (1-3/8) inches diameter, 2 inches long, average density 1.594) are fired in a model projectile of Shelby seamless tubing, 2 inches ID, 3 inches OD, SAE 1020 steel, with a welded-on cold rolled steel base. The projectile is so fired in a chamber, connected to a corridor containing velocity stations, that a desired wedge of projectile casing fragments can be observed. The fragment velocities are determined by shadow photographs, using flash bulbs, and rotating drum cameras, each behind three slits. The drum cameras have a writing speed of 30 meters per second.

(3) "Blast (Relative to TNT)."

The blast pressures and impulses given were determined almost exclusively with tourmaline gages, and the usual necessary specialized electrical circuits, shielded co-axial cables, oscillographs, etc. In general, the data represent results of tests with large cased charges.

(4) "Shaped Charge Effectiveness, TNT = 100." (k, m)

Unconfined charges 2 inches in diameter and 6 inches *long*, boostered by a 10-gm pressed tetryl pellet, set in a 20-mm pellet (truncated cone) of cast 60/40 cyclotol, are shot against 3-inch homogeneous armor plate at a 1-3/16 inches standoff. The cones used are commercial Pyrex glass funnels, sealed off at the start of the stem, 2 inches in diameter, 0.110 to 0.125 inch wall thickness.

Unconfined charges 1.63 inches in diameter and 6 inches long are tested at a standoff of 1.63 inches against stacks of $4 \times 4 \times 1$ inch mild steel plates. M9Al steel cones are used. Results are averages of 4 trials.

- (5) "Color."
- (6) "Principal Uses."
- (7) "Method of Loading."
- (8) "Loading Density."
- (9) "Storage."

Ammunition and bulk explosives in storage represent varying degrees of hazard and compatibility. This has led to their being divided into a number of hazard classes and compatibility groups as indicated in subparagraphs (b) and (c) below.

- (a) Method: Wet or dry.
- (b) Hazard Class (Quantity-Distance).

Ammunition and bulk explosives are divided into quantity-distance classes, Class 1 through 12, according to the damage expected if they explode or ignite (Reference: Army Materiel Command Regulation, AMCR 385-100, <u>AMC Safety Manual</u>, chapter 17). All standard explosives in bulk are included in four of these classes: Class 2, 2A, 9, and 12 (TM 9-1910/TO 11A-1-34).

(c) Compatibility Group.

Explosives and ammunition are grouped for compatibility with respect to the following factors:

- 1. Effects of explosion of the item.
- 2. Rate of deterioration.
- 3. Sensitivity to initiation.
- 4. Type of packing.
- 5. Effects of fire involving the item.
- <u>6.</u> Quantity of explosive per unit.
- (d) Exudation.
- d. Miscellaneous entries.

Where available and appropriate, the following or related data are given, in space at the bottom of the third form, or on plain pages.

- (1) Solubility.
- (2) Methods of manufacture.
- (3) Historical information.
- (4) Bulk compressibility modulus. (q)

The direct experimental measurement of the dynamic bulk modulus of a solid is difficult, and few such measurements have been made. One apparatus has been developed at the Naval Ordnance Laboratory and is described in detail in Reference q. Bulk modulus (its reciprocal is the compressibility) is defined as the ratio of stress to strain when the stress is a pressure applied equally on all surfaces of the sample and the strain is the resulting change in volume per unit volume.

(5) Hydrolysis tests. (0)

The 240-hour hydrolysis test is conducted as follows: A 5-gm sample of the dry nitrocellulose is weighed accurately in a tare-weighed 250-cc Pyrex flask having a ground glass connection for a Pyrex condenser. Then 100 cc of distilled water is added to the nitrocellulose in the flask and the flask fitted to the condenser. The flask is placed in a steam bath in which the water is kept boiling constantly by means of electric hotplates. At the end of 240 hours the mount of solid developed by the hydrolysis of the nitrocellulose is measured by an electromatic pH method.

(6) Sensitivity to initiation by electrostatic discharge. (n)

The samples are tested under two amounts of confinement, designated as unconfined and confined. In the unconfined test, a sample of approximately 0.05 gm is dumped into a shallow depression in a steel block and flattened out with a spatula. In the confined tests (partly confined), the sample of approximately 0.05 gm is introduced into soft-glass tube ($\sim 7 \text{ mm}$ ID x 18 mm *long*) which fits over a metal peg. The volume of the space around the charge at zero gap is ~ 0.15 cc; at a gap of 0.6 mm, it is ~ 0.4 cc. In addition to providing moderate confinement, this system also minimizes dispersion of the sample by the test spark, and reduces the effect of material being repelled from the needle point by electrostatic field effect.

When a test is to be made, the needle point electrode is screwed up until the gap between electrodes is greater than the critical gap discharge at the test voltage. The sample is then placed in position, the high-voltage terminal of the charged condensor is switched to the point electrode by means of a mercury switch, and the electrode is screwed down until discharge occurs.

The spark energy (in joules), for zero probability of ignition, is determined.

(7) Destruction by chemical decomposition.

Burning is the preferred method of destroying explosives. Initiating type explosives (in quantity) are usually destroyed by detonation with demolition blocks. Destruction of explosives by chemical decomposition can be effectively used where small laboratory quantities are involved. Procedures given are standard for only lead azide, mercury fulminate and nitrogly-cerin.

(8) Other information.

(9) References.

6. REFERENCES CITED 1N INTRODUCTION, ¹

a. W. H. Rinkenbach and A. J. Clear, Standard Laboratory Procedures for Sensitivity, Brisance, and Stability of Explosives, PATR No. 1401, 18 March 1944, Revised 28 February 1950.

b. W. R. Tomlinson, Jr. and A. J. Clear, <u>Development of Standard Tests -- Application of the Impact and Sand Tests to the Study of Nitroglycerin and Other Liquid Explosives</u>, PATR No. 1738, 13 June 1949.

c. J. H. McIvor, Friction Pendulum, PA Testing Manual 7-1, 8 May 1950.

d. Departments of the Amy and the Air Force Joint Technical Manual and Technical Order, TM 9-1910/TO 11A-1-34, <u>Military Explosives</u>, April 1955.

e. J. H. McIvor, Ballistic Mortar Test, PA Testing Manual 7-2, 8 May 1950.

f. Ph. Naoum, Z ges Schiess-Sprengetoffw, pp. 181, 229, 267 (27 June 1932).

g. G. J. Mueller, <u>Equipment for the Study of the Detonation Process</u>, PATR No. 1465, 4 July 1945.

h. NDRC Interim Report, <u>Preparation and Testing of Explosives</u>, Nos. PT-19 and PT-20, February-April 1944.

i. Linnie E. Newman, PA Chemical Laboratory Report Nos. 127815 and 134476, 11 January 1951.

j. Report AC-2983/0rg Expl 179.

¹For information regarding source of references, inquiries should be made to the Commander, U.S. Army Research Office--Durham, ATTN: CRDARD-EH, Box CM, Duke Station, Durham, North Carolina 27706.

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k. Eastern Laboratory, du Pont, <u>Investigation of Cavity Effect</u>, <u>Section 111</u>, <u>Variation of</u> <u>Cavity Effect with Composition</u>, NDRC Contract W-672-ORD-\$723.

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1. J. H. McIvor, Fragmentation Test Procedures, PA Testing Manual 5-1, 24 August 1950.

m. Eastern Laboratory, du Pont, <u>Investigation of Cavity Effect</u>, Final Report, 18 September 1943, NDRC Contract W-672-ORD-5723.

n. F. W. Brown, D. H. Kusler, and F. C. Gibson, <u>Sensitivity of Explosives to Initiation</u> by <u>Electrostatic Discharges</u>, U. S. Department of Interior, Bureau of Mines, R. I. 3852, 1946.

o. D. D. Sager, <u>Study of Acid Adsorption and Hydrolysis of Cellulose Nitrate and Cellulose</u> <u>Sulphate</u>, PATR No. 174, 12 January 1932.

p. L. C. Smith and E. H. Eyster, <u>Physical Testing of Explosives</u>, Part III, Miscellaneous <u>Sensitivity Tests</u>, <u>Performance Tests</u>, <u>OSRD Report No. 5746</u>, 27 December 1945.

q. C. S. Sandler, An Acoustic Technique for Measuring the Effective Dynamic Bulk Modulus of Elasticity and Associated Loss Factor of Rubber and Plastics, NAVORD Report No. 1524, 1 September 1950.

W. S. Cramer, <u>Bulk Compressibility Data on Several Explosives</u>, NAVORD Report No. 4380, 15 September 1956.

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| Composition : | Molecular Weight: 92 |
|---|---|
| % Ammonium Nitrate 80 TNT 20 | Oxygen Balance: CO, % +1 CO % +11 |
| | Density: gm/cc Cast 1.46 |
| | Melting Point: °C |
| C/H Ratio | Freezing Point: °C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 90 | Boiling Point: °C |
| Sample Wt 20 mg | Refractive Index, n ^D ₂₀ |
| Picatinny Arsenal Apparatus, in. 15 Sample Wt, mg 17 | n ⁵ ₂₅ |
| · · · · · · · · · · · · · · · · · · · | n_30 |
| Friction Pendulum Test: | Vacuum Stability Test: |
| Steel Shoe Unaffected | cc/40 Hrs, at 90°C |
| Fiber Shoe Unaffected | 100°C 0.45 |
| Rifle Bullet Impact Test: 5 Trials | 120°C 0.95 |
| % | 135°C |
| Explosions 0 Partials 0 | 150°C 6.8 |
| Burned 0 | 200 Gram Bomb Sand Test: |
| Unaffected 100 | Sand, gm 35.5 |
| Explosion Temperature: °C | Sensitivity to Initiation: |
| Seconds, 0.1 (no cap used) | Minimum Detonating Charge, gm |
| 1 5 kcomposes 280 | Mercury Fulminate Lead Azide 0.20 |
| 10 | |
| 15 | Tetryl 0.07 |
| 20 | Ballistic Mortar, % TNT: (a) 130 |
| | Trauzi Test, % TNT: (b) 123 |
| 75°C International Heat lest: % Loss in 48 Hrs 0.06 | Plate Dent Test: Method |
| 100°C Heat Test: | Condition |
| % Loss, 1st 48 Hrs 0.03 | Confined |
| % Loss, 2nd 48 Hrs 0.05 | Density, gm/cc |
| Explosion in 100 Hrs None | Brisance, % TNT |
| Flammability Index: | Detonation Rate: |
| | Confinement None None |
| Hygroscopicity: % | Condition Cast Cast Charge Diameter, in. 1.0 1.0 |
| 0 | - |
| 30°C, 90%RH, 2 days 61 | Density, gm/cc 1.46 1.50 |

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AMCP 706-177

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| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: |
|---|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: Buff-yellow |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc | Principal Uses: Bombs, HE projectiles |
| Charge Wt, Ib | |
| Total No. of Fragments: For TNT For Subject HE | Method of Looding: Cast |
| | Loading Density: gm/cc 1.46 |
| Fragment Velocity:ft/sec(f)At 9 ft1900At 25½ ft1750Density,gm/cc | Storage: Method Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 |
| Air: Peak Pressure Impulse Energy | Compatibility Group Group I Exudation Does not exude a t 65 ⁰ C |
| Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | Booster Sensitivity Test:(a)ConditionPressedTetryl, gn100Wax, in. for 50% Detonation0.83Density, gm/cc1.65Heat of:(d, eCombustion, cal/gm1002*Explosion, cal/gm490*Gas Volume, cc/gm930* |
| | *Calculated from composition of mixture. |

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Amatol, 60/40

| Composition: % | | Molecular Weight: | 108 |
|---|-----------------|--|-------------------|
| Mitrate 70 707 | €0 40 | Oxygen Balance: CO, % CO % | -18 + 2 |
| | | Density: gm/cc Cast | 1.60 |
| | | Melting Point: °C | |
| C/H Ratio | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | 95 | Boiling Point: °C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 93 16 17 | Refractive Index, n ^o ₂₀ n ^o 25 | |
| Friction Pendulum Test: | | n ^D ₃₀ | |
| Steel Shoe Fiber Shoe | | Vacuum Stability Test: cc/40 Hrs, at 90°C | |
| Rifle Bullet Impact Test: Trials % Explosions Partiols | | 100°C 120°C 135°C 150°C | |
| Burned Unaffected | | 200 Gram Bomb Sand Test: Sand, gm | 41.5 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 | | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate | |
| 5 Decomposes 270 | | Lead Azide | 0.20 |
| 10 15 | | Tetryl | 0.06 |
| 20 | | Ballistic Mortar, % TNT: (a) | 128 |
| | | Trauzl Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | | Plate Dent Test: Method | |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | | Detonation Rate: Confinement | None |
| Hygroscopicity: % | | Condition Charge Diameter, in. | Cast 1.0 |
| Volatility: | Ni 1 | Density, gm/cc Rate, meters/second | 1.50 5760 |

| Fragmentation Test: | | Shaped Charge Effectiveness, $TNT = 100$: |
|---|---------|---|
| 90 mm HE, M71 Projectile, Lot | WC-91: | Glass Cones Steel Cones |
| Density, gm/cc | 1.49 | Hole Volume |
| Charge Wt, Ib | 1.971 | Hole Depth |
| Total No. of Fragments: | | Color: Buff-yellow |
| For TNT | 703 | Burr yenow |
| For Subject HE | 583 | Principal Uses: Bombs, HE projectiles |
| 3 inch HE, M42A1 Projectile, Lo | t KC-5: | |
| Density, gm/cc | 1.57 | |
| Charge Wt, Ib | 0.827 | |
| Total No. of Fragments: | | Method of Loading: Cast |
| For TNT | 514 | |
| F o r Subject HE | 408 | Loading Density: gm/cc 160 |
| | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | | Storage: |
| Density, gm/cc | | Method Dry |
| Blast (Relative to TNT): | | Hazard Class (Quantity-Distance) Class 9 |
| A 1 | | Compatibility Group Group I |
| Air: Peak Pressure | 95 | |
| Impulse | 85 | Exudation Does not exude at 65°C |
| Energy | 84 | |
| Air, Confined: | | <u>Heat of</u> : (d, e) |
| Impulse | | Combustion, cal/gm 1658* |
| Under Water: Peak Pressure | | Explosion, ca 1/gm 633* Gas Volume, cc/gm 880* |
| Impulse | | |
| Energy | | |
| Underground: Peak Pressure | | |
| Impulse | | |
| Energy | | |
| | | |
| | | *Calculated from composition of mixture. |

Amatol, 50/50

| Composition: | Molecular Weight: 118 |
|--|---|
| % Ammonium Nitrate 50 TNT 50 | Oxygen Balance: <i>CO</i> , % –27 <i>CO</i> % – 3 |
| | Density: gm/cc Cast 1.59 |
| | Melting Point: "C |
| C/H Ratio | Freezing Point: "C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 95 | Boiling Point: "C |
| Sample Wt 20 mg | Refractive Index, n ^D ₂₀ |
| Picatinny Arsenal Apparatus, in. 16 Sample Wt, mg 17 | n ^D ₂₅ |
| | n ₃₀ |
| Friction Pendulum Test: | Vacuum Stability Test: |
| Steel Shoe Unaffected | cc/40 Hrs, at |
| Fiber Shoe Unaffected | 90°C |
| Rifle Bullet Impact Test: Trials | 100°C 0.2 120°C 1.0 |
| % | 135°C |
| Explosions 0 | 150°C |
| Partia ls 0 | 150 0 |
| Burned O | 200 Gram Bomb Sand Test: |
| Unaffected 100 | Sand, gm 42.5 |
| Explosion Temperature: "C | Sensitivity to Initiation: |
| Seconds, 0.1 (no cap used) | Minimum Detonating Charge, gm |
| 1 5 Decomposes 265 | Mercury Fulminate |
| 10 | Lead Azide 0.20 Tetryl 0.05 |
| 15 | Tetryl 0.05 |
| 20 | Ballistic Mortar, % TNT: (a) 124 |
| | Trouzl Test, % TNT: |
| 75°C International Heat Test: | Plate Dent Test: |
| % Loss in 48 Hrs | Method B |
| 100°C Heat Test: | Condition Cast |
| % Loss, 1st 48 Hrs | Confined No |
| % Loss, 2nd 48 Hrs | Density, gm/cc 1.55 |
| Explosion in 100 Hrs | Brisance, % TNT 52 |
| | Detonation Rate: |
| Flammability Index: | Confinement None None |
| | Condition Cast Cast |
| Hygroscopicity: % Ni1 | Charge Diameter, in. 1.0 1.0 |
| Volatility: | Density, gm/cc 1.55 1.55 |
| | Rate, meters/second 6430 6230 |

| ragmentation Test: | | Shaped Charge Effectiveness, $TNT = 100$: |
|--|----------|---|
| 90 mm HE, M71 Projectile, Lot WC-91: | | Glass Cones Steel Cones (g) |
| Density, gm/cc | 1.55 | Hole Volume 53 |
| Charge Wt, Ib | 2.053 | Hole Depth 69 |
| Total No. of Fragments: | | Color: Buff-yellow |
| For TNT | 703 | |
| For Subject HE | 630 | Principal Uses: Bombs, HE projectiles |
| 3 inch HE, M42A1 Projectile, L | ot KC-5: | |
| Density, gm/cc | 1.54 | |
| Charge Wt, Ib | 0.819 | |
| Total No. of Fragments: | | Method of Loading: Cast |
| For TNT | 514 | Method of Loading: Cast |
| For Subject HE | 385 | |
| | | Loading Density: gm/cc 1.59 |
| ragment Velocity: ft/sec At 9 ft At 25½ ft | | Storage: |
| Density, gm/cc | | Method Dry |
| last (Relative to TNT): | | Hazard Class (Quantity-Distance) Class 9 |
| Air: | | Compatibility Group Group I |
| Peak Pressure | 97 | |
| Impulse | 87 | Exudation Does not exude at 65°C |
| Energy | · | |
| Lingy | | Booster Sensitivity Test: (a) |
| Air, Confined: | | Condition Cast |
| Impulse | | Tetryl, gm 100 |
| | | Wax, in. for 50% Detonation 0.60 |
| Under Water: | | Density, gm/cc 1.55 |
| Peak Pressure | | $\frac{\text{Heat of:}}{(d, e)}$ |
| Impulse | | Combustion, cal/gm 1990 Explosion, cal/gm 703* |
| Energy | 98 | Explosion, cal/gm 703* Gas Volume, cc/gm 855* |
| Underground. | | *Calculated from composition of mixture. |
| Peak Pressure | 104 | Specific Heat: $cal/gm/^{\circ}C$ (i) |
| Impulse | 104 | Temp, 20° to 80° C 0.383 |
| Energy | 104 | Bomb Drop Test: T7, 2000-1b Semi-Armor-Piercing Bomb vs Concrete: |
| | | |

Compatibility with Metals:

Dry - Metals unaffected are zinc, iron, tin, brass, brass tin plated, brass NRC coated, brass shellac coated, nickel aluminum, steel, steel plated with nickel, zinc or tin, stain-less steel, Parkerized steel, and steel coated with acid-proof black paint. Metals slightly affected are copper, bronze, lead and copper plated steel.

Preparation :

In preparing amatols the proper granulation of ammonium nitrate is required if the maximum density of the cast amatol is desired. The ammonium nitrate should be dried so as to contain not more than 0.25% moisture. It should be heated to about 90° C before being added to the appropriate weight of molten TNT contained in a melting vessel equipped with an agitator. Continue mixing to insure uniformity and load by pouring into shell or bombs.

Origin:

Developed by the British during World War I in order to conserve TNT.

References: ²

(a) L. C. Smith and E. H. Eyster, <u>Physical Testing of Explosives</u>, Part 111, Miscellaneous <u>Sensitivity Tests</u>, <u>Performance Tests</u>, <u>OSRD Report 5746</u>, 27 December 1945.

- (b) Report AC-17/Phys Ex 1.
- (c) D. P. McDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

L. C. Smith and E. G. Eyster, Physical Testing of Explosives, Part III - Miscellaneous Sensitivity Tests; Performance Tests, OSRD Report No. 5746, 27 December 1945.

(d) Committee of Div 2 and 8, NDRC, <u>Report on HBX and Tritonal</u>, OSRD Report No. 5406, 31 July 1945.

(e) Philip C. Keenan and Dorothy Pipes, <u>Table of Military High Explosives</u>, Second Revision, NAVORD Report No. 87-46, 26 July 1946.

(f) R. W. Drake, Fragment Velocity and Panel Penetration of Several Explosives in Simulated <u>Shells</u>, OSRD Report No. 5622, 2 January 1946.

(g) Eastern Laboratory, du Pont, <u>Investigation of Cavity Effect</u>, Final Report, 18 September 1943, NDRC Contract W-672-ORD-5723.

(h) Also see the following Picatinny Arsenal Technical Reports on Amatols:

| <u>o</u> | <u>1</u> | 2 | <u>3</u> | <u>1</u> | <u>5</u> | 6 | <u>7</u> | <u>8</u> | <u>9</u> |
|--|---|--|---|----------------------------------|---|---|--------------------------------------|---|---|
| 240 350 630 950 1300 1530 | 681 731 901 1051 1311 1451 1651 | 132 182 1302 1352 1372 1552 | 743 1173 1373 1323 1493 1783 | 364 694 734 874 1344 | 65 425 695 715 1145 1225 1345 1455 1885 | 266 556 986 1376 1446 1636 1796 | 1207 1457 1797 1827 2167 | 548 638 838 1098 1148 1388 1568 1838 | 549 799 929 1129 1219 1369 1559 |

(i) TM 9-1910/TO 11A-1-34, Military Explosives, April 1955.

²See footnote 1, page 10.

Ammonal

| Composition: % | | Molecular Weight: | 102 |
|---|-----------------------|---|------------|
| Ammonium Nitrate TNT Aluminum | 22 67 11 | Oxygen Balance: CO, % CO % | -55 -22 |
| Alummum | | Density: gm/cc Cast | 1.65 |
| | | Melting Point: °C | |
| C/H Ratio | | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 91 11 19 | Boiling Point: °C Refractive Index, n ^D ₂₀ n ^D ₂₃ n ^S ₃₀ | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | | Vacuum Stability Test: cc/40 Hrs, at 90°C | |
| Rifle Bullet Impact Test: Trials % Explosions Partials | | ─ 100°C 120°C 135°C 150°C | 4.4 |
| Burned Unaffected | | 200 Gram Bomb Sand Test: Sand, gm | 47.8 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Decomposes 265 10 | | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl | 0.20 |
| 15 20 | | Ballistic Mortar, % TNT: (a) | 122 |
| | | Trauzl Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | | Plate Dent Test: Method | |
| 100°C Heat Test: | | Condition | |
| % Loss, 1st 48 Hrs | 0.00 | Confined | |
| % Loss, 2nd 48 Hrs | 0.10 | Density, gm/cc Brisance, % TNT | |
| Explosion in 100 Hrs | None | | |
| Flammability Index: | | Detonation Rate: Confinement Condition | |
| Hygroscopicity: % | | Charge Diameter, in. Density, gm/cc | |
| Volatility: | | Rate, meters/second | |

Ammonal

| Fragmentation Test: | Shaped Charge Effectiveness, TNT $=$ 100: |
|--|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: |
| For Subject HE | Principal Uses: Projectile filler |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | |
| Density, gm/cc 1.65 | |
| Charge Wt, Ib | |
| Total No. of Fragments: | Method of Loading: Cast |
| For TNT 655 | Method of Loading: Cast |
| For Subject HE 550 | |
| | Loading Density: gm/cc 1.65 |
| Fragment Velocity: ft/sec | |
| At 9 ft At 25½ ft | Storage: |
| Density, gm/cc | |
| | Method Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 |
| Air: | Compatibility Group |
| Peak Pressure | |
| Impulse | Exudation |
| Energy | |
| | Origin: |
| Air, Confined: Impulse | Castable mixture developed in United States |
| | during World War I. |
| Under Water: | References: |
| Peak Pressure | (a) W. R. Tomlinson, Jr., Physical and Ex- |
| Impulse | plosive Properties of Military Explosives, |
| Energy | PAIR No. 1372, 29 November 1943. |
| Underground: | (b) Also see the following Picatinny Ar- |
| Peak Pressure | sen al Technical Reports on Ammonals: 1108, 1286, 1292, 1308 and 1783. |
| Impulse - | 1200, 1292, 1300 and 1703. |
| Energy | |
| Preparation: | |
| Procedure same as described under Amatols, except aluminum is added to the ammonium ni- trate-TNT molten mixture under agitation un- til uniformity in composition is obtained. Loading is accomplished by pouring into the appropriate projectile. | |

| Composition: % | | Molecular Weight: $(H_4 N_2 O_3)$ | 80 |
|---|---------------------------------|--|-------------------------|
| л 35 н 5 | ин _ц ио _З | Oxygen Balance: CO, % CO % | +20 +20 |
| | | Density: gm/cc Crystal | 1,73 |
| 0 60 | | Melting Point: °C | 170 |
| C/H Ratio | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 100+ 31 17 | Boiling Point: "C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| | fected | Vacuum Stability lest: cc/40 Hrs, at 90°C | 0.2 |
| Rifle Bullet Impact lest: Trials % | | ─ 100°C 120°C 135°C | 0.3 0.3 |
| Explosions 0 Partials 0 | | 150°C | 0.3 |
| Burned 0 Unaffected 100 | | 200 Gram Bomb Sand Test: Sand, gm | Ni 1 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Ignites 465 10 15 20 | | Sensitivity to Initiation: Minimum Detonating Charge, g Mercury Fulminate Lead Azide Tetryl Ballistic Mortar, % TNT: (a) | m 0.20 0.25 56 |
| 75°C International Heat lest: (a) % Loss in 48 Hrs | 0.0 | Plate Dent lest: Method | |
| 100°C Heat lest: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | 0.74 0.13 None | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | | Detonation Rote: (b) Confinement None Condition Soli | - |
| Hygrascopicity; % | Extreme | Charge Diameter, in. 1.25 Density, gm/cc 0.9 | , - |
| Volatility : Decomposes a | t 210 ⁰ C | Rate, meters/second 1000 | |

Ammonium Nitrate

| Booster Sensitivity Lest: | Decoxygeosition $(f)_{10}^{13.8}$ $(h)_{10}^{12.3}$ |
|--|---|
| Condition | (Z/sec) |
| Tetryl, gm | Heat, kilocolorie/male 40.5 38.3 |
| Wax, in. for 50% Detonation | (AH, kcal/mal) Temperature Range, °C 243-261 217-267 |
| Wax, gm | |
| Density, gm/cc | Phase Liquid |
| Heat of: Combustion, col/gm 346 Explosion, cal/gm 346 | Armor Plate Impact lest: |
| Gas Volume, cc/gm 980 | 60 mm Mortar Projectile: 50% Inert, Velocity, ft/sec |
| Formation, col/gm 1098 | Aluminum Fineness |
| Fusion, cal/gm 18.23 | |
| | 500-1b General Purpose Bombs: |
| Specific Heat: col/gm/°C (e) | Plate Thickness, inches |
| -150 0.189 0 0.397 | |
| -100 0.330 50 0.414 | 1 |
| -50 0.364 100 0.428 | 11/4 |
| | 11/2 |
| | 13⁄4 |
| Burning Rate: | |
| cm/sec | Bomb Drop lest: |
| Thermal Conductivity: col/sec/cm/°C 2.9−3.9 x 10 ^{−14} | T7, 2000-Ib Semi-Armor-Piercing Bomb vs Concrete: |
| Coefficient of Expansion: | Max Safe Drop, ft |
| Linear, %/°C | 500-lb General Purpose Bomb vs Concrete: |
| Volume, %/°C | Height, ft |
| | Trials |
| Hardness, Mohs' Scale: | Unaffected |
| | Low Order |
| Young's Modulus: | High Order |
| E', dynes/cm² | |
| E, lb/inch² | 1000-ib General Purpose Bomb vs Concrete: |
| Density, gm/cc | |
| | Height, ft |
| Compressive Strength: lb/inch ² | Trials |
| | Unaffected |
| Vapor Pressure: (g) | Low Order |
| °C mm Mercury | High Order |
| 188 3.25 | |
| 205 7.45 | |
| 216 11.55 | |
| 223 15.80 237 27:0 | |
| 249 41.0 | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT=100$: | | | | | |
|---|--|--|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | | | | | |
| Total No. of Fragments: For TNT | Color: Colorless | | | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Explosive ingredient of mixtures used in bombs or large caliber projectiles | | | | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pressed or cast depending on composition of mixture | | | | | |
| | Loading Density: gm/cc Variable | | | | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | | | | | |
| Density, gm/cc | Method Dry | | | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 12 | | | | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Group D Exudation None | | | | | |
| Air, Confined: Impulse | Effect of Temperature on Impact Sensitivity (Chemically pure grade): (b) Temp. PA Impact Test | | | | | |
| Under Water: Peak Pressure | $\frac{^{\circ}C^{2}}{25} \qquad \frac{2 \text{ Kg } \hat{\mathbb{W}}t, \text{ inches}}{31}$ | | | | | |
| Impulse Energy | 75 28 100 27 150 27 | | | | | |
| Underground: Peak Pressure | 175 12 | | | | | |
| Impulse | | | | | | |
| Energy | In the presence of moisture, ammonium nitrate reacts with copper, iron steel, brass, lead and cadmium. | | | | | |
| | Entropy: (g) | | | | | |
| | cal/mol at 25°C 36.0 | | | | | |

Ammonium Nitrate

| Wa | ater | Alco | hol | Aceti | c Acid | Nitric | Acid | <u>Py</u> | ridine |
|---|---|--|-------------------------------------|--|---|---|---|------------------|----------------------|
| <u>°c</u> 0 20 40 60 80 100 | 7 118 192 297 421 580 871 | о _с 20 40 60 78 | <u>4</u> 2.5 5 7.5 10.5 | <u>c</u> 16.6 27.0 80.9 101.0 120.0 | <u>#</u> 0.0 0.39 5.8 20.7 125 | $\begin{array}{ccc} & & & \frac{\sigma}{6} \\ \hline 0 & 4 \overline{5.1} \\ 15 & 73.0 \\ 30 & 106 \\ 75 & 201 \end{array}$ | [₱] Nitric Acid 30.0 21.7 20.8 31.6 | ° <u>C</u> 25 | ~ 2 0-2 5 |

Solubility of ammonium nitrate, grams in 100 grams (\$) of: (e)

Preparation:

Ammonium nitrate is prepared by the neutralization of an aqueous solution of ammonia with nitric acid and evaporation of the solution. The product which is very pure is dried in a graining kettle.

Origin:

First prepared by Glauber in 1659 and first used as an explosive ingredient in 1867 when a Swedish patent was granted to Ohlsson and Norrbin for a composite dynamite.

Destruction by Chemical Decomposition:

Ammonium nitrate is decomposed by strong alkalies with the liberation of ammonia, and by sulfuric acid with the formation of ammonium sulfate and nitric acid.

References: 3

(a) Departments of the Amy and the Air Force TM 9-1910/TO lla-1-34, Military Explosives, April 1955.

(b) P. F. Macy, T. D. Dudderar, E. F. Reese and L. H. Eriksen, <u>Investigation of Sensitivity</u> of Fertilizer Grade Ammonium Nitrate to Explosion, PATR No. 1658, 11 July 1947.

(c) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(d) L. C. Smith and E. G. Eyster, Physical Testing of Explosives, Part III - Miscellaneous Sensitivity Tests; Performance Tests, OSRD Report No. 5746, 27 December 1945.

(e) International Critical Tables, McGraw-Hill Book Co., N. Y., Land-Bornst.

G. D. Clift and B. T. Federoff, <u>A Manual for Explosives Laboratories</u>, Vol. 11, Lefax Society, Inc., Philadelphia, 1943.

(f) R. J. Finkelstein and G. Gamow, <u>Theory of the Detonation Process</u>, NAVORD Report No. 90-46, 20 April 1947.

(g) George Feick, The Dissociation Pressure and Free Energy of Formation of Ammonium Nitrate, Arthur D. Little, Inc., J Am Chem Soc, <u>76</u>, 5858-60 (1954).

(h) M. A. Cook and M. Taylor Abegg, "Isothermal Decomposition of Explosive;,' University of Utah, <u>Ind Eng Chem</u>, June 1956, pp. 1090 to 1095.

³See footnote 1, page 10.

Ammonium Nitrate

| (I) | | | 0 | * | | 1 | | | |
|-----------------------------------|---|---------------------|-----------------------------|--|---|--|-----------------------------|-----------------------------------|---------------------|
| <u>o</u> | <u>1</u> | 2 | 3 | 4 | <u>5</u> | 6 | <u>7</u> | 8 | ೨ |
| 240 350 630 1290 1720 | 681 731 1051 1241 1311 1391 1431 | 182 1302 1682 | 743 1323 1783 2183 | 364 984 1094 1214 1234 1304 | 695 1145 1225 1455 1635 1675 1675 1725 | 596 666 676 946 1106 1696 | 907 1117 1947 2167 | 548 638 938 1008 1038 | 799 1369 1409 |

(i) Also see the following Picatinny Arsenal Technical Reports on Ammonium Nitrate:

| Coyorition: | Molecular Weight: (ClH ₁₄ NO ₁₄) | 117.5 | | | |
|--|---|----------------|--|--|--|
| Cl 30.2 N 11.9 | Oxygen Balance: CO, % CO % | +27·3 +27·3 | | | |
| NH ₁ , ClO ₁ , | Density: gm/cc | 1.95 | | | |
| н 3.4 4 7 | Melting Point: °C | | | | |
| 54.5 €/Н _{Ratio} | Freezing Point: °C | | | | |
| | | | | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 67 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 24 Sample Wt, mg 24 | Boiling Point: "C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | | | | |
| Friction Pendulum Test: Steel Shoe Snaps Fiber Shoe Unaffected | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C | 0,13 | | | |
| Rifle Bullet Impact Test: Trials | 120°C 135°C | 0.20 | | | |
| Explosions Partia Is | 150°C | 0.32 | | | |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm 6.0 | | | | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 435 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide | 0.20 | | | |
| 10 | Tetryl | 0.25 | | | |
| 20 | Ballistic Mortar, % TNT: | | | | |
| | _, Trauzl Test, % TNT: | | | | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method | | | | |
| 100°C Heat Test: | Condition | | | | |
| % Loss, 1st 48 Hrs 0.02 | Confined | | | | |
| % Loss, 2nd 48 Hrs 0.00 | Density, gm/cc Brisance, % TNT | | | | |
| Explosion in 100 Hrs None | | | | | |
| Flammability Index: | Detonation Rate: Confinement Condition | | | | |
| Hygroscopicity: % | Condition Charge Diameter, in. | | | | |
| Volatility : | Density, gm/cc Rate, meters/second | | | | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | | | |
|--|---|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91 : Density, gm/cc Charge Wt, lb | Glass Cones Steel Cones Hole Volume Hole Depth | | | |
| Total No. of Fragments : For TNT | Color: Colorless | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Explosive ingredient of mixtures used in pyrotechnics and as projectile filler | | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pressed or cast depending on composition of mixture | | | |
| | Loading Density: gm/cc Variable | | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | | | |
| Density, gm/cc | Method Dry | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 | | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation None | | | |
| Air, Confined: Impulse | Solubility in Water gm/100 cc saturated solution: 0°C 12 | | | |
| Under Water: Peak Pressure Impulse | 25°C 20 60°C 39 100°C aa | | | |
| Energy | Preparation: | | | |
| Underground: Peak Pressure Impulse Energy | The perchlorates are prepared by the action of the acid on a suitable base; by the ther- mal decomposition of certain chlorates; and by the electrolysis of chlorates (see origin). <u>Heat of:</u> | | | |
| | Formation, cal/gm 665 | | | |

Origin: (c)

E. Mitscherlich first prepared, in 1832, crystals of ammonium perchlorate from barium perchlorate and ammonium sulfate (Pogg Ann 25, 300). T. Schlosing treated a hot solution of sodium perchlorate with ammonium chloride, and on cooling, crystals of ammonium perchlorate were obtained (Comp rend, 73, 1269, [1871]). U. Alvisi treated a mixture of 76 parts of ammonium nitrate with 213 parts of sodium perchlorate, and obtained a crop of small crystals of ammonium perchlorate which were purified by recrystallization from hot water (German Patent, 103, 993, 1898). A. Miolati mixed magnesium or calcium perchlorate with ammonium chloride and crystals of ammonium perchlorate deposited from the solution of very soluble magnesium or calcium chloride (German Patent, 112, 682, 1899).

References: 4

(a) W. R. Tomlinson, Jr., <u>Physical and Explosive Properties of Military Explosives</u>, PATR No. 1372, 29 November 1943.

(b) T. L. Davis, <u>The Chemistry of Powder and Explosives</u>, John Wiley and Sons, Inc., New York, 1943.

(c) J. W. Mellor, <u>A Comprehensive Treatise on Inorganic and Theoretical Chemistry</u>, Vol. 11, Longmanns, Green and Co., London, 1922, p. 396.

(d) Also see the following Picatinny Arsenal Technical Reports on Ammonium Perchlorate:

| ۵ | 1 | 3 | 4 | 5 | <u>a</u> | 9 |
|-----|-----|-------------|-------------------|----------------------|----------|--------------|
| 100 | 321 | 843 1783 | 354 604 854 | 1095 1725 2205 | 1726 | 1049 1969 |

⁴See footnote 1, page 10.

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| Composition: | Molecular Weight: 125 |
|---|--|
| % Barium nitrate 67 | Oxygen Balance: CO % CO % |
| TNT 33 | Density: gm/cc Cast 2.55 |
| | Melting Point: "C |
| C/H Ratio | Freezing Point: °C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 35 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 11 Sample Wt, mg 24 | Boiling Point: °C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C |
| Rifle Bullet Impact Test: Trials % Explosions Partials | 100°C 120°C 135°C 150°C |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm 26.8 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Ignites 3 ⁸ 5 10 15 20 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide 0.20 Tetryl 0.10 Ballistic Mortar, % TNT: |
| 75°C International Heat Test: % Loss in 48 Hrs | Trauzi Test, % TNT: Plate Dent Test: (a) 73/27 Method B |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | ConditionCastConfinedNoDensity, gm/cc2.52Brisance, % TNT61 |
| Flammability Index: | Detonation Rate: Confinement |
| Hygroscopicity: % 30 ⁰ C, 90% RH 0.00 | Condition Charge Diameter, in. Density, gm/cc |
| Volatility: | Rate, meters/second |

Baratol

| Booster Sensitivity Test: Condition Cast | Decomposition Equation: Oxygen, otoms/sec |
|---|---|
| | (Z/sec) |
| Tetryl, gm 100 Wax, in. for 50% Detonation 0-32 | Heat, kilocolorie/mole |
| | (AH, kcol/mol) Temperature Range, °C |
| Wax, gm | |
| Density, gm/cc 2,55 | Phase |
| Heat of: Combustion, col/gm | Armor Plate Impact Test: |
| Explosion, cal/g m | 60 mm Mortar Projectile: |
| Gas Volume, cc/gm | 50% Inert, Velocity, ft/sec |
| Formation, col/gm | Aluminum Fineness |
| Fusion, col/gm 75/25 Baratol 2.8 (d) | |
| | 500-lb General Purpose Bombs: |
| Specific Heat: col/gm/°C (d) 75/25 Baratol <u>°C</u> | Plate Thickness, inches |
| | 1 |
| -75 0.152 75 0.280 0 0.147 85 0.213 | 11/4 |
| 25 0.180 90 0.201 | |
| 50 0.229 100 0.171 | |
| Burning Bate | 13⁄4 |
| Burning Rate: cm/sec | Bomb Drop Test: |
| Thermal Conductivity | 1 ' |
| Thermal Conductivity: cal/sec/cm/°C | T7, 2000-Ib Semi-Armor-Piercing Bomb vs Concrete: |
| Coefficient of Expansion: | Max Safe Drop, ft |
| Linear, %/°C | 500-Ib General Purpose Bomb vs Concrete: |
| Volume, %/°C | Height, ft |
| | Trials |
| Hardness, Mohs' Scale: | Unaffected |
| | Low Order |
| Young's Modulus: | High Order |
| E', dynes/cm² | |
| E, Ib/inch ² | 1000-lb General Purpose Bomb vs Concrete: |
| Density, gm/cc | |
| Compressive Observable 16 /inst-2 | Height, ft |
| Compressive Strength: Ib/inch ² | Trials |
| | Unaffected |
| Vapor Pressure: | Low Order |
| °C mm Mercury | High Order |
| | |
| | |
| | |
| | |
| | 1 |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | | | |
|---|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | | | |
| Total No. of Fragment s: For TNT | Color: | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib Total No. of Fragments : | Principal Uses: Bomb filler | | | |
| For TNT For Subject HE | Method of Loading: Cast | | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc | Loading Density: gm/cc 2.55 Storage: Method Dry | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 | | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Group I Exudation | | | |
| Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | <u>Preparation:</u> The appropriate weight of barium nitrate heated to about 90°C is added to molton TNT contained in a melting vessel equipped with an agitator. Continue mixing until uniform, and load by pouring at the lowest practical temperature. <u>Origin:</u> Baratol, an explosive containing barium nitrate and TNT, the proportions varied to suit the required purposes, was developed during World War I. | | | |

Baratol

References: 5

(a) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(b) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, Part III - Miscellaneous <u>Sensitivity Tests</u>; <u>Performance Tests</u>, OSRD Report No. 5746, 27 December 1945.

(c) Also see the following Picatinny Arsenal Technical Reports on Baratol:

| <u>o</u> | <u>3</u> | <u>6</u> | 8 |
|--------------|---------------|----------|------|
| 2010 2160 | 1-783 2233 | 2226 | 2138 |

(d) C. Lenchitz, W. Beach and R. Valicky, <u>Enthalpy Changes</u>, <u>Heat of Fusion and Specific</u> <u>Heat of Basic Explosives</u>, PATR No. 2504, January 1959.

⁵See footnote 1, page 10.

| Composition: | Molecular Weight: | 111 |
|--|---|--------------|
| % Barium nitrate 50 TNT 35 | Oxygen Balance: C0, % C0 % | -24 - 7 |
| Aluminum 15 | Density: gm/cc | 2.32 |
| | Melting Point: °C | |
| C/H Ratio | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 30 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 12 Sample Wt, mg 22 | Boiling Point: "C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C | |
| Rifle Bullet Impact Test: Trials % Explosions Particils | 120°C 135°C 150°C | |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm | 39.8 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Ignites 3 ¹⁴ 5 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate | |
| 10 | Lead Azide Tetryl | 0.20 0.10 |
| 15 20 | Ballistic Mortar, % TNT: (a) | 96 |
| | Trauzl Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method | |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: (b) Confinement | None |
| | Condition Charge Diameter, in. | Cast 1.0 |
| Hygroscopicity: % | | 1.0 |

Baronal

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT=4$ | 100: |
|--|--|--------------|
| 90 mm HE, M71 Projectile, Lot WC-91: | Glass Cones Steel | Cones |
| Density, gm/cc | Hole Volume | |
| Charge Wt, Ib | Hole Depth | |
| | | |
| Total No. of Fragments: | Color: | |
| For TNT | | |
| For Subject HE | Principal Uses: Bomb filler | |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | | |
| Density, gm/cc | | |
| Charge Wt, Ib | | |
| | | |
| Total No. of Fragments: | Method of Loading: Cast | |
| For TNT | | |
| For Subject HE | | |
| | Loading Density: gm/cc 232 | |
| Fragment Velocity: ft/sec At 9 ft | | |
| At 25½ ft | Storage: | |
| Density, gm/cc | | |
| | Method | Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 |
| | | ~ - |
| Air: Peak Pressure | Compatibility Group | Group I |
| Impulse | Exudation | |
| Energy | | |
| | Preparation: | |
| Air, Confined: | | |
| Impulse | Procedure same as described | |
| Under Water: | except aluminum is added to th trate-INT molton mixture under | |
| Peak Pressure | until uniformity in comparison | is obtained. |
| Impulse | Booster Sensitivity Test: | |
| Energy | | (c) |
| Underground: | Condition Tetryl, gm | Cast 100 |
| Peak Pressure | Wax, in. for 50% Detonation | 0.86 |
| impulse | Density, gm/cc | 2.32 |
| Energy | Heat of: | |
| | Combustion, cal/gm | 2099 |
| | Explosion, cal/gm | 1135 |
| | Gas Volume, cc/gm | 410 |
| | | |
| | | |

Barona 1

References: 6

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III</u> - <u>Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, <u>OSRD Report No. 5746</u>, 27 December 1945.

(b) G. H. Messerly, <u>The Rate of Detonation of Various Explosive Compounds</u>, OSRD Report No. 1219, 22 February 1943.

M. D. Hurwitz, The Rate of Detonation of Various Compounds and Mixtures, OSRD Report No. 5611, 15 January 1946.

(c) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(d) Arthur D. Little Report, Study of Pure Explosive Compounds, Part III, Correlation of Composition of Mixture with Performance, Contract No. DA-19-020-ORD-12, I May 1950.

(e) S. J. Lowell, Propagation of Detonation in Long and Narrow Columns of Explosives, PATR No. 2138, February 1955.

⁶See footnote 1, page 10.

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Black Powder

| Composition: | Molecular Weight: 84 |
|---|--|
| Potassium nitrate 74.0 Sulfur 10.4 Charcoal 15.6 | Oxygen Balance: CO, %-22 - 2CO %- 2Density: gm/ccVariable |
| C/H Ratio | Melting Point: °C Freezing Point: "C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 3 ² Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 16 | Boiling Point: "C Refractive Index, n ^D ₂₀ |
| Sample Wt, mg 16 | n ² 3 n ³⁰ |
| Friction Pendulum lest: Steel Shoe Snaps Fiber Shoe Unaffected Rifle Bullet Impact lest: Trials % | Vacuum Stability lest: cc/40 Hrs, at 90°C 100°C 0.5 120°C 0.9 135°C |
| Explosions Partials Burned Unaffected | 150°C 200 Gram Bomb Sand Test: Sand, gm 8 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 510 1 490 5 Ignites 10 356 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryi Sensitive to igniting fuse |
| 15 20 | Ballistic Mortar, % TNT: 50 |
| | Trauzi lest, % TNT: (a) 10 |
| 75°C International Heat lest: % Loss in 48 Hrs 0.31 | Plate Dent Test: Method |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT |
| Flammability Index: | Detonation Rate: Confinement |
| 26°C, 75% RH 0.75 Hygroscopicity: % 25°C, 90% RH 1.91 30°C, 90% RH 2.51 | Condition Charge Diameter, in. |
| Volatility: | Density, gm/cc 1.6 Rate, meters/second 400 |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT=100$: |
|---|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: Black |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: 1. Igniter powder 2. Time rings (fuzes) |
| Total No. of Fragments: For TNT | Method of Loading: 1. Loose (granulated) 2. Pressed |
| For Subject HE Fragment Velocity: ft/sec | Loading Density: gm/cc p si x 10 ³ 25 50 60 65 70 75 1.74 1.84 1.86 1.87 1.88 1.89 |
| At 9 ft At 25½ ft Density, gm/cc | Storage: Method Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 |
| Air: Peak Pressure Impulse Energy | Compatibility Group Group O Exudation None |
| Air, Confined: Impulse | 100°C Vacuum Stability Test,cc gas/40 hrs:Initial Value0.5After 2 hours at 65°C0.86 |
| Under Water: Peak Pressure Impulse Energy | After 2 hours at 65°C, 75% RH1.46Sensitivity to Electrostatic(b)Unconfined>12.5 |
| Underground: Peak Pressure Impulse Energy | Confined 0. a <u>Compatibility with Metals:</u> Dry - Compatible with all metals when moisture content is less than 0.20%. |
| <u>Initiating Efficiency:</u> Grams Required to Initiate | Wet - Attacks all common metals except stainless steel. Heat of: |
| Igniter Comp K-312.0Igniter Comp K-292.3 | Explosion, cal/gm 684 Gas Volume, cc/gm 271 |

Black Powder

Preparation:

Willow or alder charcoal, flour of sulphur and 2-3% of water are placed in a tumbling barrel and mixed for a short period (about 1/2 hour). The mixture is transferred to a "wheel mill" and crystalline potassium nitrate containing 3-4% moisture is added and the mixture is incorporated for several hours. During the incorporation period the mixture is kept damp (2-3% moisture) by adding water at intervals. The mill cake is then pressed at 6000 psi between aluminum plates. The pressed cakes are broken up between rubber or wood rolls. The material is screened and the various particle sizes are separated as desired. The screened material is then transferred to canvas trays and dried in hot air ovens at 60° C. If it is desired to glaze the black powder, the material before drying is polished by rotation in a tumbling barrel to give it a smooth surface. It is next screened to remove the dust. The smooth particles are then placed in a wooden barrel and rotated with graphite. The material is again screened to remove the excess graphite, and dried. Material finer than #40 U. S. Sieve is not graphited.

WARN ING

The batches of black powder must be of sufficient size to cover the bed of the "wheel mill." If the wheels run off on the bare bed, explosions usually result.

Origin:

The exact date of the discovery of black powder is unknown. Historians attribute its discovery to the Chinese, Hindus or Arabs. The Greeks used it during the 7th Century. Marcus Graecus in the 9th Century and Roger Bacon in the 13th Century described compositions similar to the present powder. Beginning with the 16th Century, the composition of black powder containing potassium nitrate, charcoal and sulfur has remained unchanged with respect to the proportionality (75/15/10) of the ingredients.

Destruction by Chemical Decomposition:

Black powder can be desensitized by leaching with water to dissolve the potassium nitrate. The washings must be disposed of separately because the residue of sulfur and charcoal is combustible but not explosive.

References: 7

(a) Ph. Naoum, Nitroglycerine and Nitroglycerine Explosives, Baltimore, 1928.

(b) F. W. Brown, D. H. Kusler and F. C. Gibson, Sensitivity of Explosives to Initiation by <u>Electrostatic Discharges</u>, U. S. Department of the Interior, Bureau of Mines R1 3852, 1946.

(c) Also see the following Picatinny Arsenal Technical Reports on Black Powder:

'See footnote 1, page 10.

| | | | | Blac | <u>k Powder</u> | | | | AMCP 706-177 |
|-----------------------------------|---|---|--|---|---|---|---|---|--|
| <u>o</u> | 1 | 2 | <u>3</u> | 4 | 5 | 6 | 1 | 8 | <u>9</u> |
| 250 710 850 1010 1450 | 91 471 661 901 1111 1241 1451 1541 1711 1911 1951 2051 | 222 272 322 492 582 762 872 1022 1622 1712 1802 1912 | 1633634538431043125312431333149315831683181318431973 | 354 454 554 554 574 654 664 774 844 1114 1154 1244 1504 | 65 415 545 605 1145 1275 1815 1885 1905 1915 | 56 176 356 686 1256 1316 1536 1576 1586 1946 | 347 407 547 757 847 1097 1797 1807 1827 | 188 31.8 428 558 598 608 618 698 838 898 1068 1388 1528 1778 1808 1838 1928 2178 | 379 819 839 849 859 899 1259 1309 1339 1349 1589 173P 1869 1889 |

| Composition: | Molecular Weight: (C ₄ H- _N N ₃ 0 ₉) 241 |
|--|---|
| б С 19.9 н 2.9 ^н 2 ^{с-омо} 2 | Oxygen Balance: -17 C0, % 10 |
| н ₂ с N 17.5 / | Density: gm/cc Liquid 1.52 |
| 0 59.7 | Melting Point: °C |
| ^H 2 ^{C−ON0} 2 C/H Ratio 0,13 | Freezing Point: °C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 58 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. <u>~1</u> Sample Wt, mg | Boiling Point: °C Refractive Index, n ^o ₂₀ 1.4738 n ^o ₂₅ n ^o ₃₀ |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C 2.33 |
| Rifle Bullet Impact Test: Trials % Explosions Partials | 120°C 135°C 150°C |
| Burned Unaffected | 200 Gram Bomb Sand Test:Sand, gm48.6 |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) 1 5 Decomposes 230 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide 0.20 Tetryl 0.10 |
| 15 20 | Ballistic Mortar, % TNT: |
| | Trauzi Test, % TNT: |
| 75°C International Heat lest: % Loss in 48 Hrs | Plate Dent Test: Method |
| 100°C Heat Test: % Loss, 1st 48 Hrs 1.5 % Loss, 2nd 48 Hrs 1.2 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT |
| Flammability Index: | Detonation Rate: Confinement |
| Hygroscopicity: % (a) 100 ^o F, 95% RH, 24 hrs 0.14 Volatility: | Condition Charge Diameter, in. Density, gm/cc |
| Volatility: 60°C, mg/cm ² /hr 46 | Rate, meters/second |

1,2,4-Butanetriol Trinitrate (BTTN) Liquid

AMCP 706-177

| agmentation lest: | | Shaped Charge Effectiveness, TNT | - 100. |
|--|---------------------|--|---------------|
| 90 mm HE, M71 Projectile, Lot WC | -91: | Glass Cones Ste | eel Cones |
| Density, gm/cc | | Hole Volume | |
| Charge Wt, Ib | | Hole Depth | |
| Total No. of Fragments: | | Color: Yellow | oil |
| For TNT | | | 0 |
| For Subject HE | | Principal Uses: Explosive pla | asticizer for |
| 3 inch HE, M42A1 Projectile, Lot K | C-5: | nitrocellulo | |
| Density, gm/cc | | | |
| Charge Wt, Ib | | | |
| Total No. of Fragments: For TNT | | Method of Loading: | |
| For Subject HE | | Loading Density: gm/cc | 1.52 |
| | | | 1.52 |
| agment Velocity: ft/sec At 9 ft | | | _ |
| At 25½ ft | | Storage: | |
| Density, gm/cc | | Method | |
| ast (Relative to TNT): | | Hazard Class (Quontity-Distance | e) |
| Air: | | Compatibility Group | |
| Peak Pressure | | | |
| Impulse | | Exudation | |
| Energy | | | |
| Air, Confined: | | Solubility in Water, gm/100 gm, at: | (a) |
| Impulse | | 20 ⁰ C | 0.08 |
| Under Water: | | 60 ⁰ C | 0.15 |
| Peak Pressure | | Solubility of Water in, | (a) |
| Impulse | | gm/100 gm: | Ò.Ó4 |
| Energy | | Solubility, gm/100 gm, at 25°C, in: | |
| Underground: | | | |
| Peak Pressure | | Ether Alcohol | w 00 |
| Impulse | | 2:1 Ether:Alcohol | 00 |
| Energy | | Acetone | w |
| Heat of: | (a) | Viscosity, centipoises: | (a) |
| Combustion, cal/gm Explosion, cal/gm Gas Volume, cc/gm | 2168 1457 840 | Temp. 25 ⁰ C | 59 |

Preparation (Laboratory Procedure):

To a cooled mixture of 73.8 gm of 100% nitric acid, 46.2 gms of 106.2% sulfuric acid and 60.0 gm of 96.1% sulfuric acid, 30 gms of the original (or redistilled) 1,2,4-butanetriol was added dropwise with agitation for a period of thirty minutes. The temperature of the reaction mixture was kept at $0^{\circ}-5^{\circ}$ C. When the agitation was completed, stirring was continued for one and one-half hours. The mixture was poured into ice water, and the resulting oil suspension was extracted with three 100 milliliter portions of ether. The combined ether extracts were washed with water, then with a 5% sodium bicarbonate solution and finally with water. The neutralized extract was dried with anhydrous calcium chloride and then the ether was evaporated. The yellow oil was dried in a vacuum desiccator over anhydrous calcium chloride until the material was brought to constant weight.

Origin:

1,2,4-butanetriol was first synthesized by Wagner and Ginsberg in 1894 by oxidizing allyl carbinol with potassium permanganate under mild conditions (Ber 27, 2437). Recently the U. S. Rubber Laboratory, under the direction of P. Tawney, devised a new synthesis carried out with allyl acetate and formaldehyde to give 1,2,4-butane triacetate which was readily hydrolysed to butanetriol (U. S. Rubber Company Quarterly Report, May 1948). Working with pure 1,2,4-butane-triol prepared by an improved technique of the Wagner method, the U. S. Naval Laboratory in 1948 nitrated the butanetriol on a laboratory and a pilot plant scale (Reference a).

References: 8

(a) J. A. Gallaghan, F. Macri, J. Bednarik, and F. McCollum, <u>The Synthesis of 1,2,4-Butane-triol and the Evaluation of Its Trinitrate</u>, U. S. Naval Powder Factory Technical Report No. 19, 10 September 1948.

(b) Also see the following Picatinny Arsenal Technical Reports on Butanetriol Trinitrate: 1755 and 1786.

⁸See footnote 1, page 10.

Composition A-3

AMCP 706-177

| Composition: | | Molecular Weight: | 227 |
|--|------|--|--------------|
| % RDX 9 1 | | Oxygen Balance: CO₂ % CO % | -48 |
| Wax 9 | | Density: gm/cc 12,000 ps | |
| пал | | Density: gm/cc 12,000 ps Melting Point: °C | 31 |
| | | -Melting Point: °C | |
| | | Freezing Point: °C | |
| C/H Ratio | | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | 100+ | Boiling Point: "C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. | 16 | Refractive Index, $\mathbf{n}_{20}^{\mathbf{D}}$ | |
| Sample Wt, mg | 17 | n ₂₅ | |
| · · · · | | n ₃₀ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| Steel Shoe Unaffe | cted | cc/40 Hrs, at | |
| Fiber Shoe Unaffe | cted | 90°C | 0.3 |
| Rifle Bullet Impact Test: Trials | | 100°C 120°C | 0.6 |
| % | | 135°C | 0.0 |
| Explosions 0 | | 150°C | |
| Partiols 0 | | 130 C | |
| Burned 0 | | 200 Gram Bomb Sand Test: | |
| Unaffected 100 | | Sand, gm | 51.5 |
| Explosion Temperature: "C | | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) | | Minimum Detonating Charg | |
| 1 | | Mercury Fulminote | 0.22* |
| 5 Decomposes 250 |) | Lead Azide | 0.25* |
| 10 | | * Tetryi Alternative initiating | charges |
| 15 | | | a) 135 |
| 20 | | TrauzI Test, % TNT: | |
| 75°C International Heat Test: | | Plate Dent Test: (b) | |
| % Loss in 48 Hrs | | Method B | В |
| | | Condition Pre | ssed Pressed |
| 100°C Heat Test: % Loss, 1st 48 Hrs | 0.15 | Confined No | No |
| % Loss, 2nd 48 Hrs | 0.15 | Density, gm/cc 1.6 | 1 1.20 |
| Explosion in 100 Hrs | None | Brisance, % TNT 126 | 5 75 |
| • | | Detonation Rate: (c) | |
| Flammability Index: | 195 | Confinement | None |
| - | | Condition | Pressed |
| Hygroscopicity: % 30⁰C, 90% RH | 0.0 | Charge Diameter, in. | 1.0 |
| Valatility 5000 15 to | | Density, gm/cc | 1.59 |
| Volatility: 50°C, 15 days | 0.03 | Rate, meters/second | 8100 |

| Fragmentation Test: | | Shaped Charge Effectiveness, $TNT = 100$: |
|--------------------------------------|--------------|--|
| 90 mm HE, M71 Projectile, Lot | WC-91: | Glass Cones Steel Cones |
| Density, gm/cc | 1.62 | Hole Volume |
| Charge Wt, Ib | 2.102 | Hole Depth |
| Total No. of Fragments: | | Calor: White-buff |
| For TNT | 70 <u>3</u> | |
| For Subject HE | 1138 | Principal Uses: HE, SAP, AP projectiles; |
| 3 inch HE, M42A1 Projectile, Lo | ot KC-5: | Shaped Charges |
| Density, gm/cc | 1.64 | |
| Charge Wt, Ib | 0.861 | |
| Total No. of Fragments: For TNT | 514 | Method of Loading: Pressed |
| For Subject HE | 710 | |
| | | Loading Density: gm/cc psix 10 ³ |
| Fragment Velocity: ft/sec | | 3 12 1.47 1.65 |
| At 9 ft At 25½ ft | 2800 2530 | Storage: |
| Density, gm/cc | 1.61 | Method Dry |
| Blast (Relative to TNT); | | Hazard Class (Quantity-Distance) Class 9 |
| Air: | | Compatibility Group Group I |
| Peak Pressure | | Exudation Does not exude at 65°_{2} C when waxes |
| Impulse | | melting sharply at or above 75°C are used. |
| Energy | | |
| Air, Confined: | | Preparation: |
| Impulse | | A water slurry of RDX is heated to 100 ^o C with agitation. Wax and a wetting agent are added and the mixture, under agitation, is |
| Peak Pressure | | cooled below the melting point of the wax. The wax coated RDX is collected on a filter and air dried at 75°C. |
| Impulse Energy | | Effect of Temperature on Rate of Detonation: (e) |
| Underground: Peak Pressure | | 16 hrs at, ^o c -54 21 Density, gm/cc 1.51 1.51 |
| Impulse | | Rate, m/sec 7600 7620 |
| Energy | | Booster Sensitivity Test: (d) |
| | | ConditionPressedTetryl, gn100Wax, in. for 50% Detonation1.70Density, gm/cc1.62 |
| | | Heat of: Combustion, cal/gm 1210 |

Compatibility with Metals:

Dry - Aluminum, stainless steel, mild steel, mild steel coated with acid-proof black paint and mild steel plated with nickel or zinc are unaffected. Copper, magnesium, magnesium-aluminum alloy, brass and mild steel plated with cadmium or copper are slightly affected.

Wet - Stainless steel is unaffected. Copper, aluminum, magnesium, brass, mild steel, mild steel coated with acid-proof black paint and mild steel plated with copper, cadmium, nickel or zinc are slightly affected.

Origin:

Developed by the British during World War II as RDX and beeswax. Subsequent changes in the United States replaced beeswax with synthetic waxes, changed the granulation of RDX and improved the method of manufacture.

Destruction by Chemical Decomposition:

RDX Composition A-3 (RDX/wax, 91/9) is decomposed by adding it slowly to 25 times its weight of boiling 5% sodium hydroxide. Boiling of the solution is continued for one-half hour.

References: 9

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III - Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, OSRD Report No. 5746, 27 December 1945.

(b) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(c) G. H. Messerly, The Rate of Detonation of Various Explosive Compounds, OSRD Report No. 1219, 22 February 1943.

M D. Hurwitz, <u>The Rate of Detonation of Various Compounds and Mixtures</u>, OSRD Report No. 5611, 15 January 1946.

(a) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute for</u> <u>Tetryl in Boosters</u>, NOL Mano 10,303, dated 15 June 1949.

(e) W. F. McGarry and T. W. Stevens, <u>Detonation Rates of the More Important Military Explo-</u> sives at Several Different Temperatures. PATR No. 2383, November 1956.

(f) Also see the following Picatinny Arsenal Technical Reports on RDX Composition A-3:

| <u>o</u> | 1 | 2 | 3 | 4 | <u>5</u> | 6 | <u>_7</u> | 8 | 9 |
|--------------|--------------|--------------|------|------------------------------|--|--------------|----------------------|------------------------------|--------------|
| 1380 1910 | 1451 1761 | 1492 2112 | 1493 | 1424 1614 1634 2154 | 1325 1585 1595 1715 1885 2235 | 1556 1936 | 1687 1787 1797 | 1338 1388 1728 1838 | 1639 2179 |

⁹See footnote 1, page 10.

| Composition: | Molecular Weight: 224 |
|--|--|
| % RDX 60 TNT 40 | Oxygen Balance: CO, % -43 CO % 10 |
| | Density: gm/cc Cast 1.65 |
| Wax, added 1 | Melting Point: "C (1) 78-80 |
| C/H Ratio | Freezing Point: "C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 75 | Boiling Point: °C |
| Sample Wt 20 mg | Refractive Index, ⊓₂₀ |
| Picatinny Arsenal Apparatus, in. 1^{h} Sample Wt mg 19 | n ₂₅ |
| Sample Wt, mg 19 | n ₃₀ |
| Friction Pendulum Test: | Vacuum Stability Test: |
| Steel Shoe Unaffected | cc/40 Hrs, at |
| Fiber Shoe Unaffected | 90°C 100°C 0.7 |
| Rifle Bullet Impact Test: Trials | 100°C 0.7 120°C 0.9 |
| . % | 135°C |
| Explosions 3 | 150°C 11+ |
| Partials 13 | |
| Burned 4 | 200 Gram Bomb Sand Test: |
| Unaffected 80 | Sand, gm 54.0 |
| Explosion Temperature: "C | Sensitivity to Initiation: |
| Seconds, 0.1 (no cap used) 526 | Minimum Detonating Charge, gm |
| 1 3 68 | Mercury Fulminate 0.22* |
| 5 Decomposes 278 | Lead Azide 0.20* |
| 10 255 | * Tetryl Alternative initiating charges |
| 15 > 250 | |
| 20 > 250 | |
| 75°C International Heat Test | Trauzi Test, % TNT: (b) 130 |
| % Loss in 48 Hrs | Plate Dent Test: (c) |
| | Method B |
| 100°C Heat Test: | Condition Cast |
| % Loss, 1st 48 Hrs 0.2 | Confined No |
| % Loss, 2nd 48 Hrs 0.2 | Density, gm/cc 1.71 |
| Explosion in 100 Hrs None | Brisance, % TNT 132 |
| | Detonation Rate: |
| Flammability Index: 177 | Confinement None |
| Hygroscopicity: % 30 [°] C, 90% RH 0.02 | Condition Cast |
| Hygroscopicity: % 30°C, 90% RH 0.02 | Charge Diameter, in. 1.0 |
| Volatility: | Density, gm/cc 1.68 |
| voraunty. | Rate, meters/second 7840 |

| Booster Sensitivity Test: Condition | (d) Cast | Decomposition Equation: Oxygen, atoms/sec | | |
|--|----------------|--|----------------|-------------------|
| Tetryl, gm | 100 | (Z/sec) Heat, kilocolorie/molo | 2 | |
| Wax, in. for 50% Detonation | 1.40 | (AH, kcol/mol) | | |
| Wax, gm | | Temperature Range, ' | °C | |
| Density, gm/cc | 1.69 | Phase | | |
| Heat of: Combustion, col/gm | (e) 2790 | Armor Plate Impact Tesi | t: | (e) |
| Explosion, col/gm Gas Volume, cc/gm | 1240 | 60 mm Mortar Project 50% Inert, Velocity | y, ft/sec | 209 |
| Formation, cal/gm Fusion, cal/gm (1) | 8.0 | Aluminum Finenes | | |
| | | 500-1b General Purpo | se Bombs: | |
| Specific Heat: col/gm/°C (1) | | Plate Thickness, in | ches | |
| | | | Trials | <u>% Inert</u> |
| -75 0.235 $750 0.220 85$ | 0,376 0,354 | 1 | 4 | 100 |
| 0 0.220 85 25 0.254 90 | 0.341 | ۱1⁄4 | 6 | 50 |
| 50 0,305 100 | 0.312 | 11/2 | 2 | 0 |
| | | 18/4 | 0 | |
| Burning Rate: cm/sec | | Bomb Drop Test: | | |
| Thermal Conductivity: col/sec/cm/"C | | T7, 2000-Ib Semi-Arr | nor-Piercing I | Bomb vs Concrete: |
| Coefficient of Expansion: | | Max Safe Drop, ft | | |
| Linear, %/°C | | 500-1b General Purpo | No Seal | Concrete: Seal |
| Volume, %/°C | | Height, ft | 4000 | 4000 |
| | | Trials | 65 | 39 |
| Hardness, Mohs' Scale: | | Unaffected | 58 | 36 |
| | | Low Order | 2 | 2 |
| Young's Modulus: E', dynes/cm² | | High Order | 5 | 1 |
| E, lb/inch ² | | 1000-lb General Purp | ose Bomb vs | Concrete: |
| Density, gm/cc | | | | |
| | | Height, ft | | |
| Compressive Strength: Ib/inch ² (b) | 1610-2580 | Trials | | |
| Density, gm/cc | 1.68 | Unaffected | | |
| Vapor Pressure: | | Low Order | | |
| "C mm Mercury | | High Order | | |
| | | | | |
| | | | | |
| | | | | |

Composition_B

| Fragmentation Test: | | Shaped Charge Effectiveness, TNT = 100: |
|--|--------------|---|
| 90 mm HE, M71 Projectile, Lot | MC-91. | (g) (h) Glass Cones Steel Cones |
| N2 | 1.65 | Hole Volume 178 162 |
| De n sity, gm/cc Charge Wt, Ib | 2.187 | Hole Depth 125 148 |
| Charge Wi, 10 | 2.107 | |
| Total No. of Fragments: | | |
| For TNT | 703 | Color: Yellow-brown |
| For Subject HE | 998 | |
| 3 inch HE, M42A1 Projectile, Lo | N+ KC-5. | Principal Uses: Fragmentation bombs, HE projectiles, grenades, shaped |
| Density, gm/cc | 1.67 | charges |
| Charge Wt, Ib | 0.882 | |
| | 0.002 | |
| Total No. of Fragments: | | Method of Loading: Cast |
| For TNT | 514 | Method of Loading. |
| For Subject HE | 701 | |
| | | Loading Density: gm/cc 1.68 |
| Fragment Velocity: ft/sec | | |
| At 9 ft At 25½ ft | 2940 | Storage: |
| Density, gm/cc | 2680 1.68 | Giorage. |
| Donsky, grif de | 1.00 | Method Dry |
| | | |
| Blast (Relative to TNT); | (f) | Hozord Class (Quantity-Distance) Class 9 |
| Air: | | Compatibility Group Group I |
| Peak Pressure | 110 | croup in a croup i |
| Impulse | 110 | Exudation Very slight when stored at 71°C |
| Energy | 116 | |
| | | Origin: |
| Air, Confined: | 75 | |
| Impulse | 75 | RDX Composition B was developed by the British between World War I and World War 11. |
| Under Water: | | It was standardized by the United States |
| Peak Pressure | 110 | early in World War 11. |
| Impulse | 108 | Effect of Temperature on |
| Energy | 121 | Rate of Detonation: (i) |
| Underground: | | 16 hrs at, ^o C -54 24 |
| Peak Pressure | 104 | Density, gm/cc 1.69 1.69 |
| Impulse | 97 | Rate, m/sec 7720 7660 |
| Energy | - | Bulk Modulus a t Room (j) Temperature (25°-30°C): |
| Crater radius cubed | 107 | |
| | | % Wax in Comp B 1 2 3 Dynes/cm ² x 10 ⁻¹⁰ 5.10 3.56 2.34 |
| | | Density, gm/cc 1.72 1.70 1.68 |
| | | Viscosity, poises: |
| | | Temp, 83°C 3.1 95°C 2.7 |

Compatibility with Metals:

Dry - Magnesium, aluminum, magnesium-aluminum alloy, mild steel, stainless steel, mild steel coated with acid-proof black paint and mild steel plated with zinc or nickel are unaffected. Copper, brass and mild steel plated with copper or cadmium are slightly affected.

Wet - Aluminum and stainless steel are unaffected. Copper, brass, mild steel, mild steel coated with acid-proof black paint and mild steel plated with cadmium, copper, nickel or zinc are slightly affected. Magnesium and magnesium-aluminum alloy are more heavily affected.

Preparation:

Water wet RDX is added slowly with stirring to molten TNT melted in a steam-jacketed kettle at a temperature of 100° C. Some water is poured off and heating and stirring are continued until all moisture is evaporated. Wax is then added and when thoroughly mixed, the composition is cooled to a satisfactory pouring temperature. It is cast directly into ammunition components or in the form of chips when Composition B is to be stored.

Destruction by Chemical Decomposition:

RDX Composition B is decomposed in 12 parts by weight of technical grade acetone heated to 45° C. While this is stirred vigorously, there is added 12 parts of a solution, heated to 70° C, of 1 part sodium sulfide (Na₂S·9H₂O) in 4 parts water. The sulfide solution is added slowly so that the temperature of the acetone solution does not rise above 60° C. After addition is complete, stirring is continued for one-half hour.

References:¹⁰

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III - Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, <u>OSRD Report No. 5746</u>, 27 December 1945.

(b) Philip C. Keenan and Dorothy Pipes, <u>Table of Military High Explosives</u>, Second Revision, NAVORD Report No. 87-46, 26 July 1946.

(c) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(d) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute for</u> <u>Tetryl in Boosters</u>, NOL Mano 10,303, 15 June 1949.

(e) Committee of Divisions 2 and 8, NDRC, <u>Report on HBX and Tritonal</u>, OSRD Report No. 5406, 31 July 1945.

(f) W. R. Tomlinson, Jr., <u>Blast Effects of Bomb Explosives</u>, PA Tech Div Lecture, 9 April 1948.

(g) Eastern Laboratory, du Pont, Investigation of Cavity Effect, Sec 111, Variation of Cavity Effect with Explosive Composition, NDRC Contract W672-ORD-5723.

(h) Eastern Laboratory du Pont, <u>Investigation of Cavity Effect</u>, Final Report, E Lab du Pont, Contract W-672-ORD-5723, 18 September 1943.

(i) W. F. McGarry and T. W. Stevens, Detonation Rates of the More Important Military Explosives at Several Different Temperatures, PAIR No. 2383, November, 1956.

¹⁰See footnote 1, page 10.

Composition B

(j) W. S. Cramer, <u>Bulk Compressibility Data on Several High Explosives</u>, NAVORD Report No. 4380, 15 September 1956.

| (k) | Also see th | e followi | ng Picati | nny Arsei | nal Techn | ical Repo | rts on RDX | Composi | tion B: |
|--------------------------------------|------------------------------|----------------------|--|--------------------------------------|--|--|--|--|--------------------------------------|
| <u>o</u> | <u>1</u> | 2 | <u>3</u> | <u>4</u> | <u>5</u> | <u>6</u> | <u>7</u> | 8 | 2 |
| 1360 1530 2100 2160 2190 | 1211 1451 2131 2151 | 1402 1482 1592 | 1313 1433 1803 1983 2053 2063 2103 2233 | 1224 1424 1944 2004 2104 | 1325 1435 1585 1595 1865 1885 2125 2125 2-75 2-35 | 1466 1476 1556 1756 1956 2236 | 1207 1437 1457 1737 1797 2007 2147 | 1338 1388 1438 1458 1688 1728 1828 1838 1978 2008 2138 2168 | 1339 1379 1469 1819 2019 |

(1) C. Lenchitz, W. Beach and R. Valicky, <u>Enthalpy Changes. Heat of Fusion and Specific Heat</u> of Basic Explosives, PAIR No. 2504, January 1959.

Composition B. Desensitized

| Composition: | <u></u> * | II** | Molecular Weight: | <u>I*</u> | <u>II**</u> See Comp B |
|---|-----------------------------|-------------------------|---|-------------------------------------|---------------------------|
| % RDX TNT Wax, added, (Stamoulind or Aristowax, 1650/ | 60 40 5 | 55.2 40.0 | Oxygen Balance: CO, % See | Cyclonite Cyclonite Cyclonite | |
| 1700F) Vinylseal (MA28-14), | 2 | | Density: gm/cc Cast | 1.65 | 1.65 |
| added Vistanex (B120) Albacer Wax | 2 | 1.2 3.6 | Melting Point: "C | | |
| C/H Ratio | | | Freezing Point: °C | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | <u>I*</u> 95 14 17 | <u>II**</u> 13 16 | Boiling Point: °C Refractive Index, n ^D ₂₀ n ^D ₂₃ n ^D ₃₀ | | |
| Friction Pendulum Test: | | | Vacuum Stability Test: | <u></u> | II** |
| Steel Shoe Un affect | | | cc/40 Hrs, at | <u></u> | |
| Fiber Shoe Un affect | ted | | 90°C 100°C | | |
| Rifle Bullet Impact Test: Trials | | | 120°C | 0,99 | 0.92 |
| % Explosions | $\frac{I*}{0}$ | $\frac{11^{**}}{0}$ | 135°C | | |
| Partiols | 0 | 0 | 150°C | 11+ | 11+ |
| Burned | 5 | 0 | 200 Gram Bomb Sand Test: | <u>I*</u> | <u>II**</u> |
| Unaffected | 95 | 100 | Sand, gm | 52.7 | 55.0 |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) 1 | Τ | <u> </u> | Sensitivity to Initiation: Minimum Detonating Char Mercury Fulminote | <u>⊥*</u> rge, gm | <u> </u> |
| 5 Decomposes 10 | 260 | 270 | Lead Azide Tetryl | 0.22 | 0.26 |
| 15 20 | | | Ballistic Mortar, % TNT: | | |
| | | | Trauzi Test, % TNT: | | |
| 75°C International HeatTest: % Loss in 48 Hrs | | | Plate Dent Test: Method | | |
| 100°C Heat Test: | <u>I*</u> | II** | Condition | | |
| % Loss, 1st 48 Hrs | 0.05 | 0.12 | Confined | | |
| % Loss, 2nd 48 Hrs | 0.19 | 0.18 | Density, gm/cc Brisance, % TNT | | |
| Explosion in 100 Hrs | None | None | | | |
| Flammability Index: | | | Detonation Rate: Confinement Condition | | |
| Hygroscopicity: % 30 ⁰ C, 90% RH | 0.00 | 0.00 | Charge Diameter, in. | | |
| Volatility: | Ni 1 | 0.00 Ni 1 | Density, gm/cc Rate, meters/second | | |

*Desensitized Comp B, designated I, uses emulsified wax. **Desensitized Comp B, designated 11, uses coated RDX.

| Fragmentation Test: | | | Shaped Charge | e Effectivene | ess, TNT $= 1$ | 00: |
|---|-------------------------|---------------------|--|-----------------|-------------------------|-----------------------------|
| 90 mm HE, M71 Projectile, Lo Density, gm/cc Charge Wt, Ib | ot WC-91: | | Hole Volum Hole Depth | Glass Cor le | nes Steel (| Cones |
| Total No. of Fragments: For TNT | | | Color: | | Yellow- | brown |
| For Subject HE 3 inch HE, M42A1 Projectile, Density, gm/cc | Lot KC-5: I* I-65 | <u>11**</u> 1.65 | Principal Uses | :: | Bombs | |
| Charge Wt, Ib | 0.87 | 0.86 | | | | |
| Total No. of Fragments: For TNT | 514 609 | 514 659 | Method of Lo | ading: | Cast | |
| For Subject HE | 009 | | Loading Densi | ity: gm/cc | 1.65 | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | | | Storage: | | | |
| Density, gm/cc | | | Method | | | Dry |
| Blast (Relative to TNT): | | | Hazard Cla | ss (Quantity- | Distance) | Class 9 |
| Air: Peak Pressure | | | Compatibili | ity Group | | Group I |
| Impulse Energy | | | Exudation | | | |
| Air, Confined: Impulse | | | Viscosity, Temp, 83 ⁰ 95 ⁰ | ^о с | <u>I*</u> 3.5 2.6 | |
| Under Water: Peak Pressure | | | References: | | 2.0 | |
| Impulse Energy | | | (a) See Technical I Desensitize | Reports on | wing Picat RDX Comp | inny Arsenal position B, |
| Underground : Peak Pressure | | | <u>1</u> | <u>3</u> | <u>5</u> | <u>6</u> |
| Impulse Energy | | | 2151 | 1313 2053 | 1435 1865 | 1756 |
| *Desensitized Comp B, desi emulsified wax. **Desensitized Comp B, desi coated RDX. | - | | | | | |

| Composition: % | Molecular Weight: | | | | |
|--|--|--|--|--|--|
| RDX 88.3 Plasticizer, non- | Oxygen Balance: CO, % CO % | | | | |
| explosive 11.7* | Density: gm/cc | | | | |
| *Nonexplosive oily plasticizer containing 0.6%lecithin. | Melting Point: "C | | | | |
| C/H Ratio | Freezing Point: °C | | | | |
| Impact Sensitivity, 2 Kg Wt : Bureau of Mines Apparatus, cm 100+ | Boiling Point: "C | | | | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | | | | |
| Friction Pendulum Test: | Vacuum Stability Test: | | | | |
| Steel Shoe | cc/40 Hrs, at 90°C | | | | |
| Fiber Shoe | 100°C 0.3 | | | | |
| Rifle Bullet Impact Test: Trials | 120°C 0.7 | | | | |
| Explosions 0 | 135°C | | | | |
| Partials 0 | 150°C | | | | |
| Burned 0 Unaffected 100 | 200 Gram Bomb Sand Test: Sand, gm 46.5 | | | | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate | | | | |
| 5 Decomposes 285 | Lead Azide 0.25 | | | | |
| 10 | Tetryl 0.11 | | | | |
| 15 20 | Ballistic Mortar, % TNT: (a) 120 | | | | |
| | Trauzl Test, % TNT: | | | | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method A | | | | |
| 100°C Heat Test: | Condition Hand Tamped | | | | |
| % Loss, 1st 48 Hrs 0.04 | Confined Yes | | | | |
| % Loss, 2nd 48 Hrs 0.00 | Density, gm/cc 1.58 Brisance, % TNT 112 | | | | |
| Explosion in 100 Hrs None | | | | | |
| Flammability Index: | Detonation Rate: Confinement | | | | |
| Hygroscopicity: % 30 ⁰ C, 95% RH 0.25 | Condition Charge Diameter, in. | | | | |
| Volatility: 25 ^o C, 5 days 0.00 | Density, gm/cc Rate, meters/second | | | | |

Composition C

| Fragmentation Test: | Shaped Charge Effectiveness, TNT = 100: (f) (g) |
|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: | Glass Cones Steel Cones |
| Density, gm/cc | Hole Volume 113 114 |
| Charge Wt, Ib | Hole Depth 101 114 |
| - · · · | |
| Total No. of Fragments: | Color: White |
| For TNT | |
| For Subject HE | Principal Uses: Plastic demolition explosive |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | , |
| Density, gm/cc | |
| Charge Wt, Ib | |
| | |
| Total No. of Fragments: | Method of Loading: Hand tamped |
| For TNT | |
| For Subject HE | |
| | Loading Density: gm/cc 1.49 |
| Fragment Velocity: ft/sec | |
| At 9 ft At 2 5½ ft | Storage: |
| Density, gm/cc | |
| | Method Dry |
| Plact (Polotive to TNT) | Hazard Class (Quantity-Distance) Class 9 |
| Blast (Relative to TNT): | |
| Air: | Compatibility Group Group I |
| Peak Pressure | |
| Impulse | Exudation Exudes above 40 ⁰ C |
| Energy | |
| Air, Confined: | Plasticity: |
| Impulse | Below 0 ^o C Brittle (0 ^o C) |
| | 0-40°C Plastic |
| Under Water: Peak Pressure | Above 40 [°] C Exudes (40°C) |
| Impulse | References : |
| Energy | |
| | See references for Composition C-4. |
| Underground: | |
| Peak Pressure | |
| Impulse - | |
| Energy | |
| | |
| | |
| | |
| | |
| | |

| Composition: | | Molecular Weight: | | | | |
|--|------|--|----------------------------|--|--|--|
| % RDX 78.7 TNT 5.0 DNT 12.0 | | Oxygen Balance: CO, % CO % | | | | |
| MNT 2.7 NC 0.6 | | Density: gm/cc | | | | |
| Solvent 1.0 | | Melting Point: °C | | | | |
| C/H Ratio | | Freezing Point: °C | | | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | 90 | Boiling Point: °C | | | | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 50 | Refractive Index, n ^o ₂₀ n ^o 25 n ^o 30 | | | | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | | Vacuum Stability Test: cc/40 Hrs, at 90°C | 2.0 | | | |
| Rifle Bullet Impact Test: Trials % Explosions 0 Partigls 20 | | - 100°C 120°C 135°C 150°C | 2.0 9.0 | | | |
| Burned 0 Unaffected 80 | | 200 Gram Bomb Sand Test: Sand, gm | 47.5 | | | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Decomposes 285 10 | | Sensitivity to Initiation: Minimum Detonating Cl Mercury Fulminote Lead Azide Tetryl | harge, gm 0.25 0.10 | | | |
| 15 20 | | Ballistic Mortar, % TNT: | | | | |
| | | Trauzl Test, % TNT: | | | | |
| 75°C International Heat Test: % Loss in 48 Hrs | | Plate Dent Test: Method | (c) B | | | |
| 100°C Heat Test: | | Condition | Hand tamped | | | |
| % Loss, 1st 48 Hrs | 1.8 | Confined Density, gm/cc | No 1.52 | | | |
| % Loss, 2nd 48 Hrs | 1.4 | Brisance, % TNT | 111 | | | |
| Explosion in 100 Hrs | None | | | | | |
| Flammability Index: | 178 | Detonation Rate: Confinement Condition | (d) None Hand tamped | | | |
| Hygroscopicity: % 30 ⁰ C,95% RH | 0.55 | Charge Diameter, in. | 1.0 | | | |
| Volatility: 25°C, 5 days | 0.00 | Density, gm/cc Rate, meters/second | 1.57 7660 | | | |

| Fragmentation Test: | Shaped Charge Effectiveness, TNT $=$ 100: |
|---|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: White |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib Total No. of Fragments: For TNT | Principal Uses: Plastic demolition explosive Method of Loading: Hand tamped |
| For Subject HE | Loading Density: gm/cc 1.57 |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc | Storage: |
| | Method Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 |
| Air: Peak Pressure Impulse Energy | Compatibility Group Group I Exudation Volatilizes above 52 ⁰ C |
| Air, Confined: Impulse Under Water: Peak Pressure impulse Energy Underground: Peak Pressure Impulse Energy | Plasticity: Below 0°C Plastic (-30°C) 0-40°C Plastic above 40°C Hard (52°C)* *Due to volitalization of plasticizer. References: See references for Composition C-4. |
| | |

| Composition: | Molecular Weight: |
|---|---|
| HDX 77 Tetryl 3 TNT 4 | Oxygen Balance: CO, % CO % |
| DNT 10 MNT 5 | Density: gm/cc |
| NC J | Melting Point: °C |
| C/H Ratio | Freezing Point: °C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 100+ | Boiling Point: °C |
| Sample Wt 20 mg | Refractive Index, n ^D ₂₀ |
| Picatinny Arsenal Apparatus, in. 14 Sample Wt, mg 33 | |
| | n ^D 30 |
| Friction Pendulum Test: | Vacuum Stability Test: |
| Steel Shoe Unaffected | cc/40 Hrs, at |
| Fiber Shoe Unaffected | 90°C 100°C 1.21 |
| Rifle Bullet Impact Test: Trials | 100°C 1.21 120°C 11+ |
| 9/0 | 135°C |
| Explosions 0 | 150°C |
| Particils 40 | |
| Burned 0 | 200 Gram Bomb Sand Test: |
| Unaffected 60 | Sand, gm 53-1 |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) | Sensitivity to Initiation: Minimum Detonating Charge, gm |
| 1 | Mercury Fulminote |
| 5 Decomposes 280 | Lead Azide 0.20 |
| 10 | Tetryl 0.08 |
| 15 20 | Ballistic Mortar, % TNT: (a) 126 |
| | Trauzi Test, % TNT: (b) 117 |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: (c) |
| | Method B Condition Hand tamped |
| 100°C Heat Test: | |
| % Loss, 1st 48 Hrs 3.20 | Confined NO Density, gm/cc 1.57 |
| % Loss, 2nd 48 Hrs 1.63 | Brisance, % TNT 118 |
| Explosion in 100 Hrs None | |
| Flammability Index: | Detonation Rate: (d) Confinement None |
| | Condition Hand tamped |
| Hygroscopicity: % 30 ⁰ C, 95% RH 2.4 | Charge Diameter, in. 1.0 |
| | Density, gm/cc 1.60 |
| Volatility: 25°C, 5 days 1.15 | Rate, meters/second 7625 |

| Fragmentation Test: | | Shaped Charge Effectiveness, $TNT = 100$: | | | | |
|---|--|---|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot Density, gm/cc Charge Wt, lb | WC-91 : 158 2045 | Glass Cones Steel Cones Hole Volume Hole Depth | | | | |
| Total No. of Fragments: For TNT For Subject HE | 70 3 944 | Color: Yellow Principal Uses: Plastic demolition explosive | | | | |
| 3 inch HE, M42A1 Projectile, Lo Density, gm/cc Charge <i>Wt,</i> lb | ot KC-5 : 1.60 0 . 842 | Principal Uses: Plastic demolition explosive | | | | |
| To tal N o. o f Fragments : For TNT For Subject HE | 514 671 | Method of Loading: Hand tamped | | | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc | | Loading Density: gm/cc 1.58 Storage: Method Dry | | | | |
| Blast (Relative to TNT): | | Hazard Class (Quantity-Distance) Class 9 Compatibility Group Group I | | | | |
| Peak Pressure Impulse Energy | 105 109 | Exudation Exudes a t 77°C | | | | |
| Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | | Plasticity:Below 0°CHard (-29°C)0-40°CPlasticAbove 40°CExudes (77°C)Booster Sensitivity Test:(h)ConditionPressedTetryl, gm100Wax, in. for 50%DetonationDensity, gm/cc1.62References:See references for Composition c-4. | | | | |

| Composition: % | | Molecular Weight: | | | | |
|--|------------------------------------|--|--------------------|--|--|--|
| RDX | 91 | Oxygen Balance: CO, % | | | | |
| Plasticizer, non- explosive 9* | | CO % Density: gm/cc | | | | |
| * Contains polyisobutylene 2.1 1.6% and di(2-ethylhexyl) | 1%; motor oil sebacate 5.3%. | Melting Point: °C | | | | |
| C/H Ratio | | Freezing Point: "C | | | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | 100+ | Boiling Point: "C | | | | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 19 27 | Refractive Index, n ^o ₂₀ n ^b 25 n ^D 30 | | | | |
| Friction Pendulum Test: | | Vacuum Stability Test: | | | | |
| Steel Shoe Unaffe | cted | cc/40 Hrs, at | | | | |
| Fiber Shoe Unaffe | cted | 90°C | | | | |
| Rifle Bullet Impact Test: Trials | | 100°C | 0.26 | | | |
| · | | 120°C | | | | |
| 80 Explosions 0 | | 135°C | | | | |
| Particils 0 | | 150°C | | | | |
| Burned 20 | | 200 Gram Bomb Sand Test: | | | | |
| Unaffected 80 | | Sand, gm | 55.7 | | | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) | | Sensitivity to Initiation: Minimum Detonating Ct | narge, gm | | | |
| 1 | | Mercury Fulminate | | | | |
| 5 290 | | Lead Azide | 0.20 | | | |
| 10 | | Tetryl | 0.10 | | | |
| 15 | | | (a) 130 | | | |
| 20 | | Ballistic Mortar, % TNT: | (a) 130 | | | |
| 75°C International Heat Test: | | Trauzl Test, % TNT: | | | | |
| % Loss in 48 Hrs | | Plate Dent Test: Method | (c) B | | | |
| 100°C Heat Test: | | Condition | Hand tamped | | | |
| % Loss, 1st 48 Hrs | 0.13 | Confined | No | | | |
| % Loss, 2nd 48 Hrs | 0.00 | Density, gm/cc | 1.60 | | | |
| Explosion in 100 Hrs | None | Brisance, % TNT | 115 | | | |
| Flammability Index: | | Detonation Rate: Confinement | (d) None | | | |
| | | Condition | Hand tamped | | | |
| | Hygroscopicity: % 30°C, 95% RH Nil | | | | | |
| Hygroscopicity: % 30°C, 95% RH | Nil | Charge Diameter, in. | 1.0 | | | |
| Hygroscopicity: % 30°C, 95% RH | Nil | Charge Diameter, in. | 1.0 1.59 | | | |

| Fragmentation Test: | Shaped Charge Effectiveness, TNT $=$ 100: |
|---|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm∕cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: Light brown |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Plastic demolition explosive |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Hand tamped |
| Fragment Velocity: ft/sec At 9 ft | Loading Density: gm/cc 1.60 |
| At 25½ ft Density, gm/cc | Storage: Method Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) $Class$ 9 |
| Air: Peak Pressure Impulse Energy | Compatibility Group Group I Exudation None at 77 ⁰ C |
| Air, Confined: Impulse | Effect of Temperature on (i) Rate of Detonation: |
| Under Water: Peak Pressure Impulse Energy | 16 hrs at, °C -54 21 Density, gm/ee 1.36 1.35 Rate, m/sec 7020 7040 Plasticity: 1 1 |
| Underground: Peak Pressure Impulse Energy | Below 0 ^o C Plastic (-57 ^o C) 0-40 ^o C Plastic Above 40 ^o C Plastic (77 ^o C) |
| | |

-

Preparation:

In manufacturing Composition C-3, the mixed plasticizing agent is heated in a melting kettle at 100°C. Water-wet RDX is added and heating and stirring are continued until all the water is evaporated. This mixture is then cooled and hand pressed into demolition blocks or special item ammunition.

Composition C-4 is prepared by hand kneading and rolling, or in a Schrader Bowl mixer, RDX of 144 micron size or less with the polyisobutylene-plasticizer previously made up in ether. The thoroughly blended explosive is dried in air at 60° C and loosely packed by hand tamping to its maximum density.

Origin:

Developed by the British during World War II as a plastic explosive which could be hand shaped. It was standardized in the United States during World War II and subsequent development led. to mixtures designated C-2, C-3 and C-4.

Destruction by Chemical Decomposition:

Composition C-3 is decomposed by adding it slowly to a solution composed of 11/4 parts sodium hydroxide, 11 parts water, and 4 parts 95% alcohol, heated to 50°C. After addition of Composition C-3 is complete, the solution is heated to 80°C and maintained at this temperature for 15 minutes.

References: 11

(a) Committee of Div 2 and 8, NDRC, <u>Report on HBX and Tritonal</u>, OSRD No. 5406, 31 July 1945.

(b) Philip C. Keenan and Dorothy Pipes, <u>Table of Military High Explosives</u>, Second Revision, NAVORD Report No. 87-46, 26 July 1946.

(c) D. P. MacDougall, <u>Methods of Physical Testing</u>, OSRD Report No. 803, 11 August 1942.

L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III - Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, OSRD Report No. 5746, 27 December 1945.

(d) G. H. Messerly, The Rate of Detonation of Various Explosive Compounds, OSRD Report No. 1219, 22 February 1943.

M. D. Hurwitz, <u>The Rate of Detonation of Various Compounds and Mixtures</u>, OSRD Report No. 5611, 15 January 1946.

(e) W. R. Tomlinson, Jr., <u>Blast Effects of Bomb Explosives</u>, PA Tech Div Lecture, 9 April 1948.

(f) Eastern Laboratory, du Pont, <u>Investigation of Cavity Effect</u>, <u>Sec III</u>, <u>Variation of Cavi-</u> ty Effect with Explosive Composition, NDRC Contract W672-ORD-5723.

(g) Eastern Laboratory, du Pont, <u>Investigation of Cavity Effect</u>, Final Report, 18 September 1943, NDRC Contract W-672-ORD-5723.

(h) L. C. Smith and S. R. Walton, <u>4 Consideration of RDX/Wax Mixtures as a Substitute for</u> <u>Tetryl in Boosters</u>, NOL Mamo 10, 303, 15 June 1949.

¹See footnote 1, page 10.

Compositions C, C-2, C-3, C-4

(i) W. F. McGarry and T. W. Stevens, <u>Detonation Rates of the More Important Military Explo-</u> sives at Several Temperatures, PATR No. 2383, November 1956.

(j) Also see the following Picatinny Arsenal Technical Reports on RDX Composition C:

| | <u>0</u> | <u>1</u> | <u>3</u> | <u>4</u> | 2 | <u>6</u> | <u>7</u> | <u>8</u> | <u>9</u> |
|----------------------|----------|----------|--------------|----------|----------------------|------------------------------|----------|----------------------|----------|
| Comp C | 1260 | | 1293 | | | | | 1518 1838 | |
| Comp C-2 Comp C-3 | | 1611 | 1293 1713 | 2154 | 1595 1695 1885 | 1416 1416 1556 1766 | 1797 | 1518 1518 2028 | |
| Comp C-4 | | | | | | 1766 | 1907 | 1828 1958 | 1819 |

| Coyorition: | Molecular Weight: (CuC ₂ N ₈ Cl ₂) 271 | | |
|--|---|--|--|
| C 8.9 N N N CCL N 41.5 N N N N | Oxygen Balance: CO, % -30 CO % -18 | | |
| 26.2 N _ N | Density: gm/cc 2.04 | | |
| | Melting Point: "C | | |
| C/H Ratio | Freezing Point: "C | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | Boiling Point: °C Refractive Index, n ^D ₂₀ | | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 1; (1 1b wt) <i>3</i> Sample Wt, mg 9 | n ₂₅ n ₃₀ | | |
| Friction Pendulum Test: Steel Shoe Exploded Fiber Shoe Exploded | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C 120°C 135°C 150°C | | |
| Rifle Bullet Impact Test: Trials % Explosions Partials | | | |
| Burned Unaffected | 200 Gram Bomb Sand Test: (f) Sond, gm 27.4 25.3 Black powder fuse 17.0 | | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 305 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide 0.20 0•30 Tetryl 0.10 | | |
| 15 20 | Ballistic Mortar, % TNT: | | |
| 75°C International Heat Test: % Loss in 48 Hrs | Trauzl Test, % TNT: Plate Dent Test: Method | | |
| 100°C Heat Test: % Loss, 1st 48 Hrs 2.67 % Loss, 2nd 48 Hrs 0.10 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT | | |
| Flammability Index: | Detonation Rate: Confinement | | |
| Hygroscopicity: % 30°C, 90% RH 3.11 | Condition Charge Diameter, in. | | |
| Volatility: | Density, gm/cc Rate, meters/second | | |

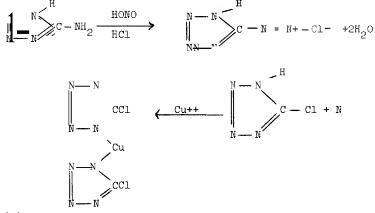
Copper Chlorotetrazole

| Fragmentation Test: | Shaped Charge Effectiveness, TNT $=$ 100: |
|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: | Glass Cones Steel Cones |
| Density, gm/cc | Hole Volume |
| Charge Wt, Ib | Hole Depth |
| Total No. of Fragments: | Color: Blue |
| For TNT | |
| For Subject HE | Principal Uses: Primary explosive |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | |
| Density, gm/cc | |
| Charge Wt, Ib | |
| Total No. of Fragments: | Method of Loading: Pressed |
| ForTNT | |
| For Subject HE | Loading Density: cm/cc $psi \times 10^3$ (c) |
| | Loading Density: gm/cc 10 20 40 70 |
| Fragment Velocity: ft/sec | 1.49 1.63 1.74 1.86 |
| At 9 ft At 25½ ft | Storage: |
| Density, gm/cc | Method Wat |
| | Method Wa |
| Blost (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 |
| Air: | Compatibility Group Group M |
| Peak Pressure | |
| Impulse | Exudation None |
| Energy | |
| Air, Confined: | <u>Stab Sensitivity:</u> (c) |
| Impulse | Density Firing Point (inch-ounces) |
| Under Water: | <u>gm/cc 0% 50% 100%</u> |
| Peak Pressure | 1.49 9 11 ¹⁵ |
| Impulse | 1.63 8.5 io 12 |
| Energy | 1.74 6 7 9 1.86 4 5 6 |
| Underground: | Heat of": |
| Peak Pressure | |
| Impulse | Explosion, cal/gm 432 |
| Energy | <u>Specific Heat, cal/gm/⁰C</u> |
| | Temp range 0° - 30° C 0.155 |
| | Wt of sample, gn 0.8910 |
| | |
| | |

Copper Chlorotetrazole

Preparation: (a)

Five grams of 5-aminotetrazole are dissolved in a mixture of 200 ml of water and 70 ml of concentrated HCl. Enough kerosene or nujol (which gives a slightly cleaner product) is added to provide a layer of oil approximately $1/4^{"}$ thick on the surface. With only moderate stirring and external cooling to 10° - 15° C, a solution of 5 grams of sodium nitrite in 70 cc of water is added rapidly by means of a burette extending below the oil layer. Immediately after this addition, a solution of 5 gms of cupric chloride in a minimum amount of water is added all at once, and stirring is continued for about 1 hour. The reaction mixture is allowed to stand for a few minutes till the bright blue copper salt separates. The oil is removed by decantation and may be reused. The salt is filtered; washed with water, alcohol, and ether; and dried - giving a yield of 6 grams or 74%.



Origin:

The copper salt of 5-chlorotetrazole was first described in 1929 by R. Stolle' (with E. Schick, F. Henke-Stark and L. Krauss) who prepared the compound by reaction of the diazonium chloride of 5-aminotetrazole with copper chloride (Ber $\underline{62}A$, 1123).

References: 12

(a) R. J. Gaughran and J. V. R. Kaufman, <u>Synthesis and Properties of Halotetrazole Salts</u>, PATR No. 2136, February 1955.

(b) A. M. Anzalone, J. E. Abel and A. C. Forsyth, <u>Characteristics of Explosive Substances</u> for Application in Ammunition, PATR No. 2179, May 1955.

(c) A. C. Forsyth, Pfc, S. Krasner and R. J. Gaughran, <u>Development of Optimum Explosive</u> <u>Trains. An Investigation Concerning Stab Sensitivity versus Loading Density of Some Initiating</u> <u>Compounds</u>, PAIR No. 2146, February 1955.

¹²See footnote 1, page 10.

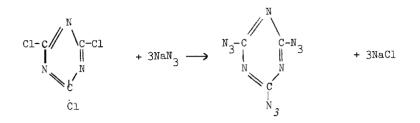
| Composition: % | Molecular Weight: (C ₃ N ₁₂) 204 | |
|---|--|--|
| c 17.6 N_3 N 82.4 | Oxygen Balance: -47.1 CO, % -23.5 | |
| N N | Density: gm/cc Crystal 1.54 | |
| | Melting Point: °C 94 | |
| C/H Ratio | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm $$ 1 kg wt $$ 7 | Boiling Point: "C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in Sample Wt, mg _ | Refractive Index, n₂₀ n₂₅ n₃₀ | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C | |
| Rifle Bullet Impact Test: Trials % Explosions Partiols | 120°C 135°C 150°C | |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm 32.2 | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 252 1 5 10 15 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate - Lead Azide 0.20 Tetryl 0.10 | |
| 20 | Ballistic Mortar, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | Trauzi Test, % TNT: Plate Dent Test: Method | |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement - | |
| Hygroscopicity: % | Condition - Charge Diameter, in. 0.3 | |
| Volatility: Decomposes above 100 ⁰ C | Density, gm/cc 1.15 Rate, meters/second 5550-5600 | |

| | Shanad Charge Effectiveness T | NT 400 |
|--|--|----------------------|
| Fragmentation Test: | Shaped Charge Effectiveness, T | NT == 100; |
| 90 mm HE, M71 Projectile, Lot WC-91: | Glass Cones | Steel Cones |
| Density, gm/cc | Hole Volume | |
| Charge Wt, Ib | Hole Depth | |
| Total No. of Fragments: | Color: | Colorless |
| For TNT | | |
| For Subject HE | Principal Uses: Not used by | ecause of difficulty |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | in control | ling sensitivity. |
| Density, gm/cc | | |
| Charge Wi, Ib | | |
| Total No. of Fragments: | Method of Loading: | Pressed |
| For TNT | | |
| For Subject HE | | |
| | Loading Density: gm/cc At 200 atmospheres | 1.4 |
| Fragment Velocity: ft/sec | At 800 atmospheres | 1.5 |
| At 9 ft At 25½ ft | Storage: | |
| Density, gm/cc | | |
| | Method | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Dista | nce) Class 9 |
| Air: | Compatibility Group | |
| Peak Pressure | | |
| Impulse | Exudation | None |
| Energy | | |
| Air, Confined: | | |
| Impulse | | |
| Under Water: Peak Pressure | | |
| Impulse | | |
| Energy | | |
| Underground: Peak Pressure | | |
| Impulse | | |
| Energy | | |
| | | |
| | | |
| | | |
| | | |
| | | |

Cyanuric Triazide

Preparation:

By the reaction of cyanuric chloride with an aqueous solution of sodium azide:



Recrystallization should be avoided as it leads to very large crystals which explode when broken.

Origin:

Cyanuric Triazide was prepared in 1847 by Cahours from chlorine and methyl cyanate. Later James improved the process (JCS 51, 268 (1887) and in 1921 E. Ott patented the preparation from cyanuric chloride and sodium azide (Ref b) Taylor and Rinkenbach prepared cyanuric triazide in a pure state and determined its properties (Ref c).

Initiating Efficiency:

Reported to be more efficient than lead azide. Capable of initiating Explosive D.

Solubility:

Insoluble in water; readily soluble in hot ethanol, acetone, benzene, and ether.

Heat of:

Formation, cal/gm -1090 to -1138

References: ¹³

(a) A. H. Blatt, <u>Compilation of Data on Organic Explosives</u>, OSRD Report No. 2014, 29 February 1944.

- (b) Ott and Ohse, Ber <u>54</u>, 179 (1921).
- (c) Taylor and Rinkenbach, Bureau of Mines, RI 2513 (1923).

Taylor and Rinkenbach, J Frank Inst 204, 369 (1927).

¹³See footnote 1, page 10.

| Composition: CH2 | | Moleculor Weight: $(C_3H_6N_6O_6)$ | 222 |
|--|----------------|--|--------------|
| 16.3 $0_2 N - N N - 1_2 C C H_2$ | | Oxygen Bolance: CO % CO % | -22 0.0 |
| N 37.8 N | | Density: gm/cc Crystal | 1.82 |
| $ \begin{array}{c} $ | | Melting Point: °C | 204 |
| C/H Ratio 0.095 | | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: | 32 | Boiling Point: "C | |
| Bureau of Mines Apparatus, cm Sample Wt 20 mg | - | Refractive Index, $\mathbf{n}_{20}^{\mathbf{D}}$ | |
| Picatinny Arsenal Apparatus, in. | 8 18 | n ₂₅ | |
| Sample Wt, mg | 10 | n ⁰ ₃₀ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| Steel Shoe Explode | | cc/40 Hrs, at 90°C | |
| Fiber Shoe Unaffec | ted | 90°C 100°C | 0.7 |
| Rifle Bullet Impact Test: Trials | | 100°C 120°C | 0.9 |
| Kine Bullet Impact Test. Mais | | | 0.9 |
| Explosions 100 | | 135°C 150°C | 2.5 |
| Partials 0 | | | 2) |
| Burned 0 | | 200 Gram Bomb Sand Test: | ()) |
| Unaffected 0 | | Sand, gm | 60.2 |
| Explosion Temperature: °C | | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) 405 | | Minimum Detonating Charge, gm | |
| 1 316 | | Mercury Fulminate | 0.19* |
| 5 Decomposes 260 | | Lead Azide | 0.05* |
| 10 240 | | * Tetryl Alternative initiating char | TOPS |
| 15 235 | | Ballistic Mortar, % TNT: (a) | 150 |
| 20 - | | Trauzi Test, % TNT: (b) | 157 |
| 75°C International Heat Test: | 0.00 | Plate Dent Test: (c) | · |
| % Loss in 48 Hrs | 0.03 | Method | А |
| | | Condition | Pressed |
| 100°C Heat Test: | 0.04 | Confined | Yes |
| % Loss, 1st 48 Hrs | 0,00 | Density, gm/cc | 1.50 |
| % Loss, 2nd 48 Hrs Explosion in 100 Hrs | None | Brisance, % TNT | 135 |
| Explosion In Too Hrs | TYONG | Detenation Poto: | |
| Flammability Index: (d) | 278 | Detonation Rate: | None |
| | | Condition | Pressed |
| Hygroscopicity: % 25°C, 100% RH | 0.02 | Charge Diameter, in. | 1.0 |
| | | Density, gm/cc | 1.65 |
| Volatility: | Ni 1 | Rate, meters/second | 8180 |

*Name given by Clarence J. Bain of Picatinny Arsenal. Germans call it Hexogen; Italians call it T4; British, RDX.

Cyclonite (RDX)

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: |
|---|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: White |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Detonator base charge, and ingredient for projectile and bomb fillers |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pressed |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Loading Density: gm/cc p s i x 10 ³ 3 10 12 15 20 1.46 1.52 1.60 1.63 1.65 1.68 Storage: |
| Density, gm/cc | Method Wat |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 |
| Air: Peak Pressure Impulse Energy | Compatibility Group Group M (wet) Group L (dry) Exudation None |
| Air, Confined: Impulse | Effect of Temperature on <u>Rate of Detonation:</u> (k) <u>16 hrs at</u> , ^o C -54 21 <u>Density</u> , gm/cc 1.61 1.62 |
| Under Water: Peak Pressure Impulse | Rate, m/sec 8100 8050 |
| Energy | Effect of Temperature on Impact Sensitivity: |
| Underground: Peak Pressure Impulse Energy | Temp.PA Impact Test°C2Kg Wt. inchesRoom932.281045 |
| | |

Cyclonite (RDX)

| Water | Alcohol | Acetone | Benzene | Toluene |
|---|--|---|--|---|
| $\begin{array}{ccc} \circ_{\rm C} & {}_{\mathcal{B}} \\ \hline 30 & 0.005 \\ 50 & 0.025 \\ 70 & 0.076 \\ 90 & 0.19 \\ 100 & 0.28 \end{array}$ | ⁰ C 0 0.040 20 0.105 40 0.240 60 0.579 78 1.195 | ° <u>c</u> <u>%</u> 20 7.3 40 11.5 60 18. | 20 0.05 40 <i>0.09</i> 60 0.20 80 0.41 | $\begin{array}{c c} & & & & \\ \hline 0 & 0.015 \\ 20 & 0.02 \\ 40 & 0.05 \\ 60 & 0.13 \\ 80 & 0.30 \\ 100 & 0.65 \end{array}$ |
| Ethvl acetate | <u>Carbon</u> tetrachloride | Methanol | Ether | INT |
| ° <u>c</u> ∯ 28 2.9 94 18. | <u>°c</u> <u>∉</u> 50 0.005 60 0.007 70 0.009 | ° <u>c</u> <u>%</u> 0 0.14 20 0.23 40 0.47 60 1.1 | °c ₫ 10 0.05 20 0.056 30 0.076 | °C % 80 4.4 85 5.0 90 5.55 95 6.2 100 7.0 105 7.9 |
| Isoamyl alcohol | <u>Methyl</u> acetate | <u><i>B</i>-Ethoxyethyl</u> <u>acetate</u> | Chlorobenzene | Trichloro- ethylene |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $\begin{array}{ccc} \bullet_{C} & \phi_{0} \\ \hline 20 & 2.9 \\ 30 & 3.3 \\ 40 & 4.1 \\ 50 & 5.6 \end{array}$ | o _c | °c ∉ 20 0.33 30 0.44 40 0.56 50 0.74 | °c ₡ 20 0.20 30 0.22 40 0.24 50 0.26 |
| <u>Tetra-</u> chloroethane | <u>Isopro-</u> panol | Isobutanol | Chloroform | Mesityloxide |
| °c <u>%</u> 38 0.09 | <u>°c ∯</u> 38 0.18 | ° <u>c</u> <u>₫</u> 23 0.0 | <u>°c</u> <u>∦</u> 20 0.01 | $ \frac{\circ_{\mathbf{C}}}{27} \frac{\%}{3.2} \\ 97 12.2 $ |
| <u>Cyclo-</u> hexanone | <u>Nitro-</u> Þ onson e | Nitro- ethane | Cyclo- pentanone | Acetonitrile |
| <u>°c</u> 25 12.7 97 25 | <u>oc</u> <u>%</u> 25 1.5 97 12.4 | <u>°c ∦</u> 28 3.6 93 19 | °c ∦ 28 11.5 90 37 | ${ \circ_{\rm C} \atop 28 \ 11 \atop 82 \ 33 } { {\rm A} \atop 11 \atop 32 \ 33 }$ |
| | | l ethyl ketone | | |
| | °c 28 95 | <u>7</u> 5.6 14 | | |

Solubility of Cyclonite; gm/100 gm of the following substances: (j)

Solubility of Cyclonite, Holston Lot E-2-5 in Various Solvents:

Solubility

Solvent

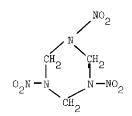
| Solvent | <u>Boiling</u> <u>Point,</u> <u>oc</u> | Grade or Source* | 28 ⁰ C | Heated | Crystalline Form |
|--------------------------|--|---------------------|-------------------|---------------------------|----------------------------|
| Acetone | 56 | CP | 8.2 | 16.5 at 60°C | hexagonal-thick |
| Cyclohexanone | 155.6 | CP | 13.0 | 24.0 at 93°C | cubic (massive form) |
| Nitromethane | 100.8 | | 1.5 | 12.4 at 97°C | plates |
| Acetonitrile | 81.6 | Miacet | 11.3 | 33.4 at 93°C | plates |
| | | Chem. Co. | 1 4 | 10.6 at 93 ⁰ 0 | short needles |
| 1-Nitropropane | 126.5 | EK Pract | 1.4 | | short needles |
| 2-Nitropropane | 120 | EK Pract | 2.3 | 11.6 at 93°C | |
| 2,4-Pentanedione | 140.5 | Carbide & | 2.9 | 18.3 at 93°C | flat prisms |
| | | Carbon | | 0.6 | 1 |
| Methylisobutylketone | 115.8 | | 2.4 | 9.6 at 93°C | long prisms |
| n-Propylacetate | 101.6 | EK Red Label | 1.5 | 6.0 at 93 ⁰ C | long prisms, some cubic |
| n-Butylformate | 105.6 | EK Red Label | 1.4 | 4.6 at 93°C | long prisms |
| Ethyl acetate | 77.1 | Baker's OP | 2.0 | 6.1 at boil. | hexagonal plates |
| | 121 | EK Red Label | 0.8 | 1.6 at 93°C | short prisms, some |
| n-Propylpropionate | 121 | | | | cubic |
| Butylacetate | 126.5 | EK Technical | 1.1 | 4.0 at 93 ⁰ 0 | long prisms |
| Methylethylketone | 79.6 | | 5.6 | 13.9 at boil. | coarse plates |
| Nitroethane | 114.2 | EK Red Label | 3.6 | 19.5 at 93 ⁰ 0 | plates |
| Isopropylacetate | 88-90 | CP | 1.1 | 3.2 at boil. | long prisms |
| Mesityloxide | 128 | EK Red Label | 4.8 | 14.5 at 93°C | plates |
| n-Amylaceta t e | 146 | CP | 1.0 | 2.1 at 93°C | prisms |
| Dimethylcarbonate | 88-91 | EK Red Label | 1.4 | 6.6 at boil. | plates |
| Diethylcarbonate | 125-126.5 | EK Red Label | 0.7 | 3.2 at 93°C | prisms |
| Isoamylacetate | 132 | CP | 1.2 | 3.6 at 9300 | prisms |
| Ethylpropionate | 98-100 | EK Red Label | 3.0 | 10.7 at 93°C | fairly thick hex |
| Linyipiopionate | <i>y</i> o 1 0 | | - | | plates |
| Methyl-n-butyrate | 101.5-103.5 | EK Red Label | 1.2 | 4.9 at 93 ⁰ 0 | needles |
| Cyclopentanone | 130.6 | EK Red Label | 11.5 | 39.0 at 93.5% | |
| Acrvlonitrile | 77.3 | Cyanamid Co. | 4.0 | 16.4 at boil. | flat plates |
| Methylcellosolveacetat | | Carbide & | 1.6 | 8.8 at 93°C | massive hexagons and |
| inethy reenosory caectar | U 177.J | Carbon | | | prisms |
| | | caroon | | | |

* EK, Eastman Kodak; Pract, practical.

Preparation:

(Summary Technical Report of the NDRC, Div 8, Vol 1)

$$(CH_2)_6 N_4 + 4HNO_3 + 2NH_4NO_3 + 6(CH_3CO)_2 O$$



Ammonium nitrate and acetic anhydride are placed in a flask and, while the mixture is stirred at 75°C, the following three liquids are introduced concurrently and proportionately: acetic anhydride, concentrated nitric acid, and a solution of hexamine in glacial acetic acid. The final mixture is held for a short time at 75°C, diluted with water to 30% acetic acid, and simmered to hydrolyze unstable reaction by-products, which are a mixture of various nitrated and acetylated derivatives of hexamine fragments. After simmering, the slurry is cooled and the precipitated cyclonite removed by filtration. The yield is 78% of the theoretical amount (2 moles) of cyclonite melting at 199°C. By dissolving the ammonium nitrate in the nitric acid, a continuous process, based on 3 liquids, is possible.

The product is recrystallized from acetone, or cyclohexanone, to (a) remove acidity, (b) control particle size and (c) to produce stable β -HMX. The preparative procedure described above, the Bachmann or Combination process, yields cyclonite containing 3-8%HMX.

Origin:

First prepared by Henning in 1899 (German Patent 104,280) and later by von Hertz (U. S. Patent 1, 402,693) in 1922 who recognized its value as an explosive. Not used on a large scale in explosive ammunition until World War 11.

Destruction by Chemical Decomposition:

Cyclonite (RDX) is decomposed by adding it slowly to 25 times its weight of boiling 5% sodium hydroxide. Boiling should be continued for one-half hour.

References: 14

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III</u> - <u>Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, <u>OSRD Report No.</u> 5746, 27 December 1945.

- (b) Ph. Naoum, <u>Z. ges Schiess Sprengstoffw</u>, pp. 181, 229, 267 (27 June 1932).
- (c) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(d) Philip C. Keenan and Dorothy Pipes, <u>Table of Military High Explosives</u>, Second Revision, NAVORD Report No. 87-46, 26 July 1946.

¹⁴See footnote 1, page 10.

Cyclonite (RDX)

(e) Armament Research Department (Woolwich), <u>Solubility of RDX in Nitric Acid</u> (ARD Expl Rpt 322/43 September 1943).

(f) Report AC-2587.

(g) <u>International Critical Tables</u> Land. Bornst.

B. T. Fedoroff et al, <u>A Manual for Explosives Laboratories</u>. Lefax Society Inc, Philadelphia, 1943-6.

(h) E. Hutchinson, <u>The Thermal Sensitiveness of Explosives</u>. <u>The Thermal Conductivity of</u> <u>Explosive Materials</u>, AC 2861, First Report, August 1942.

(i) R. J. Finkelstein and G. Gamow, <u>Theory of the Detonation Process</u>, NAVORD Report No. 90-46, 20 April 1947.

(j) International Critical Tables.

(k) W. F. McGarry and T. W. Stevens, Detonation Rates of the More Important Military Explosives at Several Different Temperatures, PAIR No. 2383, November 1956.

(1) Also see the following Picatinny Arsenal Technical Reports on Cyclonite:

| <u>o</u> | <u>1</u> | 2 | <u>3</u> | <u>4</u> . | <u>5</u> | <u>6</u> | <u>7</u> | 8 | 9 |
|--|--|---|---|--|--|--|---|--|---|
| 1170 1290 1360 1450 1760 1980 2100 | $1211 \\ 1241 \\ 1311 \\ 1421 \\ 1481 \\ 1561 \\ 1611 \\ 1651 \\ 1741 \\ 1751 \\ 1761 \\ 2131 \\ 2151$ | 582 1342 1352 1372 1402 1452 1492 1532 2062 2112 | 863 1193 1293 1433 1483 1503 1693 1713 1793 1923 | 1184 1414 1454 1614 1634 2024 2154 2204 | 65 1175 1185 1435 1445 1715 1885 1915 1935 2095 2125 2205 | $1236 \\1316 \\1416 \\1446 \\1466 \\1476 \\1516 \\1556 \\1756 \\1756 \\1766 \\1796 \\1836 \\1956 \\1956 \\2016 \\2056$ | 857 1207 1427 1437 1517 1617 1687 1737 1747 1787 1797 1957 2147 2227 | 1438 1458 1498 1578 1958 1958 2008 2028 2178 2198 | 709 1379 1429 1449 1469 1709 1909 2059 2179 |

2176

| Composition: | Molecular Weight: 224 |
|--|--|
| % RDX 75 INT 25 | Oxygen Balance: CO, % - 35 CO % - 6 |
| | Density: gm/cc Cast 1.71 |
| | Melting Point: °C |
| C/H Ratio | Freezing Point: "C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | Boiling Point: "C |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ |
| Friction Pendulum Test: Steel Shoe Un affected Fiber Shoe Un affected | Vacuum Stability Test: cc/40 Hrs, at 90°C |
| Rifle Bullet Impact Test: Trials % Explosions 30 | - 100°C 0.23 120°C 0.41 135°C - 150°C |
| Partials Smokes 40 Burned 0 Unaffected 30 | 200 Gram Bomb Sond Test: Sand, gm |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) 1 5 10 15 20 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminote Lead Azide Tetryl Ballistic Mortar, % TNT: |
| 20 | Trauzl Test, % YNT: |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT |
| Flammability Index: | Detonation Rate: Confinement None None |
| Hygroscopicity: % | Condition Cast Cast Charge Diameter, in. 1.0 1.0 |
| Volatility: | Density, gm/cc1.701.71Rate, meters/second80357938 |

| Booster Sensitivity Test: Condition | | Decomposition Equation: Oxygen, otoms/sec (Z/sec) |
|---|---------------|---|
| Tetryl, gm | | Heat, kilocalarie/male |
| Wax, in. for 50% Detonation | | (AH, kcal/mal) |
| Wax, gm | | Temperature Range, °C |
| Density, gm/cc | | Phase |
| Heat of: Combusticn, col/gm | 2625* | Armor Plate Impact Test: |
| Explosion, cal/gm | 1225* | 60 mm Mortar Projectile: |
| Gas Volume, cc/gm | 862 | 50% Inert, Velocity, ft/sec |
| Formation, col/gm | | Aluminum Fineness |
| Fusion, col/gm (h) | 5.0 | |
| *Calculated from composition of miz | <u>xture.</u> | 500-Ib General Purpose Bombs: |
| Specific Heat: col/gm/°C (h) O_{C} O_{C} | | Plate Thickness, inches |
| -75 0.220 75 0.352 | | 1 |
| 0 0.225 85 0.325 | | 11/4 |
| 25 0.254 90 0.332 | | 11/2 |
| 50 0.296 100 0.351 | | 134 |
| Burning Rate: | | - '/4 |
| cm/sec | | Bomb Drop Test: |
| | | |
| Thermal Conductivity: cal/sec/cm/°C | | T7, 2000-1b Semi-Armor-Piercing Bomb vs Concrete: |
| Coefficient of Expansion: | | Max Safe Drop, ft |
| Linear, %/°C | | 500-1b General Purpose Bomb vs Concrete: |
| Volume, %/°C | | Height, ft |
| | | Trials |
| Hardness, Mohs' Scale: | | Unaffected |
| 1 | | Low Order |
| Young's Modulus: | | High Order |
| E', dynes/cm² | | |
| E, Ib/inch² | | 1000-Ib General Purpose Bomb vs Concrete: |
| Density, gm/cc | | |
| | | Height, ft |
| Compressive Strength: Ib/inch ² | | Trials |
| | | Unaffected |
| | | Low Order |
| °C mm Mercury | | High Order |
| | | |
| | | |

| Fragmentation Test: | | Shaped Charge Effectiveness, TNT | = 100: |
|---|-----------|--|----------------------|
| 90 mm HE, M71 Projectile, Lo | t WC-91: | Glass Cones S | teel Cones |
| Density, gm/cc | 1.72 | Hole Volume | |
| Charge Wt, Ib | 2.22 | Hole Depth | |
| Total No. of Fragments: | | | |
| For TNT | 703 | Color: Yellow-but | I |
| For Subject HE | 1514 | Principal Uses: Shaped charge | e bomb especially |
| 3 inch HE, M42A1 Projectile, | _ot KC-5: | | ; HE projectiles; |
| Density, gm/cc | | grenades | |
| Charge Wt, Ib | | | |
| | | | |
| Total No. of Fragments: For⊤N⊤ | | Method of Loading: | Cast |
| For Subject HE | | Loading Density: gm/cc | 1.71 |
| | | | 1.71 |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | | Storage: | |
| Density, gm/cc | | Method | Dry |
| Blast (Relative to TNT): | (d) | Hazard Class (Quantity-Distance | e) Class 9 |
| | | Compatibility Group | Group I |
| Air: Peak Pressure | 111 | | Gloup 1 |
| | 126 | Exudation | |
| Impulse | 120 | | |
| Energy | | Preparation: See Compositio | n B |
| Air, Confined: | | Origin: Developed by the Br | |
| Impulse | | Wars I and II and standar States early in World Wa | rdized in the United |
| Under Water: Peak Pressure | | Black Modulus at Room Temperature (25°-30°C): | |
| Impulse | | Dynes/cm ² x 10-10 | 3.09 |
| Energy | | Density, gm/cc | 1.7 ⁴ |
| Undergr o und : Peak Pressure | | Absolute Viscosity, poises: Temp, 85°C 90°C | 210** |
| Impulse | | Efflux Viscosity, Saybolt S | econds: |
| Energy | | Temp, 85°C | 9-14 |
| | | Compositions using Spec G Class A RDX. ** Composition prepared using particle size. | |

| Composition: % | Molecular Weight: | 224 |
|--|--|----------------------------|
| 70 RDX 70 TNT 30 | Oxygen Balance: CO, % CO % | - 37 - 8 |
| | Density: gm/cc Cast | 1.71 |
| | Melting Point: °C | |
| C/H Ratio | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 60 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 14 Sample Wt, mg 20 | Boiling Point: "C Refractive Index, n ^D ₂₀ n ^D ₂₃ n ^D ₃₀ | |
| Friction Pendulum Test: Steel Shoe Unaffected Fiber Shoe Unaffected | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C | |
| Rifle Bullet Impact Test: Trials Kerplosions 30 Partials 30 | 120°C 135°C 150°C | 0.86 |
| Burned 0 Unaffected 40 | 200 Gram Bomb Sand Test: Sand, gm | 56.6 |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) - 1 - 5 Decomposes 265 10 | Sensitivity to Initiation: Minimum Detonating Charge, g Mercury Fulminate Lead Azide Tetryl * Alternative initiating char | 0.21* 0.20* |
| 15 20 | Ballistic Mortar, % TNT: (a) | 135 |
| | Trauzl Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: (b) Method | В |
| 100°C Heat Test: % Loss, 1st 48 Hrs 0.07 % Loss, 2nd 48 Hrs 0.08 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT | Cast No 1.725 136 |
| Flammability Index: | Detonation Rate: Confinement | None |
| Hygroscopicity: % N i 1 | Condition Charge Diameter, in. | Cast 1.0 |
| Volatility: N i 1 | Density, gm/cc Rate, meters/second | 1.73 8060 |

| ragmentation Test: | | Shaped Charge Effectiveness, TNT == | 100: |
|--------------------------------|-------------|--|-----------------|
| 90 mm HE, M71 Projectile, Lo | t WC-91: | Glass Cones Steel | Cones (e) |
| Density, gm/cc | 1.71 | Hole Volume | |
| Charge Wt, Ib | 2.213 | Hole Depth 1 | 30 |
| Total No. of Fragments: | | Color: Ye | llow-buff |
| For TNT | 70 3 | | .110 w - 0 u 11 |
| For Subject HE | 1165 | Principal Uses: Shaped charge bo | |
| 3 inch HE, M42A1 Projectile, L | ot KC-5: | especially fragm | entation HE |
| Density, gm/cc | 1.72 | projectiles, gre | nades |
| Charge Wt, Ib | 0.923 | | |
| Total No. of Fragments: | | Mathad of Londian | Gent |
| For TNT | 514 | Method of Loading: | Cast |
| For Subject HE | 828 | | |
| | | Loading Density: gm/cc | i.71 |
| ragment Velocity: ft/sec | | | |
| At 9 ft At 25½ ft | | .Storage: | |
| Density, gm/cc | | | Dry |
| | | Method | Diy |
| last (Relative to TNT): | (d) | Hazard Class (Quantity-Distance) | Class 9 |
| Air: | | Compatibility Group | Group I |
| Peak Pressure | 110 | | |
| Impulse | 120 | Exudation | |
| Energy | | | |
| Air, Confined: | | Preparation: See Composition B | |
| Impulse | | Origin: Developed by the Briti | |
| | | World Wars I and II and stan the United States early in | |
| Under Water: | | - | MOLTA Mai T |
| Peak Pressure | | Absolute Viscosity, poises:* | |
| Impulse | | Temp, 85°C 90°C | 52 0 |
| Energy | | Efflux Viscosity, Saybolt Seco | 53.2 nds: |
| Underground: | | Temp, 85°C | |
| Peak Pressure | | Heat of: |) ** |
| Impulse | | | 2605 |
| Energy | | Combustion, cal/gm Explosion, cal/gm | 2685 1213 |
| | | Gas Volume, cc/gm | 854 |
| | | * Composition using Spec Grade | 'Type A, |
| | | ** Class A RDX. | <u> </u> |
| | | Calculated from composition | ot mixture. |

| Composition: | Molecular Weight: | | |
|---|--|-------|--|
| % RDX 55 | Oxygen Balance: CO, % CO % | -40 | |
| TNT 35 | | - 9 | |
| | Density: gm/cc Cast | 1.71 | |
| | Melting Point: "C | | |
| C/H Ratio | Freezing Point: °C | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | Boiling Point: "C | | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. | Refractive Index, n ^o ₂₀ | | |
| Sample Wt, mg | n ^D ₂₅ | | |
| | n_30 | | |
| Friction Pendulum Test: | Vacuum Stability Test: | | |
| Steel Shoe Unaffected | cc/40 Hrs, at | | |
| Fiber Shoe Unaffected | 90°C 100°C | | |
| Rifle Bullet Impact Test: Trials | 120°C | | |
| % | 135°C | | |
| Explosions | 150°C | | |
| Partials | | | |
| Burned | 200 Gram Bomb Sand Test: | 55.4 | |
| Unaffected | Sand, gm |))··· | |
| Explosion Temperature: °C | Sensitivity to Initiation: | | |
| Seconds, 0.1 (no cap used) | Minimum Detonating Charge, gm | | |
| 1 5 Decomposes 270 | Mercury Fulminote | | |
| 10 | | | |
| 15 | Tetryl | | |
| 20 | Ballistic Mortar, % TNT: (a) | 134 | |
| | Trauzi Test, % TNT: | | |
| 75°C International Heat Test: | Plate Dent Test: | | |
| % Loss in 48 Hrs | Method | | |
| 100°C Heat Test: | Condition | | |
| % Loss, 1st 48 Hrs | Confined | | |
| % Loss, 2nd 48 Hrs | Density, gm/cc | | |
| Explosion in 100 Hrs | Brisance, % TNT | | |
| · · · · · · · · · · · · · · · · · · · | Detonation Rate: | | |
| Flammability Index: | Confinement | None | |
| | Condition | Cast | |
| Hygroscopicity: % Ni 1 | Charge Diameter, in. | 1.0 | |
| NA TRANSPORT | Density, gm/cc | 1.72 | |
| Volatility: Ni 1 | Rate, meters/second | 7975 | |

| Fragmentation Test: | | Shaped Charge Effectiveness, $TNT = 2$ | 100: |
|--|---------------------|---|-------------|
| 90 mm HE, M71 Projectile, Lot | WC-91: | Glass Cones Steel | Cones (e) |
| Density, gm/cc | 1.71 | Hole Volume | |
| Charge Wt, Ib | 2.253 | Hole Depth 130 |) |
| Total No. of Fragments: | | Color: Yellow-bu | οfε. |
| For TNT | 703 | 16110w-bd | (1) |
| For Subject HE | 1153 | Principal Uses: Shaped charge bon | |
| 3 inch HE, M42A1 Projectile, L | ot KC-5: | especially fragm | |
| Density, gm/cc | 1.71 | projectiles, gren | lades |
| Charge Wt, Ib | 0.922 | | |
| Total No. of Fragments: | | Method of Loading: | Cast |
| For TNT | 514 | U | |
| Far Subject HE | 769 | Loading Density: gm/cc | 1.71 |
| | | Loading Density, gni/ cc | 1.71 |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | | Storage: | |
| Density, gm/cc | | | |
| Benaity, giny ee | | Method | Dry |
| Blast (Relative to TNT); | | Hazard Class (Quantity-Distance) | Class 9 |
| Air: | | Compatibility Group | Group I |
| Peak Pressure | | | L. |
| Impulse | | Exudation | |
| Energy | | | |
| | | Preparation: See Composition B | |
| Air, Confined: | | | |
| Impulse | | Origin: Developed by the Britis World Wars I and II and stand the United States early in Wa | lardized in |
| Under Water: Peak Pressure | | | |
| Impulse | | Eutectic Temperature, ^O C: | 79 |
| Energy | | gm RDX/100 gm TNT | |
| | | 79°C | 4.16 |
| Underground: | | 95 ⁰ C | 5.85 |
| Peak Pressure | | Absolute Viscosity, poises:* | |
| Impulse | | | |
| Energy | | Temp, 85°C 90°C | 30.2 |
| Heat of: | * | * Composition using Spec Grade | 26.0 |
| Combustion, cal/gm Explosion, cal/gm * Gas Volume, cc/gm | 2755 1205 845 | Class A RDX. | туде А, |
| * Calculated from composi | tion of mixture. | | |

| Composition: % | Molecular Weight: | 224 |
|--|--|----------------------------|
| 70 RDX 60 TNT 40 | Oxygen Balance: CO, % CO % | -43 10 |
| | Density: gm/cc Cast | 1.68 |
| | Melting Point: °C | |
| C/H Ratio | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 75 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 1 ¹ / ₄ Sample Wt, mg 19 | Boiling Point: "C Refractive Index, n ^D ₂₀ n ^D ₂₃ n ^D ₃₀ | |
| Friction Pendulum lest: Steel Shoe Unaffected Fiber Shoe Unaffected | Vacuum Stability lest: cc/40 Hrs, at 90°C | |
| Rifle Bullet Impact lest: Trials % Explosions 5 Partio Is 55 | | 0.29 |
| Burned25Unaffected15 | 200 Grcm Bomb Sand Test: Sand, gm | 54.6 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Decomposes 280 10 | Sensitivity to Initiation: Minimum Detonating Charge, gn Mercury Fulminate Lead Azide Tetryl. <u>*Alternative_initiating_char</u> | 0.22* 0.20* |
| 15 | Ballistic Mortar, % TNT: (a) | 1.33 |
| 20 | Irauzliest, % TNT: | |
| 75°C International Heat lest: % Loss in 48 Hrs | Plate Dent lest: (b) Method | В |
| 100°C Heat lest: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | Cast No 1.72 1.32 |
| Flammability Index: | Detonation Rate: Confinement | None |
| Hygroscopicity: % Ni 1 | Condition Charge Diameter, in. | Cast 1.0 |
| Volatility: N i 1 | Density, gm/cc Rate, meters/second | 1. 7 2 7900 |

.

Cyclotol, 60/40

| Fragmentation lest: | | §hoped Charge Effectiveness, $TNT = T$ | 100: |
|--------------------------------------|-------------------------|--|---------------|
| 90 mm HE, M71 Projectile, Lot | WC-91: | | Cones (e) |
| Density, gm/cc | 1.65 | Hole Volume 178 1 | 62 |
| Charge Wt, Ib | 2.187 | Hole Depth 125 1 | 48 |
| Total No. of Fragments: | | Color: Yello | ow-buf f |
| For TNT | 703 | | |
| For Subject HE | 998 | Principal Utes: Shaped charge bo | mb; |
| 3 inch HE, M42A1 Projectile, Lo | t KC-5: | especially fragm projectiles, gre | entation HE |
| Density, gm/cc | 1. 67 | 1 2 7 3 | |
| Charge Wt, Ib | 0.882 | | |
| Total No. of Fragments: | | Method of Loading: | Cast |
| For TNT | 514 | | |
| For Subject HE | 701 | Loading Density: gm/cc | 1.68 |
| | (-) | | 1.00 |
| Fragment Velocity: ft/sec At 9 ft | (c) 2965 | | |
| At 25½ ft | 2800 | Storage: | |
| Density, gm/cc | | | |
| | | Method | Dry |
| last (Relative to TNT): | (d) | Hazard Class (Quantity-Distance) | Class 9 |
| Air: | | Compatibility Group | Group I |
| Peak Pressure | 104 | | |
| Impulse | 116 | Exudation | |
| Energy | | | |
| Air, Confined: | | Preparation: See Composition E | 3 |
| Impulse | | Origin: Developed by the Briti | sh between |
| | | World Wars I and II and stan | dardized in |
| Under Water: Peak Pressure | | the United States early in V | world War II. |
| | | Bulk Modulus at Room | |
| Impulse | | Temperature (25°-30°C): | |
| Energy | | Dynes/cm ² x 10 ⁻¹⁰ | 4.14 |
| Underground: | | Dynes/cm ⁻ x 10 Density, gm/cc | 4.14 1.72 |
| Peak Pressure | | | |
| Impulse | | Absolute Viscosity, poises:* | |
| Energy | * | Temp, 85 ^o C | 12.3 |
| Heat of: | 0 | 90°C | |
| Combustion, cal/gm | 2820 | * Compositions using Spec Grade | Type A |
| Explosion, cal/gm | 1195 845 | Class A RDX. | Type A, |
| Gas 'Volume, cc/gm | 2 nah ² | | |
| Compressive Strength: 1b/i | <u>nen</u> 2200-3000 | | |

X Calculated from composition of mixture.

References: 15

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III</u> - <u>Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, OSRD Report No. 5746, 27 December 1945.

(b) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(c) R. W. Drake, <u>Fragment Velocity and Panel Penetration of Several Explosives in Simulated Shells</u>, OSRD Report No. 5622, 2 January 1946.

(d) V. Philipchuk, Free Air Blast Evaluation of RDX-TNT-A1, RDX-TNT, and TNT-Metal Systems, National Northern Summary Report, NN-P-34, April 1956.

(e) Eastern Laboratory, du Pont, Investigation of Cavity Effect. Section 111, Variation of Cavity Effect with Composition, NDRC Contract W-672-ORD-5723.

(f) W. S. Cramer, Bulk Compressibility Data on Several High Explosives, NAVORD Report No. 4380, 15 September 1956.

(g) Also see the following Picatinny Arsenal Technical Reports on Cyclotols:

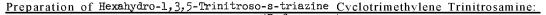
| <u>o</u> | <u>1</u> | 2 | <u>3</u> | <u>4</u> | 5 | <u>6</u> | <u>7</u> | <u>8</u> | 9 |
|--------------|--------------|------|----------------------|------------------------------|--------------|------------------------------|----------------------|----------------------|----------------------|
| 1290 1530 | 1651 1741 | 1482 | 1483 1793 1983 | 1824 1834 1944 2004 | 1435 1585 | 1476 1756 1796 1876 | 1427 1507 1747 | 1398 1488 1838 | 1469 1509 1709 |

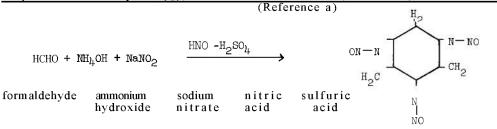
(h) C. Lenchitz, W. Beach and R. Valicky, <u>Enthalpy Changes</u>, <u>Heat of Fusion and Specific</u> <u>Heat of Basic Explosives</u>, PAIR No. 2504, January 1959.

¹⁵See footnote 1, page 10.

| Composition: H | | Molecular Weight: (C ₃ H ₆ N ₆ O ₃) | 174 |
|--|----------------------|--|---------------------|
| % 12 с 20.6 н 3.5 О=N-N | <u>∕</u> n−n=o | Oxygen Balance: CO, % CO % | -55 -28 |
| N 48.3 H ₂ C | CH ₂ | Density: gm/cc | |
| 0 27.6 | | Melting Point: "C | 105 to 107 |
| C/H Ratio 0.12 | | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | | Boiling Point: °C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 15 to 22 17 to 20 | Refractive Index, n ^D ₂₀ n ^D ₂₅ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | (c) |
| Steel Shoe | Unaffected | cc/40 Hrs, at 90°C 0.20 | |
| Fiber Shoe | Unaffected | 100°C 9.19 | 3.71* |
| Rifle Bullet Impact Test: Trials % | | *Average value of 5 gn sample lized from isoamyl alcohol. | |
| Explosions | | | |
| Partials | | | |
| Burned Unaffected | | 200 Gram Bomb Sand Test: Sand, gm | 59.2 54.1 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) | | Sensitivity to Initiation: Minimum Detonating Charge, gm | |
| 1 | | Mercury Fulminate | 0.200** |
| 5 220 | | Lead Azide | 0,100** |
| 10 | | **Alternative initiating charg | ;es. |
| 20 | | Ballistic Mortar, % TNT: | 130 |
| | | Trauzl Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | | Plate Dent Test: Method | |
| 100°C Heat Test: | | Condition | |
| % Loss, 1st 48 Hrs | 8.79 | Confined | |
| % Loss, 2nd 48 Hrs | 2.98 | Density, gm/cc | |
| Explosion in 100 Hrs | None | Brisance, % TNT | |
| Flammability Index: | | Detonation Rate: Confinement | (b) None |
| Hygroscopicity: % 30 [°] C , 90% RH | 0.02 | Condition Charge Diameter, in. | Cast 1.2 |
| Volatility: | | Density, gm/cc | 1.42 100 to 7300 |

| Fragmentation Test: | Shaped Charge Effectiveness, TNT == | 100: |
|---|---|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Hole Volume Hole Depth | l Cones |
| Total No. of Fragments: For TNT | Color: | Yellow |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Ingredient of pr | ojectile filler |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pressed or c melting poin | ast with added t depressants |
| | Loading Density: gm/cc S | see below |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | |
| Densîty, gm/cc | Method | Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | Group M None |
| Air, Confined: Impulse | Density at Various Pressures: lb/inch ² | (b) gm/cc |
| Under Water: Peak Pressure Impulse Energy | 2,420 4,830 9,650 14,500 24,200 33,800 42,500 | 1.10 1.23 1.37 1.44 1.53 1.57 1.59 |
| Underground: Peak Pressure Impulse Energy | <u>Heat of:</u> Combustion, cal/gm | 3158 |
| | Explosion, cal/gm Formation, cal/gm | 876 -914 |





An ammoniacal solution of an amine is prepared by adding aqueous formaldehyde to ammonium hydroxide. The rate of addition of formaldehyde is regulated to maintain a solution temperature of 30° to 35° C.

Sodium nitrite is dissolved in water and the solution or slurry is then poured into the previously prepared amine-ammonia solution and totally dissolved by stirring. This solution is chilled to below $0^{\circ}C$.

Into a mixed acid solution, previously prepared by dissolving concentrated nitric acid in water and adding concentrated sulfuric acid, all chilled to -9 C, there is added the cold amine-nitrite solution below the surface of the acid mixture. The addition is regulated to take 20 to 30 minutes.

The resulting foamy head of cyclotrimethylene trinitrosamine is allowed to sit over the icy spent liquor for 1/2 hour and is then collected on a sintered glass funnel and washed to neutrality. The moist cyclotrimethylene trinitrosamine is removed from the funnel and air-dried on filter paper. The dry crude product melts at 106° to 107° C. Recrystallization from isoamyl alcohol gives a pure compound melting at 105° to 107° C.

Orinin:

Cyclotrimethylene trinitrosamine was discovered in 1888 simultaneously by Griess and Harrow (Ber 21 (1888), p. 2737) and by Mayer (Ber 21 (1888), p. 2883) when sodium nitrite was allowed to react with hexamethylene tetramine in acid solution. This compound was later studied by Duden and Scharff (Ann 288 (1895), p. 218) and by Delepine who determined its heat of formation, which was negative (Bull Soc chim (3) 15 (1896), p. 1199). Because cyclotrimethylene trinitrosamine could be made at first in very poor yield only, it was a long time before it received consideration for practical application as an explosive. However, the study of cyclotrimethylene trinitrosamine was continued and investigations were made as to its behavior in mixtures with other substances (Prof. D. G. Romer "Report on Explosives," BIOSGP 2-HEC 5742).

Destruction by Chemical Decomposition:

Cyclotrimethylene trinitrosamine is easily decomposed by acid or alkali and even by boiling in water.

Cyclotrimethylene Trinitrosamine

| <u>Ingli remperature Decomposition. 0.02 an rin rome rest ruce.</u> | High Temperature | Decomposition. | 0.02 | gm in | 10 ml | Test Tube: | (b) |
|---|------------------|----------------|------|-------|-------|------------|-----|
|---|------------------|----------------|------|-------|-------|------------|-----|

| I | | | | | |
|-----|---|---------------------------------|--|--|--|
| | | Temp. ^O C | | | |
| (1) | Melting begins Decomposition begins Nitrous gas Entire decomposition | 105 150 160 170 | | | |
| (2) | Some bubbles Very slow decomposition Decomposes in 2 minutes Decomposes in 40 seconds Immediate decomposition | 110 150 200 250 300 | | | |

Long Term Stability: (b)

Cyclotrimethylene Trinitrosamine loosely packed in covered wooden boxes for six years at ambient temperature and protected from the sun:

- 1. Explosive showed no color change.
- 2. Melting point decreased from 104.5° to 104° C.
- 3. Coefficient of "Utilisation Practique" decreased from 125.5 to 123.5.
- 4. An Abel Test at 110^oC gave no color to iodine starch paper in 15 minutes.

| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | Melting _o Point, C | I | <u>Øv</u> clotrimethylene Trinitrosamine, % |
|---|---|---|--|
| 60 69 70 77 95 95 | 68 62 55 55 (Eutectic) 61 69 77 | | 20 30 40 42 50 60 70 |

Fusion Tests, Mixtures of Cyclotrimethylene Trinitrosamine and TNT: (b)

42% Cyclotrimethylene Trinitrosamine 58%TNT

7,000

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AMCP 706-177
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<u>Reaction of Cyclotrimethylene Trinitrosamine With Other Materials:</u> (b)

| 1. | Iron powder | Slight reaction |
|----|------------------------------------|--|
| 2. | Copper powder | Slight reaction |
| 3. | Aluminum powder | Slight reaction |
| 4. | 2 parts picric acid + 1part R-Salt | a. Violent decomposition after 2 hours at 10°C b. Violent decomposition after 10 to 15 minutes at 100°C |

Detonation Rate: (b)

| Confinement | Paper cartridge |
|--|--|
| Condition | Pressed |
| Charge Diameter, in. | 1.18 |
| Rate, meters/second | Density, gm/cc |
| 5180 5760 6600 7330 7600 7800 | 0.85 1.00 1.20 1.40 1.50 1.57 |

References: 16

(a) Arthur D. Little, Inc. Progress Report No. 106, Fundamental Development of High Explosives, April 1955, Contract No. DAI-19-020-501-0RD(P)-33.

(b) Louis Médard and Maurice Dutour, "Étude Des Proprietés De La Cyclotriméthyléne Trinitrosamine, "Mém poudr, <u>37</u>, 1924 (1954).

(c) H. A. Bronner and J. V. R. Kaufman, "Synthesis and Properties of R-Salt," PATR in preparation 1959.

(d) Also see the following Picatinny Arsenal Technical Reports on Cyclotrimethylene Trinitrosamine: 1174, 2179.

16See footnote 1, page 10.

DBX (Depth Bomb Explosive)

| Composition: % | Molecular Weight: 83 |
|--|---|
| Ammonium Nitrate 21 | Oxygen Balance: CO, % -46 CO % -26 |
| RDX 21 | |
| TNT 40 | Density: gm/cc Cast 1.68 |
| Aluminum 18 | Melting Point: "C |
| C/H Ratio | Freezing Point: "C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 35 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 13 Sample Wt, mg 14 | Boiling Point: "C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C |
| Rifle Bullet Impact Test: Trials % Explosions Partiols | 120°C 6.15 135°C 150°C |
| Burned Unaffected | 200 Grom Bomb Sand Test: Sand, gm 58.5 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Ignites 400 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminote Lead Azide 0.20 Tetryl 0.10 |
| 15 | Ballistic Mortar, % TNT: (a) 146 |
| 20 | Trauzi Test, % TNT: |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: (b) Method B |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | ConditionCastConfinedNoDensity, gm/cc1.76Brisance, % TNT102 |
| Flammability Index: | Detonation Rate: (c) Confinement None Condition Cast |
| Hygroscopicity: % | Charge Diameter, in. 1.6 |
| Yolatility : | Density, gm/cc 1.65 Rate, meters/second 6600 |

DBX (Depth Bomb Explosive)

| Booster Sensitivity Test: | (e) | Decomposition Equation: |
|---|------------------------|---|
| Condition | Cast | Oxygen, otoms/sec |
| Tetryl, gm | 100 | (Z/sec) Heat, kilocolorie/mole |
| Wax, in. for 50% Detonation | 1.35 | (AH, kcol/mol) |
| Wax, gm | | Temperature Range, °C |
| Density, gm/cc | 1.76 | Phase |
| | | |
| Heat of: | (d) | Armer Diete Impect Test |
| Combustion, cal/gm | | Armor Plate Impact Test: |
| Explosion, col/gm | 1700 | 60 mm Mortar Projectile: |
| Gas Volume, cc/gm | | 50% Inert, Velocity, ft/sec |
| Formation, col/gm | | Aluminum Fineness |
| Fusion, col/gm | | |
| | | 500-Ib General Purpose Bombs: |
| Specific Heat: col/gm/°C | (d) | |
| -5° C, density 1.75 gm/cc | 0.25 | Plate Thickness, inches |
| | | |
| | | 1 |
| | | 11/4 |
| | | 11/2 |
| | | 13⁄4 |
| Burning Rate: | | |
| cm/sec | | |
| | | Bomb Drop Test: |
| Thermal Conductivity: | -4 | T7, 2000-1b Semi-Armor-Piercing Bomb vs Concrete: |
| col/sec/cm/"C | 13.2×10^{-4} | 17, 2000-16 Semi-Amor-Piercing Bomb +3 Concrete. |
| Density 1.75 gm/cc | | Max Safe Drop, ft |
| Coefficient of Expansion: Linear, %/°C -73 ⁰ -75 ⁰ C | 4.5 × 10 ⁻⁵ | |
| Linear, $\%/^{\circ}C = 73^{\circ} = 15^{\circ}C$ | 4.5 x 10 ² | 500-lb General Purpose Bomb vs Concrete: |
| | | |
| Volume, %/°C | | Height, ft |
| Handasaa Mahal Casta | | Trials |
| Hardness, Mohs' Scale: | | Unaffected |
| | (a) | Low Order |
| Young's Modulus: | (d) | High Order |
| E', dynes/cm² | 10.4×10^{10} | |
| E, lb/inch ² | 1.51 x io ⁶ | 1000-Ib General Purpose Bomb vs Concrete: |
| Density, gm/cc | 1.72 | |
| | | Height, ft |
| Compressive Strength: $lb/inch^2$ (d) | 3210-3380 | Trials |
| Density 1.78 gm/cc | | Unaffected |
| Vapor Pressure: | | Low Order |
| "C mm Mercury | | High Order |
| , | | |
| | | |
| | | |
| | | |
| | | |

| Fragmentation Test: | | Shaped Charge Effectiveness, T N T | = 100: |
|-------------------------------|-----------|--|---------------------|
| Fragmentation rest. | | | |
| 90 mm HE, M71 Projectile, L | ot WC-91: | | teel Cones |
| Density, gm/cc | | | |
| Charge Wt, Ib | | Hole Depth | |
| Total No. of Fragments: | | Color: | Gray |
| For TNT | | | Gruy |
| For Subject HE | | Principal Uses: | Depth charge |
| 3 inch HE, M42A1 Projectile, | Lot KC-5: | | · - |
| Density, gm/cc | | | |
| Charge Wt, Ib | | | |
| Total No. of Fragments: | | Method of Loading: | Cast |
| For TNT | | | |
| For Subject HE | | Loading Density: gm/cc | 1.61-1.69 |
| Fragment Velocity: ft/sec | | | · |
| At 9 ft | | 2447777 | |
| At 25½ ft | | Storage: | |
| Density, gm/cc | | Method | Dry |
| Blast (Relative to TNT): | (d) | Hazard Class (Quantity-Distance | e) Class 9 |
| Air: | | Compatibility Group | Group I |
| Peak Pressure | 118 | | |
| Impulse | 127 | Exudation | |
| Energy | 138 | | |
| Air, Confined: | | Preparation: | |
| Impulse | | DBX can be manufactured | hy slowly adding |
| | | water-wet RDX to molten TNT | melted in a steam- |
| Under Water: Peak Pressure | | jacketed kettle equipped wi all the water has evaporate | |
| Impulse | | is added and with heating a | nd stirring con- |
| Energy | 136 | tinued, grained aluminum is ture is cooled with stirrin | added. The mix- |
| | | maintain uniformity and whe | |
| Underground: Peak Pressure | | | BX can also be made |
| | | by adding 21% ammonium nitr num to 42% cyclotol or Com | |
| Energy | | RDX/TNT content plus 19% of | TNT previously |
| | | melted at about 100°C. | |
| | | | |
| | | | |
| | | | |
| | | | |

Origin:

DBX was developed and used by the United States and Great Britain during World War II.

References: 17

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III</u> - <u>Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, <u>OSRD Report No. 5746</u>, 27 December 1945.

(b) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(c) G. H. Messerly, <u>The Rate of Detonation of Various Explosive Compounds</u>, OSRD Report No. 1219, 22 February 1943.

M. D. Hurwitz, The Rate of Detonation of Various Compounds and Mixtures, OSRD Report No. 5611, 15 January 1946.

(d) Philip C. Keenan and Dorothy Pipes, <u>Table of Military High Explosives</u>, Second Revision, NAVORD Report No. 87-46, 26 July 1946.

(e) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute for</u> <u>Tetryl in Boosters</u>. NOL Mano 10,303, 15 June 1949.

(f) Also see the following Picatinny Arsenal Technical Reports on DBX: 1585 and 1635.

¹⁷See footnote 1, page 10.

| Composition: | Molecular Weight: $(C_6H_5N_5O_6)$ | 2 3 |
|---|--|-----------------------|
| $\begin{array}{c} \% \\ \textbf{C} \textbf{29.6} \\ \textbf{H} \textbf{2.1} \\ \end{array} \xrightarrow{\text{NH}_2} \\ \text{NO}_2 \\ \end{array}$ | Oxygen Balance: CO, % CO % | |
| N 28.8 | Density: gm/cc C | Crystal 1.83 |
| 0 3 9.5 ^{NO} 2 | Melting Point: "C | (a) 290 |
| C/H Ratio 0.380 | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: | Boiling Point: "C | |
| Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 18 Sample Wt, mg 9 | Refractive Index, n ^D ₂₀ n ^D ₃₀ | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C | |
| Rifle Bullet Impact Test: Trials % Explosions Partials Burned Unaffected | 100°C 120°C 135°C 150°C | |
| | 200 Gram Bomb Sand Test: Sand, gm | 46.6 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 10 | Sensitivity to Initiation: Minimum Detonating Charge, gr Mercury Fulminate Lead Azide Tetryl | m 0.20 0.10 |
| 15 20 | Ballistic Mortar, % TNT: | 100 |
| | Trauzl Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method | |
| 100°C Heat Test: % Loss, 1st 48 Hrs 0.00 % Loss, 2nd 48 Hrs 0.4 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT | |
| Ficammability Index: | Detonation Rate: Confinement | None |
| Hygroscopicity: % | Condition Charge Diameter, in. | Pressed 0.5 |
| Volatility: | Density, gm/cc Rate, meters/second | 1.65 7500 |

| Fragmentation Test: | Shaped Charge Effectiveness, TN | T = 100: |
|---|--|-------------|
| 90 mm HE, M71 Projectile, Lot WC-91: | Glass Cones | Steel Cones |
| Density, gm/cc | Hole Volume | |
| Charge Wt, Ib | Hole Depth | |
| Total No. of Fragments: | Color: | Yellow |
| For TNT | | |
| For Subject HE | Principal Uses: | |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | | |
| Density, gm/cc | | |
| Charge Wt, Ib | | |
| Total No. of Fragments: For TNT | Method of Loading: | Pressed |
| For Subject HE | Loading Density: gm/cc At 50,000 psi | 1.65 |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | |
| Density, gm/cc | Method | Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distan | ce) |
| Air: | Compatibility Group | |
| Peak Pressure | Exudation | None |
| Impulse | Exudation | None |
| Energy | | |
| Air, Confined: Impulse | <u>Cook-Off</u> Temperature: ^O C Time, minutes | 320 8 |
| | Heat of: | |
| Under Water: Peak Pressure | Explosion, cal/gm | 2876 |
| Impulse | | |
| Energy | | |
| Underground: Peak Pressure | | |
| Impulse | | |
| Energy | | |
| | | |
| | | |
| | | |
| | | |

Preparation:

Fifty grams (50 gm) of dry styphnic acid was added to 200 gm of anhydrous pyridine with stirring. The resulting slurry was stirred for an additional 30 minutes. The yellow product, dipyridinium styphnate, was collected by filtration and washed with approximately 100 milli-liters of diethyl ether. The product was dried over phosphorus (V) oxide, at room temperature, for 5 hours. Yield of 77 gm (94%), melting point 168° to 170° C (literature melting point 173° C).

To 50 milliliters of phosphorus oxytrichloride, 29.8 gm of the dipyridinium styphnate were added in small portions, with stirring. The reaction mixture was then warmed on a steam bath for 15 minutes. This solution was quenched in 500 gm of ice water. The light yellow precipitate was separated by filtration and washed with water until the washing was neutral to litmus. Yield of 1,3-dichloro-2,4,6-trinitrobenzene 20.4 gm (98%), MP 130 to 131°C (literature MP 128°C).

A suspension of 3 gm of 1,3-dichloro-2,4,6-trinitrobenzene in 9 milliliters of absolute methanol was prepared. This slurry was cooled to 0° C, and dry ammonia was bubbled into the stirred suspension. After 20 minutes the reaction mixture was allowed to warm to room temperature, filtered by suction and washed with methanol and ether until a negative Beilstein test for chloride ion was obtained on the washings. Yield of 1,3-diamino-2,4,6-trinitrobenzene 2.5 gm (97%), MP 288° to 290°C (literature MP 285°C).

Origin:

DATNB, also called 2,4,6-trinitro-1,3-diamino-benzol or 2,4,6-trinitro-phenylenediamine-(1,3), was first obtained by Noelting and Collin in 1884 (Ber <u>17</u>, 260) and also by Barr in 1888 (Ber <u>21</u>, 1546) from 2,4,6-trinitroresorcin dimethylether in contact with ammoniacalalcohol for several days. J. J. Blanksma obtained the same product in 1902 by reacting either 2-chloro-2,4,6-trinitroanisole or 3-chloro-2,4,6-trinitrophenetol with ammoniacalalcohol (Rec trav chim <u>21</u>, 324) and from 2,4,6-trinitroresorcin methylethyl ether with ammoniacal alcohol (Rec trav chim <u>27</u>, 56 (1908)).

Meisenheimer and Patzig in 1906 prepared DATMB in the form of yellow needles, MP 280° C from 1,3,5-trinitrobenzene hydroxylamine and sodium methylate in methyl alcohol (Ber <u>39</u>, 2540). The product was slightly soluble in glacial acetic acid but poorly soluble in other solvents. It decomposed into NH₃ and 2,4,6-trinitroresorcin when boiled with dilute N4OH or KOH (Beil <u>13</u>, 60).

Körner and Contardi prepared DATNB by the reaction of either 2,4-dichloro-1,3,5-trinitrobenzene or 2,4-dibromo-1,3,5-trinitrobenzene with ammoniacal alcohol at room temperature or better by heating to 100° C (Atti R. Accad Lincei (5), 171, 473 (1908)); (5) 18 I, 101 (1909)). A method of preparation by prolonged reaction of N-nitro-N-methyl-2,3,4,6-tetranitroaniline with a saturated ammonia solution was reported in 1913 by van Romburgh and Schepers (Akad Amsterdam Versl 22, 297).

C. F. Van Duin obtained DATNB melting at 301° C by reacting a concentrated aqueous ammonia solution with N-nitro-N,N,N-trimethyl-2,4,6-trinitrophenylenediamine-(1,3) or with N-nitro-N-methyl-N-phenyl-2,4,6-trinitrophenylenediamine-(1,3) (Rec trav chim <u>38</u>, 89-100 (1919)). Later Van Duin and Van Lennep reacted concentrated aqueous ammonia with 2,4,6-trinitro-3-aminoanisole or 2,4,6-trinitro-3-aminophenetol to obtain DATNB melting at 287° to 288°C (Rec trav chim <u>39</u>, 147-77 (1920)). In 1927 Lorang prepared the same compound by boiling 2,4,6-trinitro-1,3-bis (-nitroethyl ureido) benzene with water or by heating it with ammoniacal alcohol in a tube at 100° C (Rec trav chim <u>46</u>, 649) (Beil E <u>17</u>, E II 33).

A recent report describes the preparation of DATNB in two steps from commercially available starting materials. First m-nitroaniline was nitrated with H_2SO_4 -HNO₃ acid mixture to tetranitroaniline. The crude tetranitroaniline was converted by methanolic ammonia to diaminotrinitro-benzene in a high degree of purity. A conversion of 100 parts of m-nitroaniline into 110 parts of DATNB was obtained by this method, which can easily be carried out on a commercial scale.

| Composition: | N | Molecular Weight: (C6H2N4O5) | 210 |
|---|---------------------|---|---------------------|
| % c 34.3 H 0.9 or* | | Oxygen Balance: | -61 -15 |
| \mathbb{N} 26.7 $\mathbb{O}_2^{\mathbb{N}}$ \mathbb{I} $\mathbb{N}_2^{\mathbb{O}_2^{\mathbb{N}}}$ | 4 NO ⁵ | Density: gm/cc Crystal | 1.63 |
| 0 38.1 | Ö | Melting Point: °C | 157 |
| C/H Ratio 1.056 | | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | | Boiling Point: "C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 4 Sample Wt, mg | ; (1 1b wt) 7 15 | Refractive Index, ກ ^ວ ວ ກ ^ວ ສ ກ ₃₀ | |
| Friction Pendulum lest: | | Vacuum Stability lest: | |
| Steel Shoe | Detonates | cc/40 Hrs, at | |
| Fiber Shoe | Detonates | 90°C | 7.6 |
| Rifle Bullet Impact lest: Trials | | 100°C 120°C | 1.0 |
| % | | 135°C | |
| Explosions | | 150°C | |
| Partials | | | |
| Burned Unaffected | | 200 Gram Bomb Sand lest: | 47.5 45.6 |
| | | Sand am Black powder fuse | 45.6 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) | | Sensitivity to Initiation: Minimum Detonating Charge, gm | |
| 1 200 | | Mercury Fulminate | |
| 5 195 | | Lead Azide | 0.20 |
| 10 180 | | Tetryl | 0.10 |
| 15 | | | 07 |
| 20 | | Ballistic Mortar, % TNT: (a) | 97 |
| 75°C International Heat lest: | | Irauzilest, % TNT: | |
| % Loss in 48 Hrs | | Plate Dent lest: Method | |
| 100°C Heat lest: | | Condition | |
| % Loss, 1st 48 Hrs | 2.10 | Confined | |
| % Loss, 2nd 48 Hrs | 2.20 | Density, gm/cc | |
| Explosion in 100 Hrs | None | Brisance, % TNT | |
| Flammability Index: | | Detonation Rate: Confinement | 4 |
| Hygroscopicity: % 30°C, 90% RH | 0.04 | Charge Diameter, in. | essed |
| Volatility: 50°C, 30 months | Unaffected | • • • | 1.5 1.6 600 6900 |

^{(Until} it is established which picramic acid (melting point 169^oC) isomer is involved (Ref: <u>J</u> <u>Chem Soc</u>, 2082, August 1949).

Diazodinitrophenol

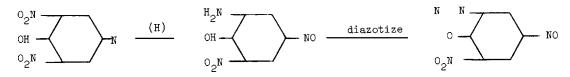
| Fragmentation Test: | Shaped Charge Effectiveness, $TNT=100$: |
|---|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT For Subject HE | Color: Yellow needles |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Percussion caps |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pressed |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Loading Density: gm/cc Apparent 0.27 At 3000 psi 1.14 Storage: |
| Density, gm/cc | Method Under water Hazard Class (Quantity-Distance) Class 9 |
| Blast (Relative to TNT): Air: Peak Pressure Impulse Energy | Compatibility Group Exudation None |
| Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | Solubility:Soluble in nitroglycerin, nitrobenzene, aniline, pyridine, concentrated hydrochloric acid, and in most common organic solvents.Heat of:Combustion, cal/gm3243 820 Gas Volume, cc/gmGas Volume, cc/gm865Sensitivity to Electrostatic Discharge, Joules:0.012 |

Diazodini

| <u>Solubility: gm/100 gm of the following substances:</u> (c | c) |) |
|--|----|---|
|--|----|---|

| <u>Solubility at 50%</u> | <u>c</u> |
|--|---|
| Solvent | <u>%</u> |
| Ethyl acetate Methanol Ethanol Ethylenedichloride Carbon tetrachloride Chloroform Benzene Toluene Petroleum ether Ethyl ether Carbon disulfide | 2.45 1.25 2.43 0.79 trace 0.11 0.23 0.15 Insoluble (at 20°C) 0.08 (30°C) trace (30°C) |

Preparation: (Chemistry of Powder and Explosives, Davis)



Ten gn of picramic acid is suspended in 120 cc of 5% hydrochloric acid, and under efficient agitation at about 0° C. 3.6 gn sodium nitrite in 10 cc water is dumped into the suspension. Stirring is continued for 20 minutes, the product filtered off and washed thoroughly with ice water. The **dark** brown product, if dissolved in acetone and precipitated in water, turns brilliant yellow.

Origin:

Discovered by Griess in 1858 (Annalen 106, 123; 113, 205 (1860) and studied extensively by L. V. Clark (Ind Eng Chem 25, 663 (1933). Developed for commercial use in 1928. This compound was patented in the United States by Professor William M. Dane.

Destruction by Chemical Decomposition:

Diazodinitrophenol is decomposed by adding the water-wet material to 100 times its weight of 10% sodium hydroxide. Nitrogen gas is evolved.

References: 18

(a) Philip C. Keenan and Dorothy Pipes, <u>Table of Military High Explosives</u>, Second Revision, NAVORD Report No. 87-46, 26 July 1946.

(b) F. W. Brown, D. H. Kusler and F. C. Gibson, Sensitivity of Explosives to Initiation by

¹⁸See footnote 1, page 10.

Diazodinitrophenol

Electrostatic Discharges, U. S. Dept of Int, Bureau of Mines, RI 3852, 1946.

(c) L. V. Clark, "Diazodinitrophenol, A Detonating Explosive," Ind Eng Chem 25, 663 (1933).

Seidell, <u>Solubilities of Inorganic and Organic Compounds</u>, Van Nostrand and Co., N. Y.

(d) Also see the following Picatinny Arsenal Technical Reports on Diazodinitrophenol:

| ۵ | 2 | 4 | 5 | Z | 8 | 9 |
|--------------------|------|------------------|-----|-----|--------------------|------|
| 150 610 2120 | 1352 | 34 214 | 355 | 827 | 318 1838 | 2179 |

| | | 10(|
|--|--|-------------------------|
| Composition: % | Molecular Weight: $(C_4H_8N_2O_7)$ | 196 |
| c 24.5 H_2^{C} ONO ₂ H 4.1 H_2^{C} ONO ₂ | Oxygen Balance: CO, % CO % | - ⁴ 1 - 8 |
| | Density: gm/cc Liquid | 1.38 |
| $\begin{bmatrix} N & 14.3 & {}^{12} \\ 0 & 57.1 & {}^{12} \\ H_2 C & ONO_2 \end{bmatrix}$ | Melting Point: °C | 2 |
| C/H Ratio 0.143 | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 100+ | Boiling Point: °C Decomposes | 160 |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 9 Sample Wt, mg | Refractive Index, n ^D n ^D ₂₅ n ^D ₃₀ | 1.4498 |
| Friction Pendulum Test: Steel Shoe Explodes Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C | 0.3cc/20 hr/gm |
| Rifle Bullet Impact Test: Trials % Explosions Partioːs | 120°C 135°C 150°C | o. 300, 20 m², 3m |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm | 42.2 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 237 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl | |
| 15 20 | Ballistic Mortar, % TNT: | 90 |
| | - Trauzl Test, % TNT: | 77 |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method | |
| 100°C Heat Test: % Loss, 1st 48 Hrs 4.0 % Loss, 2nd 48 Hrs 3.0 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement | |
| Hygroscopicity: % | Condition Charge Diameter, in. Density, gm/cc | 1.38 |
| Volatility: 60°C, mg/cm ² /hr 193 | Rate, meters/second | 6760 |

| Booster Sensitivity lest: Condition | | Decomposition Equation: Oxygen, atams/sec |
|--|------|---|
| Tetryl, gm | | (Z/sec) |
| Wax, in. for 50% Detonation | | Heat, kilocalarie/mole |
| Wax, gm | | (AH, kcol/mol) Temperature Range, ℃ |
| Density, gm/cc | | Phase |
| | | |
| Heat of: | | Armer Plate Impact locit |
| Combustion, cal/gm | 2792 | Armor Plate Impact lest: |
| Explosion, cal/gm | 841 | 60 mm Mortar Projectile: |
| Gas Volume, cc/gm | 796 | 50% Inert, Velocity, ft/sec |
| Formation, cal/gm | 2020 | Aluminum Fineness |
| Fusion, cal/gm | | |
| | | 500-1b General Purpose Bombs: |
| Specific Heat: col/gm/°C | | Plate Thickness, inches |
| | | |
| | | |
| | | |
| | | |
| Burning Rate: | | - 1¾ |
| cm/sec | | |
| | | Bomb Drop Test: |
| Thermal Conductivity: cal/sec/cm/°C | | T7, 2000-Ib Semi-Armor-Piercing Bomb vs Concrete: |
| Coefficient of Expansion: | | Max Safe Drop, ft |
| Linear, %/°C | | 500-Ib General Purpose Bomb vs Concrete: |
| Volume, %/°C | | Height, ft |
| | | Trials |
| Hardness, Mohs' Scale: | | Unaffected |
| | | Low Order |
| Young's Modulus: | | High Order |
| E', dynes/cm² | | |
| E, Ib/inch ² | | 1000-Ib General Purpose Bomb vs Concrete: |
| Density, gm/cc | | |
| | | Height, ft |
| Compressive Strength: Ib/inch ² | | Trials |
| | | Unaffected |
| Vapor Pressure: | | Low Order |
| "C mm Mercury | | High Order |
| 20 0.0036 60 0.130 | | |
| 60 0.130 | | |
| | | |
| | | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: |
|---|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, ¹ b | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: Colorless |
| For Subject HE | Principal Uses: Propellant compositions |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | |
| Total No. of Fragments: For TNT | Method of Loading: |
| For Subject HE | Loading Density: gm/cc |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: |
| Density, gm/cc | Method Liquid |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation |
| Air, Confined: Impulse Under Water: Peak Pressure | Preparation: DECN can be prepared with approxi- mately 85% yield by adding diethyleneglycol to mixed acid (50% HNO ₃ , 45% H ₂ SO ₄ , and 5% H ₂ O). The temperature is kept at 30°C or lower. The separated DEGN is purified by washing with successive portions of water, |
| Impulse Energy | dilute sodium carbonate solution and water until neutral. |
| Underground: Peak Pressure | Hydrolysis, % Acid: 10 days at 22°C 0.003 5 days at 60°C 0.003 |
| Impulse Energy | $\begin{array}{c c} Solubility in Water, gm/100 gm, at: \\ \hline 25\% C & 0.40 \\ \hline 60\% C & 0.60 \\ \end{array}$ |
| <u>Viscosity, centipoises:</u> Temp, 20 ⁰ C 8.1 | Solubility, gm/100 gm, at 25°C, in:Ether00Alcohol002:1 Ether:Alcohol00Acetone00 |

Origin:

First prepared and studied by Wm H. Rinkenbach in 1927 (Ind Eng Chem <u>19</u>, 925 (1927) and later by Rinkenbach and H. A. Aaronson (Ind Eng Chem <u>23</u>, 160 (1931)) both of Picatinny Arsenal. Used in propellant compositions by the Germans during World War **11**.

structi by Chemical Decomposition:

| | 1 i | s de | composed | by adding | it | slo | wly (| o 10 | times | ;i | W | 1 18% | sodiur | n sulf | fide |
|-----|-----|------|----------|-----------|----|------|-------|--------|-------|-------|--------|-------|--------|--------|------|
| | | | Heat is | liberated | by | thi | rea | iction | but | this | is not | hazar | i | sti | is |
| mai | | ď | the | tion | of | DEGN | and | conti | nued | until | solut | i s | comple | te. | |

References: 19

See the following Picatinny Arsenal Technical Reports on DEN:

| <u>o</u> | <u>1</u> | 2 | <u>3</u> | 4 | <u>6</u> | Z | <u>9</u> |
|----------------------------------|----------------------------|---------------------------|-------------|-------------|-----------------------------|-----------------------------|--------------------|
| 50 180 620 1490 1990 | 231 551 1391 1421 | 72 602 1282 1392 | 673 1443 | 494 1624 | 346 1516 1616 1786 | 487 1427 1487 1817 | 279 579 1439 |

¹⁹See footnote 1, page 10.

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| Composition: | Molecular Weight: (C10 ^H 12 ^N 4 ⁰ 12) | 380 |
|--|---|-------------------|
| % с 31.6 н 3.2 ¶ ^{снсо} 2 ^{сн} 2 ^{сн} 3 | Oxygen Balance: CO, % CO % | -59 -17 |
| и 14.7 снсо ₂ сн ₂ с(NO2)2сн3 | Density: gm/cc Crystal | 1.60 |
| 0 50.5 C/H Ratio | Melting Point: "C Form II Freezing Point: "C | 89 86 |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 100+ Sample Wt 20 mg Picatinny Arsenal Apparatus, in, 18 Sample Wt, mg 18 | Boiling Point: °C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| Friction Pendulum lest: Steel Shoe Unaffected Fiber Shoe Unaffected | Vacuum Stability lest: cc/40 Hrs, at 90°C 100°C | 0.66 |
| Rifle Bullet Impact lest: Trials % Explosions Partiols | 120°C 135°C 150°C | 0.91 |
| Burned Unaffected | 200 Gram Bomb Sand lest: Sand, gm | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 4 Smokes 250 10 15 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminote Lead Azide Tetryl | |
| 20 | Ballistic Mortar, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | Trauzl lest, % TNT : Plate Dent lest: Method | |
| 100°C Heat lest: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement | |
| Hygroscopicity: % | Condition Charge Diameter, in. | |
| Volatility: | Density, gm/cc Rate, meters/second | 1.49 6050 |

| Fragmentation Test: | Shaped Charge Effectiveness, TN | IT = 100: |
|--|--|--------------------------------|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm∕cc Charge Wt, Ib | Glass Cones Hole Volume Hole Depth | Steel Cones |
| Total No. of Fragments: For ⊤N⊤ For Subject HE | Color: | White |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: | Cast |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc | Loading Density: gm/cc Storage: | 1.50 Dry |
| Blast (Relative to TNT): | Method Hazard Class (Quantity-Distar | · |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | None |
| Air, Confined: Impulse | <u>Heat of:</u> Combustion, cal/gm Detonation, cal/gm | 3070 (calculated) 767 |
| Under Water: Peak Pressure Impulse Energy | Viscosity, poises: Temp, 98.9°C 106.5 c | (calculated) 0.586 0.435 |
| Underground: Peak Pressure Impulse Energy | Liquid Density, gm/cc: Temp, 98.9°C 106.5°C Origin: | 1.382 1.375 |
| | Synthesized in 1952 by U.S. Naval Ordnance Labor Maryland. | |

Preparation:

(a, b)

HC-COC1 -со₂сн₂с(мо₂)₂сн₃ AlCla + 2CH₃C(NO₂)₂CH₂OH H-COCL HC-CO2CH2C(NO2)2CH2 3.3 mol 83%yield 7.3 mol 1.6 mol fumaryl chloride 2,2-dinitropropanol aluminum bis(dinitropropyl) fumarate chloride

Dinitropropanol was mixed with chloroform (1320 milliliters) and the mixture heated to boiling. The distillate was collected in a water separator. At first the distillate was cloudy and this was dried with calcium chloride before being returned to the system. When no more water was collected in the water separator, the mixture was cooled to room temperature and the separator removed. Fumaryl chloride was introduced, followed by the aluminum chloride which was added in four equal portions. Air was blown into the flask for a minute to effect mixing, and the reaction sustained itself without the addition of heat for one hour. Steam was gradually introduced so that the reflux temperature was reached 2-1/2 hours after the beginning of the reaction. After 3 hours of reflux, the hot liquid was poured into a bucket. As cooling took place the slurry was vigorously agitated until it finally set up at room temperature. This material was broken up and mixed with dilute ice cold HCL. The solid product was collected on a sintered funnel, washed with water and with hexane. The crude material was recrystallized from methanol to give a product melting at 86° C (uncorrected), but after storage for several days the melting point was 89° C.

References: 20

(a) M. E. Hill, Preparation and Properties of 2,2-Dinitropropanol Esters, NAVORD Report No. 2497, 3 July 1952.

(b) D. L. Kouba and H. D. McNeil, Jr., Hercules Report on High Explosives, Navy Contract Nord-11280, Task A, 26 May 1954.

²⁰See footnote 1, page 10.

| Composition: | Molecular Weight: $(C_{10}H_{14}N_{4}O_{12})$ | 382 | | | |
|--|--|------------|--|--|--|
| % C 31.4 H 3.7 | Oxygen Balance: O, % CO % | -63 -21 | | | |
| $ \begin{array}{c} CH_2CO_2CH_2C(NO_2)_2CH_3 \\ N 14.7 \\ 1 \end{array} $ | Density: gm/cc Crystal | 1.51 | | | |
| $\begin{array}{c} \text{CH}_{2}\text{CO}_{2}\text{CH}_{2}\text{C}(\text{NO}_{2})_{2}\text{CH}_{3}\\ \text{N} 1^{4} \cdot 7 \\ 0 50.2 \text{CH}_{2}\text{CO}_{2}\text{CH}_{2}\text{C}(\text{NO}_{2})_{2}\text{CH}_{3} \end{array}$ | Melting Point: °C | 86 | | | |
| C/H Ratio 0.250 | Freezing Point: °C | | | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | Boiling Point: °C | | | | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₂₀ | | | | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C | o.lo | | | |
| Rifle Bullet Impact Test: Trials % Explosions Partials Burned Unaffected | 120°C 135°C 150°C | | | | |
| | 200 Gram Bomb Sand Test: Sand, gm | | | | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 >400 10 15 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl Ballistic Mortar, % TNT: | | | | |
| 20 | Trauri Test, % TNT: | | | | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method | | | | |
| 100°C Heat lest: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | | | | |
| Flammability Index: | Detonation Rate: Confinement | | | | |
| Hygroscopicity: % | Condition Charge Diameter, in. | | | | |
| Volatility: | Density, gm/cc Rate, meters/second | | | | |

Bis(2,2-Dinitropropyl) Succinate (DNPS)

AMCP 706-177

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | | | | | |
|---|---|---------------------------|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Co Hole Volume Hole Depth | ones | | | | |
| Total No. of Fragments: For TNT | Color: | White | | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib Total No. of Fragments: For TNT | Principal Uses: Method of Loading: | Cast | | | | |
| For Subject HE | Loading Density: gm/cc | | | | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc | Storage: Method | Dry | | | | |
| Blast (Relative to TNT): | Hazard Class (Quontity-Distonce) | | | | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | None | | | | |
| Air, Confined: Impulse Under Water: Peak Pressure | <u>Origin:</u> Synthesized in 1953 by M. E. U.S. Naval Ordnance Laboratory, Maryland. | Hill of the White Oak, | | | | |
| Impulse Energy | | | | | | |
| Underground: Peak Pressure Impulse Energy | | | | | | |

Preparation:

$$\begin{array}{c} 2 \operatorname{CH}_3 \operatorname{C}(\operatorname{NO}_2)_{2}_{\operatorname{CH}^2 \operatorname{OH}} & + \begin{array}{c} \operatorname{CH}_2 \operatorname{COCl} \\ \operatorname{CH}_2 \operatorname{COCl} \end{array} & \xrightarrow{\operatorname{AlCl}_3} & \operatorname{CH}_2 \operatorname{COOCH}_2 \operatorname{C}(\operatorname{NO}_2)_2 \operatorname{CH}_3 \\ \operatorname{CH}_2 \operatorname{COOCH}_2 \operatorname{C}(\operatorname{NO}_2)_2 \operatorname{CH}_3 \end{array} & + 2 \operatorname{Hcl} \\ \operatorname{dinitropropanol} & \operatorname{succinyl} \\ \operatorname{chloride} & \operatorname{chloride} \end{array} & \operatorname{bis}(2,2-\operatorname{dinitropropyl}) \operatorname{succinate} \end{array}$$

A methylene chloride solution of dinitropropanol (0.02 mol in 15 milliliters) was mixed with 0.01 mol of succinyl chloride. To this solution 0.003 mol of crushed anhydrous aluminum chloride was added. It was necessary to cool the reaction vessel due to the vigorousness of the reaction. After 25 minutes at room temperature the reaction solution was refluxed 1-1/2 hours. Fine needle-like crystals formed upon cooling and adding hexane. The crystals were slurried in dilute hydrochloric acid and on recrystallization from methanol gave a 93% yield of DNPS (melting point 85° to 85.6° C).

References: 21

(a) M. E. Hill, Synthesis of New High Explosives, NAVORD Report No. 2965, 1 April 1953.

²¹See footnote 1, page 10.

2,2-Dinitropropyl-4,4,4-Trinitrobutyrate (DNPTB)

AMCP 706-177

| Composition: % | Molecular Weight: $(C_7H_9N_5O_{12})$ 355 |
|---|--|
| ^ю с 23.6 н 2.5 <u>осн₂с(NO₂)₂сн₃</u> | Oxygen Balance: CO, % -29 CO % +2.3 |
| N 19.7 C=0 | Density: gm/cc Crystal 1.68 |
| 0 54.2 CH2CH2C(NO3) | Melting Point: "C Form I 11 Form II 95 Form III 59 |
| C/H Ratio | Freezing Point: °C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | Boiling Point: "C Refractive Index, n ⁰ ₂₀ n ^D ₂₅ n ³⁰ |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C |
| Rifle Bullet Impact Test: Trials % Explosions Partic Is | 120°C 135°C 150°C |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) 1 5 300 10 15 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl Ballistic Mortar, % TNT: |
| 20 | |
| 75°C International Heat Test: % Loss in 48 Hrs | Trauzi Test, % TNT: Plate Dent Test: Method |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT |
| Flammability Index: | Detonation Rate: Confinement |
| Hygroscopicity: % | Condition Charge Diameter, in. |
| Volatility: | Density, gm/cc 1.67 Rate, meters/second 7600 |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | | | |
|---|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | | | |
| Total No. of Fragments: For TNT For Subject HE | Color: White | | | |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: | | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Cast | | | |
| | Loading Density: gm/cc 1.67 | | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | | | |
| Density, gm/cc | Method Dry | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation None | | | |
| Air, Confined: Impulse | $\begin{array}{ccc} \underline{\text{Heat of:}} & (c) & \underline{\text{Solvent}} \\ \hline \text{Transition, cal/gm} & \underline{\text{CCL}}_{\mu} & \underline{\text{DMF}} \\ \text{I} & \longrightarrow \text{III} & 6.2 & 4.8 \end{array}$ | | | |
| Under Water: Peak Pressure Impulse Energy | II I -16.6 -22.0 <u>Heat of Solution, 30⁰C:</u> <u>ΔH Solution, cal/gm</u> <u>Materia 1</u> | | | |
| Underground : Peak Pressure Impulse Energy | Form III 29.5 8.1 Form I 35.6 12.8 Form II 19.1 -9.1 | | | |
| | <u>Origin:</u> Synthesized in 1952 by M. E. Hill of the U.S. Naval Ordnance Laboratory, White Oak, Maryland. | | | |

 $\begin{array}{rcl} {}^{\mathrm{CH}_{3}\mathrm{C}(\mathrm{NO}_{2})_{2}\mathrm{OH}} & + & (\mathrm{NO}_{2})_{3}\mathrm{CCH}_{2}\mathrm{CH}_{2}\mathrm{COCl} & \\ & & & \\ & & \\ \mathrm{dinitropropanol} & & \\$

dinitropropyl trinitrobutyrate

(c)

Dinitropropanol, trinitrobutyryl chloride and aluminum chloride were slowly mixed in carbon tetrachloride at 60° C. This mixture was refluxed at 75° C for two hours. After the reaction was completed, the mixture was cooled and the crystalline product separated and purified. Water in the dinitropropanol was removed by azeotropic distillation before the acid chloride was added. The purified product had a melting point of 95° to 96° C.

Crystallographic Data:

Three distinct crystallographic modifications of DNPTB have been observed. These polymorphs have been characterized by means of X-ray diffraction and microscopic observation. Form I crystallizes from solution in carbon tetrachloride, chloroform, acetone, chloroformhexane, acetone-water, or methanol-water at room temperature. Prolonged standing of Form I at room temperature under the mother liquor promotes a transition to Form 11. Upon solidification of molten DNPTB, Form II is always observed.

| Temperature, | Average Rate, sq inch/hour | | Standard Deviation | Average Rate, mm/hour |
|--------------|-------------------------------|---|-----------------------|--------------------------|
| 15 | 0.347 | 1 | 0.036 | 0.012 |
| 20 | 0.435 | | 0.025 | 0.128 |
| 25 | 0.452 | | 0.048 | 0.133 |
| 30 | 0.475 | | 0.049 | 0.140 |
| 35 | 0.253 | | 0.037 | 0.075 |

Both Forms I and III gave very erratic sensitivity values. The high temperature polymorph, Form II of DNPTB, gave consistent sensitivity values.

References: 22

(a) M. E. Hill, <u>Preparation and Properties of 2,2-Dinitropropanol Esters</u>, NAVORD Report No. 2497, 3 July 1952.

(b) W. B. Hewson, Hercules Report on High Explosives. Navy Contract Nord-11280, Task A, 18 October 1954.

(c) J. R. Holden and J. Wenograd, <u>Physical Properties of an Experimental Castable Explo</u>sive 2,2-Dinitropropyl 2,4,4-Trinitrobutyrate DNPTB, NAVORD Report No. 4427, **11** December 1956.

²²See footnote 1, page 10.

| Composition: | Molecular Weight: $(C_7H_6N_2O_4)$ | 1.82 |
|---|--|--------------|
| $^{\%}$ $^{CH}_3$ c 46.3 $^{NO}_2$ | Oxygen Balance: O, % CO % | -114 - 53 |
| N 15.4 | Density: gm/cc | 1.521 |
| 0 35.0 NO ₂ | Melting Point: "C | 71 |
| C/H Ratio 0.579 | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in | Boiling Point: °C Decomposes Refractive Index, n ⁰ ₂₀ n ⁰ ₂₅ | 300 |
| Sample Wt, mg | n ₃₀ | |
| Friction Pendulum Test: Steel Shoe Unaffected Fiber Shoe Unaffected Rifle Bullet Impact Test: Trials % 0 Portials 0 | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C 120°C 135°C 135°C 150°C | 0.04 |
| Burned 0 Unaffected 100 | 200 Gram Bomb Sand Test: Sand, gm | 19.3 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Decomposes 310 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminote Lead Azide | 0.20 |
| 10 | Tetryl | 0.25 |
| 15 20 | Ballistic Mortar, % TNT: (a) | 71 |
| 75°C International Heat Test: % Loss in 48 Hrs | Trauzl Test, % TNT: (b) Plate Dent Test: Method | 64 |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement | |
| Hygroscopicity: % 25°C, 100% RH 0.00 | Condition Charge Diameter, in. Density, gm/cc | |
| Volatility: | Rote, meters/second | |

2,4-Dinitrotoluene (DNT)

| fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | | | |
|---|---|-------------------------|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Hole Volume Hole Depth | Cones | | |
| Total No. of Fragments: For TNT | Color: Y | <i>C</i> ellow | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Ingredient of propellant powder, dynamites and plastic explosives | | | |
| Total No. of Fragments: For TNT | Method of Loading: Pressed, ext composition | ruded or cast | | |
| For Subject HE | Loading Density: gm/cc | Variable | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | | | |
| Density, gm/cc | Method | Dry | | |
| Blost (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 12 | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | Group D | | |
| Air, Confined: Impulse | 65.5 ⁰ C KITest: Minutes | 60+ | | |
| Under Water: Peak Pressure Impulse Energy | Heat of: Combustion, cal/gm (b) Thermal Conductivity: | 1545 | | |
| Underground: Peak Pressure Impulse Energy | cal/sec/cm/ ^o C Density 1.322 gm/cc | 6.28 x 10 ⁻⁴ | | |
| | | | | |

Preparation:

See TMT.

Solubility: gm/100 gm of the following substances.;

| Ethyl | <u>30%</u> Alcohol | Nitrog | glycerin | | Water | |
|----------------------------|--------------------------------------|-----------|----------|------------------------|-------------------------|--|
| <u>°c</u> | <u>%</u> | <u>oc</u> | K | <u>oc</u> | Ľ | |
| 25 35 45 55 60 | 0.16 0.29 0.49 0.77 1.03 | 20 | 30 | 22 50 100 | 0.027 0.037 0.254 | |

Solubility at 15°C, in:

| Solvent | <u>%</u> | Solvent | 20 |
|---|----------|------------------------|--------|
| $\begin{array}{c} \overset{\mathrm{CHCl}}{_{\mathrm{Ccl}}}_{4} \\ \overset{\mathrm{CcHc}}{_{\mathrm{CfHc}}} \\ \mathrm{Toluol} \\ \overset{\mathrm{CHC}}{_{\mathrm{CcHc}}}_{2\mathrm{H}_{5}\mathrm{CH}} (96\%) \end{array}$ | 65.076 | ତ୍ର୍ୟୁକୁଡିH (absolute) | 3.039 |
| | 2.431 | Ether (absolute) | 9.422 |
| | 60.644 | Acetone | 81.901 |
| | 45.470 | Ethyl acetate | 57.929 |
| | 5.014 | CS ₂ | 2.306 |
| | 1.916 | Pyridine | 76.810 |

Origin:

Occurs as 75% of the products obtained on the nitration of toluene, the remaining 25% being mainly 2,6-DNT and other isomers of DNT. Also occurs as an impurity in crude TNT obtained by standard manufacturing process. Used in explosive mixtures at least since 1931.

References: 23

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives, Part III - Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, <u>OSRD Report No. 5/46</u>, 27 December 1945.

(b) A. H. Blatt, <u>Compilation of Data on Organic Explosives</u>, OSRD Report No. 2014, 29 February 1944.

- (c) Report AC-2861.
- (d) Also see the following Picatinny Arsenal Technical Reports on DNT:

| <u>o</u> | <u>1</u> | 2 | 3 | 4 | 5 | <u>م</u> | ヱ | 8 | 9 |
|-------------|---|--|--|--|--------------|-----------------------------|------------------|--------------------|--|
| 810 1830 | 1351 1501 1651 1781 1821 2031 2221 | 72 372 922 1142 1672 1692 | 43 233 673 1023 1663 1743 2013 | 394 804 1044 1094 1164 1324 1464 1524 1674 1754 2094 | 1615 2125 | 186 1556 1816 1896 | 97 817 837 | 768 938 1538 | 69 149 249 279 779 1749 |

23See footnote 1, page 10.

| Composition : | Molecular Weight: $(C_{10}H_{16}N_{6}O_{19})$ 554 |
|--|--|
| % C 21.7 H 2.9 N 15.2 ONO ₂ ONO ₂ O 60.2 I 2 ¶ ² | Oxygen Balance: CO, % -26 CO % + 3 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | Density: gm/cc Crystal 1.63 |
| $ON_2OCH_2C - CH_2 - O - CH_2 - CH_2ONO_2$ | Melting Point: "C 73.7 |
| \dot{c}_{1}^{H} \dot{c}_{2}^{H} | Freezing Point: "C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 1 ¹ 4 | Boiling Point: "C |
| Bureau of Mines Apparatus, cm 1 ¹ 4 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. ¹ 4 Sample Wt, mg 10 | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ |
| Friction Pendulum Test: | Vacuum Stability Test: |
| Steel ShoeExplodesFiber ShoeUnaffected | cc/40 Hrs, at 90°C |
| Rifle Bullet Impact Test: Trials | 100°C 3.7 |
| w | 120°C 11+ 135°C |
| Explosions | 150°C |
| Partio Is Burned | 200 Gram Bomb Sand Test: |
| Unaffected | Sand, gm 57.4 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 300 5 Explodes 255 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl |
| 15 20 | Ballistic Mortar, % TNT: (a) 142 |
| | Trauzi Test, % TNT: (b) 128 |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method |
| 100°C Heat Test: | Condition |
| % Loss, 1st 48 Hrs 0.11 | Confined Density, gm/cc |
| % Loss, 2nd 48 Hrs 0.10 | Brisance, % TNT |
| Explosion in 100 Hrs None | () |
| Flammability Index: | Confinement Copper tube |
| Hygroscopicity: % 0.03 | Condition Pressed Charge Diameter, in. 0.39 |
| Volatility: | Density, gm/cc 1.59 Rate, meters/second 7410 |

| Fragmentation Test: | Shaped Charge Effectiveness, TNT = 100: | | |
|--|---|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, lb | Glass Cones Steel Cones Hole Volume Hole Depth | | |
| Total No. of Fragment s: For TNT | Color: White | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Ingredient of priming compositions | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pressed | | |
| | Loading Density: gm/cc | | |
| Fragment Velocity: ft/sec | At 3000 to 4000 psi 1.59 | | |
| At 9 ft At 25½ ft | Storage: | | |
| Density, gm/cc | Method Dry | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) $Class 9$ | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | | |
| Air, Confined: Impulse | Preparation: (Chemistry of Powder and Explosives, Davis) | | |
| Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | 2(H0-CH ₂) ₄ C <u>Dehydration</u> (H0-CH ₂) ₃ C-O-C(CH ₂ -OH) ₃ (O ₂ NO-CH ₂) ₃ C-O-C(CH ₂ -ONO ₂) ₃ Dipentaerythritol Hexanitrate is procured in the pure state (melting point 72°C) by fractional crystallization of crude PEIN from moist acetone. <u>Origin:</u> Formed as an impurity in the prepa- ration of PEIN. Properties first described by W. Frederick and W. Brün in 1930 (Berichte <u>63</u> , 2861 (1930); Z. ges Schiess- Sprengstoffw 27, 73-6, 125-7, 156-8 (1932)) | | |
| | $\frac{\text{Heat of:}}{\text{Combustion, cal/gm}} = 2260$ | | |

References: 24

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III - Miscellaneous</u> <u>Sensitivity Tests</u>: <u>Performance Tests</u>, OSRD Report No. 5746, 27 December 1945.

(b) A. Stettbacher, <u>Die Schiess und Sprengstoffe</u>, Leipsiz, p. 363.

(c) T. L. Davis, The Chemistry of Powder and Explosives, John Wiley and Sons, Inc., Nav York (1943) pp. 218-283.

(d) S. Livingston, <u>Characteristics of Explosives HMX and DPMN</u>, PAIR No. 1561, 6 September 1945.

²⁴See footnote 1, page 10.

| Composition: 99.5/0.5 RDX/1-MA dye* 17.5 | Molecular Weight: |
|---|--|
| % TNT 67.8 Tripentaerythritol 8.6 68/32 Vistac No 1/DOS binders* 4.1 | Oxygen Balance: CO, % CO % |
| Cellulose acetate, LH-1 2.0 *RDX, Class E; 1-MA is 96% pure 1-methylamino- anthraquinone. | Density: gm/cc Loading 0,9 |
| **Vistac No 1 is low MW polybutene; DOS is dioctylsebacate. | Melting Point: "C |
| C/H Ratio | Freezing Point: "C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | Boiling Point: "C |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 22 | Reftactive Index, n ^D ₂₀ |
| Sample Wt, mg 19 | n ^D 23 |
| | n ^D ₃₀ |
| Friction Pendulum Test: | Vacuum Stability Test: |
| Steel Shoe Unaffected | cc/40 Hrs, at 90°C |
| Fiber Shoe Unaffected | 100°C |
| Rifle Bullet Impact Test: Trials | 120°C 0.90 |
| % Explosions | 135°C |
| Portials | 150°C |
| Burned | 200 Grom Bomb Sand Test: |
| Unaffected | 10.5 |
| | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) | Sensitivity to Initiation: Minimum Detonating Charge, gm |
| 1 | Mercury Fulminate |
| 5 Ignites 480 | Lead Azide 0.20 |
| 10 | Tetryl 0.15 |
| 15 | Ballistic Mortar, % TNT: |
| 20 | Treuzi Test, % TNT: |
| 75°C International Heat Test: | IFGUZI JEST, % INT. |
| % Loss in 48 Hrs | Plate bent Test: Method |
| 100°C Heat Test: | Condition |
| % Loss, 1st 48 Hrs | Confined |
| % Loss, 2nd 48 Hrs | Density, gm/cc |
| Explosion in 100 Hrs | Brisance, % TNT |
| Flammability Index: | Detonation Rate: |
| | Confinement None |
| Hyproscopicity: % 0.31 71°C, 95% RH, 30 days Satisfactory | Condition Hand tamped Charge Diameter, in. 1.25 |
| 71°C, 95% RH, 30 days Satisfactory Volatility: | Density, gm/cc 0.9 |
| | Rote, meters/second 4397; or 14400 ft/sec |

L

Dynamite, Low Velocity, Picatinny Arsenal (LVD)

| Fragmentation Test: | Shaped Charge Effectiveness, TNT $=$ 100: | | | |
|---|--|---|--|--|
| 90 mm HE, M71 Projectile, Lot WÇ-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Co Hole Volume Hole Depth | nes | | |
| Total No. of Fragments: For TNT | Color: | Pink | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib Total No. of Fragments: For TNT | Principal Uses: Excavation, demo and cratering Method of Loading: Hall Packer mac | | | |
| For Subject HE Fragment Velocity: ft/sec | Loading Density: gm/cc Tamped cartridge 1-1/2" diamete | 0.9 r, 8" long | | |
| At 9 ft At 25½ ft Density, gm/cc | Storage: Method | Dry | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | Group A | | |
| Air, Confined: Impulse | Sensitivity to Initiation: Stick dry, No. 6 Electric cap Stick dry, Corps of Engineers Stick wet, Corps of Engineers | Positive Positive Positive | | |
| Under Water: Peak Pressure Impulse Energy | Air Gap Propagation: Max distance will, inch min distance will not, inch Stick Water Immersion: | 2-1/2 3 | | |
| Underground: Peak Pressure Impulse Energy | Weight gain, % <u>Heat of:</u> Explosion, cal/gm Gas Volume, cc/gm <u>Cold Storage:</u> Plastic to Low Temperature Usage: -65°F, 1 day, M2 cap | 9-16 625 611 -65°F tisfactory | | |

Preparation:

To date this dynamite has been prepared on a laboratory scale, the details of which are classified, It has been shown, however, to be machine loadable on a Hall packing machine,

Origin:

Nobel invented the original dynamite in 1866 and gave the name dynamite to mixtures of nitroglycerin and kieselguhr. The strength of a dynamite was indicated by the percentage of NG in the mixture. Later oxidants and combustibles were substituted for the kieselguhr, and ammonium nitrate and/or nitrostarch replaced the NG, bringing into existence new types of dynamites. World War II military operations required special demolition and cratering explosives free from the objectionable characteristics of NG and many "dynamite substitutes" were developed for specific applications. The subject low velocity dynamite was developed in 1956 by Picatinny Arsenal (Ref a).

References: 25

(a) H. W. Voigt, <u>Development of Low-Velocity Military Explosives Equivalent to Commercial</u> Dynamites, PA Technical Report 2374, March 1957.

(b) Also see the following Picatinny Arsenal Technical Reports on Dynamites:

| <u>o</u> | 1 | 2 | 4 | ٤ | <u>6</u> | ユ | 8 | <u>9</u> |
|------------------------------|--------------|-------------|-------------|------|-------------------------------------|------------|-------------|----------|
| 1260 1360 1720 1760 | 1381 1611 | 782 1532 | 864 1464 | 1285 | 1416 1436 1506 2056 | 507 957 | 848 1828 | 1819 |

²⁵See footnote 1, page 10.

| Composition: | Molecular Weight: | |
|--|---|-------|
| % RDX 75 TIVT 15 Starch 5 | Oxygen Balance: CO, % -51 CO % | |
| SAE No. 10 0 i l 4 Vistanex o i l gel* 1 | Density: gm/cc Loading 1.1 | |
| 80/15/5, SAE No. 10 weight o 1/Vistanex B- | Melting Point: °C | |
| 120XC/Navy D2 wax. C/H Ratio | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: | Nitroglycerin Equivalent, 🖇 60 | |
| Bureau of Mines Apparatus, cm >100 Sample Wt 20 mg 18 | Refractive Index, n ^D ₂₀ | |
| Picatinny Arsenal Apparatus, in. 25 | n ^D ₂₅ | |
| Sample Wt, mg | n ₃₀ | |
| Friction Pendulum Test: | Vacuum Stability Test: | |
| Steel Shoe Crackles | cc/40 Hrs, at | |
| Fiber Shoe Unaffected | 90°C | |
| Rifle Bullet Impact Test: Trials | 100°C 0.80 120°C 0.94 | |
| % | | |
| Explosions 0 | 135°C | |
| Partials 0 | 150°C | |
| Burned 10 | 200 Gram Bomb Sand Test: | |
| Unaffected 90 | Sand, gm 52.6 | |
| Explosion Temperature: °C | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) | Minimum Detonating Charge, gm | |
| 1 | Mercury Fulminate | |
| 5 | Lead Azide 0.20 | |
| 10 | Tetryl 0.10 | |
| 15 | Ballistic Mortar, % TNT: 122 | |
| 20 | | |
| 75°C International Heat Test: | Plate Dent Test: | |
| % Loss in 48 Hrs | Method | |
| | Condition | |
| 100°C Heat Test: | Confined | |
| % Loss, 1st 48 Hrs 0.62 % Loss, 2nd 48 Hrs 0.12 | Density, gm/cc | |
| Explosion in 100 Hrs None | Brisance, % TNT | |
| | Detonation Rate: | |
| Flammability Index: | Confinement None | |
| · · ·································· | Condition Machine ta | amped |
| Hygroscopicity: % | Charge Diameter, in. 1.50 | |
| 71°C, 95% RH, 30 days Satisfactor | | |
| Volatility: | Rate, meters/second 6000-6600; or 20, | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | | |
|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | | |
| Total No. of Fragments: For TNT | Color: Buff | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, 1b | Principal Uses: Excavation, demolition, and cratering | | |
| Total No. of Fragments: For TN T For Subject HE | Method of Loading: Hall Packer machine loaded | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Loading Density: gm/cc 1.1 Cartridge 1-1/2" diameter, 8" long Storage: | | |
| Density, gm/cc | Method Dry | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) $ m Class~9$ | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Group A | | |
| Air, Confined: Impulse | Sensitivity to Initiation: Stick dry, No. 6 Electric cap Positive Stick dry, Corps of Engineers Positive Stick wet, Corps of | | |
| Under Water: Peak Pressure Impulse Energy | Engineers > 50% Positive <u>Air Gap Propagation:</u> <u>Max distance will</u> , inch 1 <u>Min distance will not</u> , inch 2-1/2 Quarry Performance: 4 tons rock/ton | | |
| Underground: Peak Pressure Impulse Energy | explosiveStick Water Immersion:Weight gain, %25-27Heat of: Explosion, cal/gm935Gas Volume, cc/gm945Cold Storage:Plastic to -70°FLow Temperature Usage: | | |
| • | -65°F, 1 day, M2 cap crimper Satisfactory | | |

Preparation:

Manufactured on standard dynamite line and packaged on a Hall packing machine. Details of handling materials and techniques of manufacture are classified.

Orinin:

Military forces frequently require excavation, demolition, and cratering operations for which standard high explosives are unsuitable. Commercial blasting explosives, except black powder, are called dynamites although they may contain no nitroglycerin. The subject dynamite substitute was developed in 1952 by the Hercules Powder Company (Ref a).

References: 26

(a) W. R. Baldwin, Jr., <u>Blasting Explosives (Dynamite Substitute)</u>, Hercules Powder Company Formal Progress Report, RI 2086, 15 August 1952, Army Contract DA-36-034-0RD-110.

(b) H. W. Voigt, <u>Development of Low-Velocity Military Explosives Equivalent to Commercial</u> Dynamites, PA Technical Report No. 2374, March 1957.

²⁶See footnote 1, page 10.

EC Blank Fire

| Composition: % | Molecular Weight: Approximately 503 |
|--|--|
| Nitrocellulose, 13.25% N 80 Barium Nitrate 8 Potassium Nitrate 8 | Oxygen Balance: $\begin{array}{c} & & & +5 \\ & & & & -25 \end{array}$ |
| Starch 3 Diphenylamine 0.75 | Density: gm/cc |
| Aurine 0.25 | Melting Point: "C |
| C/H Ratio | Freezing Point: "C |
| Impact Sensitivity 2 K with ty, z Kg with Bureau of Mines Apparatus, cm <u>19</u> Sample Ma 20 | Boiling Point: °C |
| Sample Wit Zu ma Picatibhy Arsenal Apparatus, in. Sample Wt, mg 20 | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ |
| Friction Pendulum Test: Steel Shoe Snaps Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C |
| Rifle Bullet Impact Test: Trials % Explosions | 100°C 120°C 135°C |
| Partials Burned | 150°C |
| Unaffected | 200 Gram Bomb Sand Test: Sand, gm 46.8 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) ¹ ⁵ Decomposes 200 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate 0.22 Lead Azide Tetryl |
| 15 20 | Ballistic Mortar, % TNT: |
| /5°C International Heat Test; | Trauzi Test, % TNT: |
| % Loss in 48 Hrs 1.8 | Plate Dent Test: Method |
| 100°C Heat Test: % Loss, 1st 48 Hrs 2.0 % Loss, 2nd 48 Hrs 0.2 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT |
| Flammability Index: | Detonation Rate: Confinement |
| Hygroscopicity: % 30°C, 90% RH 6.2 | Condition Charge Diameter, in. |
| Volatility: | Density, gm/cc Rate, meters/second |

| Fragmentation Test: | Shaped Charge Effectiveness, TNT = 1 | 00: |
|--|---|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel C Hole Volume Hole Depth | Cones |
| Total No. of Fragments: For TNT | Color: | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, 1b | Principal Uses: Grenades; caliber | .30 blank |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: | Loose |
| Fragment Velocity: ft/sec | Loading Density: gm/cc | 0.40 |
| At 9ft At 25½ ft | Storage: | |
| Density, gm/cc | Method | W e t |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class O |
| Air: Peak Pressure | Compatibility Group | Group J |
| Impulse Energy | Exudation | |
| Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy | Preparation: EC Blank Fire is a colloided propellant manufac cess using either acetone an mixture of butyl acetate and gelatinize only a part of th lose. The process is contro the product passes through a and is retained on a No. 50 | tured by a pro- d ethanol or a benzene to e nitrocellu- lled so that No. 12 sieve |
| Underground: Peak Pressure Impulse Energy | Origin: Invented in 1882 as bulk spo less) powder by W. F. Reid and the Explosive Company (whence t in England (British Patent 619) | D. Johnson at he name "EC") |
| References: ²⁷ (a) See the following Picatinny Arsenal Technical Reports on EC Blank Fire: 891 901, 372, 512, 822, 233, 1373, 854, 65, 667, 817, 69, 579 and 1399. | 120 [°] C Heat Test: Salmon Pink Red Fumes Explodes | Minutes 150 300+ 300+ |

²⁷See footnote 1, page 10.

Ednatol, 55/45

| Composition: | Molecular Weight: | 178 |
|---|--|----------------|
| % | Oxygen Bulonce: | |
| Haleite (Ethylene Dinitramine) 55 | CO. % | -51 -17 |
| INT 45 | CO % | -11 |
| | Density: gm/cc Cast | 1.62 |
| | Metring Point: "C Eutectic | 80 |
| C/H Ratio | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt; | Bailing Point; °C | |
| Bureau of Mines Apparatus, cm. 95 Sample Wt 20 mg | Refractive Index, n20 | |
| Picotinny Arsenol Apparatus, in. | h25 | |
| Sample Wt, mg 20 | n ^D ₃₀ | |
| | ¥130 | |
| Friction Pendulum Test: Steel Shoe Unaffected | Vacuum Stability Test: | |
| | cc/40 Hrs, at 90°C | |
| Fiber Shoe Un affected | - 100°C | 1.0 |
| Rifle Bullet Impact Test: Trials | 120°C | 11+ |
| ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | 135°C | |
| Explosions 0 Partials 0 | 150°C | |
| Burned 7 | 200 Gram Bamb Sand Test: | |
| Unaffected 93 | | 49.4 |
| + | Sand, gm | |
| Explosion Temperature: °C | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) 435 1 248 | Minimum Detonating Charge, gm Mercury Fulminate | |
| 5 Decomposes 190 | Lead Azide | 0.22* 0.26* |
| 10 183 | *Alternative initiating charp | |
| 15 176 | | , |
| 20 168 | Ballistic Mortar, % TNT: (a) | 119 |
| *Composition Haleite/INT, 60/40. | Trouzi Teat, % TNT: (b) | 120 |
| 75°C International Heat Test: % Loss in 48 Hrs | Plote Dent Test: | 52/48 |
| | Method | В |
| 100°C Heat Test: | Condition | Cast |
| % Loss, 1st 48 Hrs 0.2 | Confined | No |
| % Loss, 2nd 48 Hrs 0.1 | Density, gm/cc | 1.62 |
| Explosion in 100 Hrs None | Brisance, % TNT | 112 |
| | Detonation Rote: | |
| Flammability Index: Will not continue to burn | Confinement | None |
| | Condition | Cast |
| Hygroscopicity: % None | Charge Diameter, in. | 1.0 |
| Volatility: | Density, gm/cc | 1.63 72ko |
| V0 | Rate, meters/second | 7340 |

| Fragmentation Test: 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc 1.56 1.62 | | | Shaped Charge Effectiveness, $TNT = 100$: $50/50$ Glass Cones Steel Cones Hole Volume 126 123 | | |
|---|--------------------------|-------------|--|----------------|--|
| | | | | | |
| Total No. of Fragments : For TNT | 70 3 | 703 | Color: | Yellow | |
| For Subject HE | 842 | 902 | Principal Uses: Projectiles, bor | nbs; special | |
| 3 inch HE, M42A1 Projectile, | Lot KC-5: | | ammunition comp | onents | |
| Density, gm/cc | | 1.60 | | | |
| Charge Wt, Ib | | 0.845 | | | |
| Total No. of Fragments: For TNT | | 514 | Method of Looding: | Cast | |
| For Subject HE | | 536 | | | |
| • | | | Loading Density: gm/cc | 1.65 | |
| Fragment Velocity: ft/sec | | 2730 | | | |
| At 9 ft At 25½ ft | | 2430 | Storage: | | |
| Density, gm/cc | | 1.62 | Method | Dry | |
| Blast (Relative to TNT): | Blast (Relative to TNT): | | Hazard Closs (Quantity-Distance) | Class 9 | |
| Air: | | | Compatibility Group | Group I | |
| Peak Pressure | | 108 | | | |
| Impulse | | 110 | Exudation Does no | t exude at 65° | |
| Energy | | 108 | | | |
| Air, Confined: | | | Eutectic Temperature, ^O C: | 79.8 | |
| Impulse | | | gm Haleite/100 gm TNT 79.8°C | 0.48 | |
| | | | 95.0°C | 1.12 | |
| Under Water: Peak Pressure | | | Compatibility with Metals: | | |
| Impulse | | | Brass, aluminum, stain المنتخط | | |
| Energy | | 113 | mild steel, mild steel coated proof black paint, and mild st | eel plated | |
| Underground: Peak Pressure | | | with cadmium or nickel are una per, magnesium, magnesium-alum mild steel plated with copper | inum alloy an | |
| Impulse | | | slightly affected. | | |
| Energy | | | Wet: Copper, brass, magnesiu | | |
| Booster Sensitivity Tes | st: | (d) | aluminum alloy, mild steel, mi with acid-proof black paint an | | |
| Condition Totryl m | | Cast 100 | plated with copper, cadmium, n | ickel or zinc | |
| Tetryl, gm Wax, in. for 50% Deto | nation | 1.28 | are heavily attacked. Aluminu | n is slightly | |
| Density, gm/cc | | 1.62 | affected and stainless steel i | s unaffected. | |

Preparation:

Wet Haleite is added slowly to molton TNT heated at about 100° C in a steam jacketed melting kettle equipped with a stirrer. Heating and stirring are continued until all moisture is evaporated. Loading is done by pouring the mixture cooled to 85° C.

Origin:

Mixtures of Haleite (EDNA) and TNT, designated Ednatol, were developed at Picatinny Arsenal just prior to World War II.

References: 28

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III</u> - <u>Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, OSRD Report No. 5746, 27 December 1945.

(b) Philip C. Keenan and Dorothy C. Pipes, <u>Table of Military High Explosives</u>, Second Revision, NAVORD Report No. 87-46, 26 July 1946.

(c) D. P. MacDougall, <u>Methods of Physical Testing</u>, OSRD Report No. 803, 11 August 1942.

(d) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute for</u> <u>Tetryl in Boosters</u>, NOL Mano 10,303, 15 June 1949.

(e) W. R. Tomlinson, Jr., <u>Blast Effects of Bomb Explosives</u>, PA Tech Div Lecture, 9 April 1948.

(f) Eastern Laboratory, du Pont, <u>Investigation of Cavity Effect</u>, See III, Variation of <u>Cavity Effect with Composition</u>, NDRC Contract W-672-ORD-5723.

(g) Eastern Laboratory, du Pont, <u>Investigation of Cavity_Effect</u>, Final Report, 18 September 1943, NDRC Contract W-672-ORD-5723.

(h) Also see the following Picatinny Arsenal Technical Reports on Eduatol:

| <u>0</u> | 1_ | 2 | <u>3</u> | 4 | 5 | 6 | <u>7</u> | 8 | <u>2</u> |
|------------------------------|----------------------|----------------------|----------------------|--------------|----------------------|------|------------------------------|----------------------|--------------|
| 1290 1400 1420 1530 | 1291 1451 1651 | 1162 1372 1482 | 1193 1363 1493 | 1294 1434 | 1325 1395 1885 | 1796 | 1457 1477 1737 1797 | 1198 1388 1838 | 1279 1469 |

²⁸See footnote 1, page 10.

| Composition: | Molecular Weight: $(C_{10}H_{12}N_6O_{16})$ | 468 |
|--|---|--------------|
| % с 25.6 н 2.6 | Oxygen Balance: CO, % CO % | - 34 0 |
| $\begin{array}{c} \mathbb{N} 17,1 \\ \mathbb{CH}_2^{CO_2 CH_2 CH_2 CH_2 C}(\mathbb{N}O_3) \\ \mathbb{CH}_2^{CO_2 CH_2 CH_2 C}(\mathbb{N}O_3) \end{array}$ | Density: gm/cc Crystal | 1.63 |
| $o 54.7$ $cH_2 cO_2 cH_2 cH_2 c(NO_3)$ | Melting Point: °C | 96 |
| C/H Ratio 0.235 | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | Boiling Point: "C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| Friction Pendulum lest: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C | |
| Rifle Bullet Impact lest: Trials % Explosions Partials Burned Unaffected | 120°C 135°C 150°C | |
| | 200 Gram Bomb Sand lest: Sand, gm | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 550% point 230 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl | |
| 15 20 | Ballistic Mortar, % TNT: | |
| | Trauzi lest, % TNT: | |
| 75°C International Heat lest: % Loss in 48 Hrs 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Plate Dent lest: Method Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement | |
| Hygroscopicity: % | Condition Charge Diameter, in. | |
| Volatility: | Density, gm/cc Rate, meters/second | 1.63 7340 |

Ethylene Glycol Di-Trinitrobutyrate (GTNB)

| Fragmentation Test : | Shaped Charge Effectiveness, TNT = $'$ | 100: | | |
|---|---|----------------|--|--|
| 90 mm ME, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | | | |
| Total No. of Fragments: For TNT | Color: | | | |
| For Subject HE | Principal Uses: Casting medium for HE comp | | | |
| 3 inch Hf, M42A1 Projectile, Lot KÇ-5; Density, gm/cc | | | | |
| Charge Wt, Ib | | | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: | Cast | | |
| | Loading Density: gm/cc | 1.60 | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | | | |
| Density, gm/c c | Method | Dry | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | None | | |
| Air, Confined: Impulse | Preparation: (a) By the addition of nitroform to ethylene glycol diacrylate. As the method of prepa- ration often leads to products difficult to purify , a preparation from ethylene glycol and pure trinitrobutyric acid is in process. | | | |
| Under Water: Peak Pressure Impulse | | | | |
| Energy | <u>Origin:</u> | | | |
| Underground: Peak Pressure Impulse | First synthesized in 1951 b Rubber Company, Research and D General Laboratories, Passaic, | Development | | |
| Energy | Viscosity, poises: | | | |
| | Тетр, 98.9 ⁰ с 106.5°с | 0.246 0.193 | | |
| | Liquid Density, gm/cc: Temp, 98.9°C 106.5°C | 1.467 1.459 | | |

References:29

(a) U. S. Rubber Company Progress Report No. 14, Navy Contract Nord-10129, 1 February 1951 to 1 May 1951.

(b) U. S. Naval Ordnance Laboratory, Silver Spring, Maryland, Letter from Dr. O. H. Johnson to Commanding Officer, Picatinny Arsenal, 8 April 1955 (ORDBB 471.86/44-3, Registry No. 39815); and NOL Letter from Dr. D. V. Sickman to Commanding Officer, Picatinny Arsenal, 29 November 1955 (ORDBB 471.86/159-1; Serial No. 02894).

²⁹See footnote 1, page 10.

| Composition: % | Molecular Weight: $(C_{6}H_{6}N_{4}O_{7})$ | 246 |
|---|--|----------------|
| C 29.3 $0 - NH_{1_4}$ H 2.4 $0_2N - NO_2$ | Oxygen Balance: OO, % CO % | -52 -13 |
| N 22.7 | Density: gm/cc Crystal | 1.72 |
| 0 45.6 | Melting Point: "C Decomposes | 265 |
| C/H Ratio 0.317 | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | Boiling Point: "C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 17 | Refractive Index, n ^D ₂₀ a _O | 1.508 |
| Sample Wt, mg 18 | þ _o | 1.870 1.907 |
| Friction Pendulum lest: Steel Shoe Unaffected Fiber Shoe Unaffected | Vacuum Stability lest: cc/40 Hrs, at 90°C | |
| Rifle Bullet Impact lest: Trials | 100°C | 0.2 |
| % | 120°C 135°C | 0.4 |
| Explosions 0 | 150°C | 0.4 |
| Partiols 0 Burned 30 | | |
| Unaffected 70 | 200 Gram Bomb Sand lest: Sand, gm | 39.5 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 405 1 367 5 Decomposes 318 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate | |
| 10 314 | Lead Azide | 0.20 |
| 15 299 | Tetryl | 0.06 |
| 20 295 | Ballistic Mortar, % TNT: (a) | 99 |
| 75°C International Heat lest: | _ Trauri lest, % TNT: | |
| % Loss in 48 Hrs | Plate Dent lest: Method | A |
| 100°C Heat lest: | Condition | Pressed |
| % Loss, 1st 48 Hrs 0.1 | Confined | Yes |
| % Loss, 2nd 48 Hrs 0.1 | Density, gm/cc | 1.50 |
| Explosion in 100 Hrs None | Brisance, % TNT | 91 |
| Flammability Index: | Detonation Rate: Confinement | None |
| Hygroscopicity: % 100% RH 0.1 | Condition Charge Diameter, in | Pressed |
| | Density, gm/cc | 1.0 1.55 |
| Volatility: | | 6850 |
| 1 | Rate, meters/second | 0000 |

| Fragmentation Test: | | Shaped Charge Effectiveness, TNT = | 100: |
|---------------------------------|---------|---|---------------------------|
| 90 mm HE, M71 Projectile, Lot V | NC-91: | Glass Cones Steel | Cones |
| Density, gm/cc | 1.50 | Hole Volume | |
| Charg e Wt, Ib | 1.94 | Hole Depth | |
| Total No. of Fragments: | | Color: Ye | ellow-orange |
| For TNT | 703 | | or or unge |
| For Subject HE | 649 | Principal Uses: AP projectiles | and bombs |
| 3 inch HE, M42A1 Projectile, Lo | t KC-5: | | |
| Density, gm/cc | 1.55 | | |
| Charge Wt, Ib | 0.82 | | |
| Total No. of Fragments: | | Method of Loading: | Pressed |
| For TNT | 514 | J | |
| For Subject HE | 508 | | |
| | | Loading Density: gm/cc psix1 | .0 ⁻⁵ 15 20 |
| Fragment Velocity: ft/sec | | 1.33 1.41 1.47 1.49 | 1.51 1.53 |
| At 9 ft At 25½ ft | | Storage: | , <u></u> |
| Density, gm/cc | | Method | Dry |
| Blast (Relative to TNT): | | Hazard Class (Quantity-Distance) | Class 9 |
| Air: | | Compatibility Group | Group I |
| Peak Pressure | | E | (65 0a |
| Impulse | | Exudation Nor | ne at 65°C |
| Energy | | | |
| Air, Confined: | | Sensitivity to Electrostatic | (-) |
| Impulse | | Discharge, Joules: | (d) |
| | | Through 100 Mesh: | |
| Under Water: | | Confined | 6.0 |
| Peak Pressure | | Unconfined | 0.025 |
| Impulse - | | Booster Sensitivity Test: | (c) |
| Energy | | Condition | Pressed |
| Underground: | | Tetryl, gn Way in fan 50% Detensti | 100 am 1 97 |
| Peak Pressure | | Wax, in. for 50% Detonati Density, gm/cc | on 1.27 1.54 |
| Impulse | | Heat of: | |
| Energy | | | 2900 |
| | | Combustion, cal/gm Explosion, cal/gm | 2890 800 |
| | | Formation, cal/gm | 395 |
| | | | |
| | | | |

Preparation:

Explosive D is manufactured by suspending picric acid in hot water and neutralizing it with gaseous or liquid ammonia. As the picrate is formed, it goes into solution; on cooling, it precipitates. An excess of ammonia leads to formation of the red form of ammonium picrate. This should be avoided. The separated crystals are washed with cold water and dried.

Effect of Storage on Sand Test Values:

| | <u>Minimum</u> Detonating <u>Charge</u> | | | | | |
|--------------------------------|---|-------------------------------------|----------------------|----------------------------------|--|--|
| <u>Stor</u> Years | <u>age</u> C | <u>Mercury</u> Fulminate (gm) | Tetryl (gm) | Crushe (gm) | | |
| 0 3.5 2 * 4 * 2 ** | 50 Normal Nomal 50 | 0.25 0.24 | 0.06 0.03 0.04 | 23 23 23 23 23 23 | | |
| 2 ** | | 0.24 | | 23 | | |

After 3.5 years at 50°C. ** After 3.5 years at 50°C and 2 years at magazine temperature.

<u>Solubility: gm/100 gm (%), of:</u> (e)

| W | ater | Alcohol | | Ethy | 1 Acctate |
|------------------|------------------|----------------------------------|---|----------------------------------|---|
| o _C | 1/2 | °C | <u>%</u> | <u>°c</u> | 20 |
| 20 100 | 1.1 75 | 0 10 30 50 80 | 0.515 0.690 1.050 1.890 3.620 | 0 10 30 <i>50</i> 80 | 0.290 0.300 0.380 0.450 0.560 |

Origin:

First prepared by Marchand in 1841 and used by Brugere in admixture with potassium nitrate as a propellant in 1869. Used as a high explosive after 1900.

Destruction by Chemical Decomposition:

Explosive D (ammonium picrate) is decomposed by dissolving in 30 times its weight of a solution made from 1 part of sodium sulfide ($Na_2S \cdot 9H_2O$) in 6 parts of water.

References: 30

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III</u> - <u>Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, <u>OSRD</u> Report No. 5746, 27 December 1945.

³⁰See footnote 1, page 10.

Explosive D (Ammonium Picrate)

(b) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(c) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute for</u> <u>Tetryl in Boosters</u>, NOL Mamo 10,303, 15 June 1949.

(d) F. W. Brown, D. H. Kusler and F. C. Gibson, Sensitivity of Explosives to Initiation by Electrostatic Discharges, U. S. Dept of Int, Bureau of Mines, RI 3852, 1946.

(e) Various sources in the open Literature.

(f) Also see the following Picatinny Arsenal Technical Reports on Explosive D:

| <u>o</u> | <u>1</u> | 2 | <u>3</u> | <u>4</u> | 5 | 6 | <u>7</u> | <u>8</u> | <u>9</u> |
|--------------------|--------------|--|----------|-----------------------------------|---|--|---------------------|--------------------|--------------|
| 340 870 1380 | 1441 1651 | 132 582 1172 1352 1372 1492 | a43 | 694 704 874 1234 1724 | 65 425 1585 1655 1725 1885 1895 | 266 556 796 986 1466 1796 | 1737 1797 | 328 838 1838 | 1729 1759 |

AMCP 706-177

Glycerol Monolactate Trinitrate (GLTN) Liquid

| Composition: % | Molecular Weight: (C ₆ H ₉ N ₃ O ₁₁) 299 |
|--|---|
| 24.1 0 0N0 3.0 $CH_{2} - 0 - C - CH - CH$ | Oxygen Balance: -30 CO, % 3 |
| N 14.1 CH-ONO ₂ | Density: gm/cc Liquid 1.47 |
| о 58.8 ^{Сн} 2 ^{— омо} 2 | Melting Point: "C |
| C/H Ratio 0.180 | Freezing Point: "C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 15 (11 b wt); 42 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | Boiling Point: "C Refractive Index, n ^D ₂₀ n ^D ₂₅ 1.464 n ^D ₃₀ |
| Friction Pendulum Test: Steel Shoe Unaffected Fiber Shoe Unaffected | Vacuum Stability Test: cc/40 Hrs, at 90°C |
| Rifle Bullet Impact Test: Trials % Explosions Portials | 100°C 5.9 120°C 135°C 150°C |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm 13-1 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 223 10 15 20 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminote Lead Azide Tetryl Ballistic Mortar, % TNT: |
| 20 | Trauzi Test, % TNT: |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method |
| 100°C Heat Test: % Loss, 1st 48 Hrs 2.5 % Loss, 2nd 48 Hrs 1.8 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT |
| Flammability Index: | Detonation Rote: Confinement |
| Hygroscopicity: % | Condition Charge Diameter, in. |
| Volatility: 60°C, mg/cm ² /hr 28 | Density, gm/cc Rate, meters/second |

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Glycerol Monolactate Trinitrate (GLTN) Liquid

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| ragmentation Test: | Shaped Charge Effectiveness, TNT = | 100: |
|--|---|----------------|
| 90 mm 旺, M71 Projectile, Lot WC-91: | Glass Cones Steel | Cones |
| Density, gm/cc | Hole Volume | |
| Charge Wt, Ib | Hole Depth | |
| Total No. of Fragments: | Color: | |
| For TNT | | |
| For Subject HE | Principal Uses: Gelatinizer for n | itrocellulose |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | | |
| Density, gm/cc | | |
| Charge Wt, Ib | | |
| Total No. of Fragments: For TNT | Method of Loading: | |
| Far Subject HE | Loading Density: gm/cc | |
| | | |
| ragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | |
| Density, gm/cc | Method | Liquid |
| last (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 |
| . | Compatibility Group | |
| Air: Peak Pressure | | |
| Impulse | Exudation | |
| Energy | | |
| Air, Confined: | Hydrolysis, % Acid: | |
| Impulse | 10 days at 22 ⁰ C 5 days at 60 ^o C | 0.021 0.014 |
| Under Water: Peak Pressure | Solubility in Water, gm/100 gm, at: | |
| Impulse | 25 ⁰ .c 60 ^o c | <0.01 |
| Energy | | < 0.015 |
| Underground: | Solubility, gm/100 gm, at 25 ⁰ C, in: | |
| Peak Pressure | Ether | 8 |
| Impulse Energy | 2: 1 Ether:Alcohol Acetone | m ∞ |
| 5, | Heat of: | |
| | Combustion, cal/gm | 2407 |
| | | |
| | | |

Preparation:

Glycerol monolactate (GML) is prepared by heating a glycerol lactic acid mixture containing $\frac{4\%}{16}$ excess lactic acid at 116°C for 112 hours with dry air bubbling through the liquid. The product which contains 0.67% free acid is carefully mixed with 6 parts of $\frac{40}{60}$ HNO₃/H₂SO₄ maintained at 20°C, stirred for 1 hour, cooled to 5°C, and poured on ice. It is extracted with ether, water-washed, adjusted to pH 7 by shaking with a sodium bicarbonate solution, and again water-washed three times. It is then dried with calcium chloride, filtered and freed of ether by bubbling with air until minimal loss in weight is obtained. The product has a nitrate-nitrogen content of 13.43% (theoretical 14.1% N). Another batch, prepared from GML obtained from glycerol-lactic acid containing 6.5% excess glycerol, had a nitrate-nitrogen content of 14.30%, dorresponding to a mixture containing 5.5% nitroglycerin. It is not considered practicable to prepare the pure GLTN.

Origin:

The preparation of a nitrated ester of lactic acid and glycerol, by nitrating a glyceryl lactate with nitric and sulfuric acids, for use in explosives, was reported in 1931 by Charles Stine and Charles Burke (U. S. Patent 1,792,515).

The preparation of glycerol monolactate by heating glycerol with equimolar proportions of a lactic acid ester of an alcohol boiling below 100°C (ethyl lactate) was patented by Richie H. Locke in 1936 (British Patent 456,525 and U. S. Patent 2,087,980).

Reference: 31

(a) P. F. Macy and A. A. Saffitz, <u>Explosive Plasticizers for,Nitrocellulose</u>, PATR No. 1616, 22 July 1946.

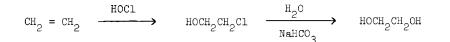
³¹See footnote L, page LO.

| Composition: % | Molecular Weight: $(C_2H_4N_2O_6)$ |) 1.52 |
|---|--|-------------------------------|
| c 15.8 ONO ₂ | Oxygen Bolance: CO, % CO % | 0.0 21 |
| N 184 | Density : gm/cc Liquid, 25 | ^D C 1.48 |
| 0 63.2 | Melting Point: "C | -20 |
| C/H Ratio 0.092 | freezing point: "C | |
| Impact Sensitivity, 2 Kg Wt: | Boiling Point: °C | |
| Bureau of Mines Apparatus, cm 4 (1 1b wt); 56 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | Refractive Index, n ^D ₂₀ n ^D ₂₃ n ^D ₃₀ | 1.4452 |
| Friction Pendulum Test: | Vacuum \$toþilit y Test: | |
| Steel Shoe Fiber Shoe | cc/40 Hrs, at 90°C | |
| Rifle Bullet Impact Test: Trials | 100°C 120°C | |
| Explosions | 135°C 150°C | |
| Partials Burned | 200 Gram Bomb Sand Test: | |
| Unaffected | Sand, gm | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Explodes 257 10 | Sensitivity to Initiation: Minimum Detonating Charge, Mercury Ful minote Lead Azide Tetryl | gm |
| 15 20 | Ballistic Morter, % TNT: | |
| | Trauzi Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method | |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: | Class tuba |
| - | Confinement Condition | Glass tube Liquid |
| Hygroscopicity: % 30 [°] C, 90% RH 0.00 | Charge Diameter, in. | 10 |
| Volatility: | Density, gm/cc Rate, meters/second | 1.485 7300 and 2050 |

| Fragmentation Test: | Shaped Charge Effectiveness, TNT == 100: | | | |
|---|---|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, lb | Glass Cones Steel Cones Hole Volume Hole Depth | | | |
| Total No. of Fragments: For ⊤N⊤ | Color: Yellow | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Ingredient of nonfreezing dynamite | | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: | | | |
| Fragment Velocity: ft/sec | Loading Density: gm/cc | | | |
| At 9 ft At 25½ ft | Storage: | | | |
| Density, gm/cc | Method Liquid | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 | | | |
| Air: Peak Pressure impulse Energy | Compatibility Group Exudation | | | |
| Air, Confined: Impulse | $\frac{\text{Solubility in 1000 cc Water:}}{\frac{\text{Temp.} ^{\text{O}}\text{C}}{15}} \frac{\text{Grams}}{6.2}$ | | | |
| Under Water: Peak Pressure | 20 6.8 50 9.2 | | | |
| Impulse Energy | Viscosity, centipoises: Temp, 20 ⁰ C 4.2 | | | |
| Underground: Peak Pressure Impulse Energy | Vapor Pressure: $^{\circ}C$ mm Mercury 0 0.0044 20 0.038 40 0.26 60 1.3 80 5.9 100 22.0 Heat of: 22.0 | | | |
| | InterviewCombustion, cal/gm1764Formation, cal/gm(b)366 | | | |

Preparation:

Glycol dinitrate (ethylene glycol dinitrate, dinitroglycol, nitroglycol, dinitrodimethyleneglycol) may be prepared by nitration of ethylene glycol, $HOCH_2CH_2OH$, with a mixed nitric acid in the same apparatus that is used for the preparation of nitroglycerin. The glycol is prepared by synthesis from ethylene, and ethylene chlorohydrin:



Origin:

Henry was the first to prepare and identify glycol dinitrate (Ber 3, 529 (1870) and Ann chim phys [4] 27, 243 (1872) but Kekulé had previously nitrated ethylene and obtained an unstable oil which he supposed to be glycol nitrate-nitrate. No immediate practical use was made of glycol diqitrate because glycol itself was relatively rare and expensive at the time. It was 1904 before a patent was granted covering the use of GDN as an explosive (DRP 179,789), but it was seven years later before its actual use as an explosive was recorded (Mém poudr 16 (1911) p. 214). The principal physical properties of GDN were determined or recorded by Rink-enbach (Ref b).

References: 32

(a) Ph. Naoum, <u>Nitroglycerin and Nitroglycerin Explosives</u>, translation, E. M. Symmes, The Williams and Wilkins Company, Baltimore (1928), p. 224.

(b) Wm H. Rinkenbach, "The Properties of Glycol Dinitrate," Ind Eng Chem 18, 1195 (1926).

(c) Wm H. Rinkenbach, "Glycol Dinitrate in Dynamite Manufacture," Chem Met Eng, <u>34</u>, 296 (1927).

(d) Wm H. Rinkenbach, <u>Application of the Vacuum Stability Test to Nitroglycerin and Nitro-</u> glycerin Explosives, PAIR 1624, 27 August 1946.

³²See footnote 1, page 10.

<u>H-6</u>

| Composition: | Molecular Weight: | |
|--|--|--------|
| % | | 93 |
| RDX 45 | Oxygen Balance: | |
| TNT 30 Aluminum 20 | CO % | -36 |
| D-2 Wax 5 | Density: gm/cc Cast | 2 (7) |
| Calcium Chloride, | Density: gm/cc Cast | 1.74 |
| added 0.5 | Melting Point: °C | |
| C/H Ratio | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | Boiling Point: °C | |
| Sample Wt 20 mg | Refractive Index, n ^D ₂₀ | |
| Picatinny Arsenal Apparatus, in, (c) 14 | n25 | |
| Sample Wt, mg 18 | | |
| Frietian Dandukum Tasti | n ₃₀ | |
| Friction Pendulum Test: Steel Shoe Unaffected | Vacuum Stability Test: | |
| Fiber Shoe Unaffected | cc/40 Hrs, at | |
| | 90°C 100°C | |
| Rifle Bullet Impact Test: Trials (b) | 120°C | 0.47 |
| % | 135°C | |
| Explosions 80 | 150°C | |
| Partials | 130 0 | |
| Burned | 200 Gram Bomb Sand Test: | |
| Unaffected 20 | Sand, gm | 49.5 |
| Explosion Temperature: °C (a) | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) | Minimum Detonating Charge, gm | |
| 1 | Mercury Fulminate | |
| 10 | Lead Azide | 0.20 |
| 15 | Tetryl | 0.10 |
| 20 | Ballistic Mortar, % TNT: (d) | 135 |
| | Trauri Test, % TNT: | -07 |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: | |
| | Method | |
| 100°C Heat Test: | Condition | |
| % Loss, 1st 48 Hrs 0.78 | Confined | |
| % Loss, 2nd 48 Hrs 0.00 | Density, gm/cc | |
| Explosion in 100 Hrs None | Brisance, % TNT | |
| Flammability Index: | Detonation Rate: | (a, b) |
| | Confinement | None |
| Hygroscopicity: % 30°C, 95% RH, 7 days 2.01 | Condition | Cast |
| Hygroscopicity: % 30°C, 95% RH, 7 days 2.01 71°C, 95% RH, 7 days 1.77 | Charge Diameter, in. | 1.0 |
| Volatility: | Density, gm/cc | 1.71 |
| | Rate, meters/second | 7191 |

| Booster Sensitivity Test: Condition Tetryl, gm Wax, in. for 50% Detonation Wax, gm Density, gm/cc Heat of: Combustion, cal/gm Explosion, cal/gm Formation, cal/gm Fusion, cal/gm | 3972 923 733 10.25 | Decomposition Equation: Oxygen, atams/sec (Z/sec) Heat, kilocolorie/mole (AH, kcal/mol) Temperature Range, °C Phase Armor Plate Impact lest: 60 mm Mortar Projectile: 50% Inert, Velocity, ft/sec Aluminum Fineness |
|--|--|---|
| a <u>nness</u> a <u>nn</u> e | | 500-lb General Purpose Bombs: |
| Specific Heat: col/gm/°C 30 ^୦ ୯ | (b) 0.269 | Plate Thickness, inches |
| 50°C | 0.268 | 1 11/4 11/2 13/4 |
| Burning Rate: cm/sec | | Bomb Drop Test: |
| Thermal Conductivitv: col/sec/cm/°C 35°℃ | (b) -3 1.10 x 10 | T7, 2000-Ib Semi-Armor-Piercing Bomb ♥\$ Concrete: |
| Coefficient of ,Expansion: Linear, ∆ℓ /inch 0 [°] C 35 [°] C 70 [°] C | 40×10^{-4} 83×10^{-1} 131×10^{-1} | Max Safe Drop, ft 500-Ib General Purpose Bomb vs Concrete: Height, ft |
| Hardness, Mohs' Scale: | | Trials Unoffected |
| Young's Modulus: E', dynes/cm² E, Ib/inch² Density, gm/cc | (b) 9.0 x 10 ⁹ 1.30 x <i>i</i> 5 ¹ 1.71 | Low Order High Order 1000-1b General Purpose Bomb vs Concrete: Height, ft |
| Compressive Strength: Ib/inch ² | See below | Trials Unaffected |
| Vapor Pressure: °C mm Mercury | | Low Order High Order |
| Compressive Strength: 1b/inch Density, gm/cc Ultimate deformation, % | 2 1083 1.71 1.32 | |

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| Fragmentation Test: | (b) | Shaped Charge Effectiveness, TNT = | 100: |
|--|------------|--|-----------|
| 90 mm HE, M71 Projectile, Lot EGS-1– Density, gm/cc Charge Wt, Ib | 17: | Glass Cones Steel Hole Volume Hole Depth | Cones |
| Total No. of Fragments: For Composition B | 998 | Color: | Gray |
| For Subject HE For 80/20 Tritonal | 714 616 | Principal Uses: | HE charge |
| 3 inch HE, M42A1 Projectile, Lot KC-5 Density, gm/cc Charge Wt, Ib | | | |
| Total No. of Fragments: For TNT | | Method of Loading: | Cast |
| For Subject HE | | Loading Density: gm/cc | 1.71 |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | | Storage: | |
| Density, gm/cc | | Method | Dry |
| Blast (Relative to TNT): | (a) | Hazard Class (Quantity-Distance) | Class 9 |
| Air: 3.25" diameter sphere Peak Pressure Δ psi Catenary | 25.4 | Compatibility Group | Group I |
| Impulse NFOC Pendulum Energy | 19.8 | Exudation | None |
| Air, Confined: Impulse | | | |
| Under Water: Peak Pressure | | | |
| Impulse Energy | | | |
| Underground: Peak Pressure | | | |
| Impulse Energy | | | |
| | | | |
| | | | |
| | | | |

| | | (Reference | e) | | |
|------------------------|--------------------------------------|------------------------------------|-----------------------------|---|--------------------------------------|
| Explosive | Simulated Altitude, i <u>Feet</u> | <u>One-Inch</u> Confined m/s | Column Inconfined m/s | $\frac{\text{Two-Inc}}{\frac{\text{Confined}}{\text{m/s}}}$ | h Column <u>Unconfined</u> m/s |
| TNT, | Ground | 6820 | 6720 | 6670 | 5270 |
| density, gm/cc 1.59 | 30,000 | 6660 | 69 30(2) | 6610 | 6760(4) |
| 8 <i>,</i> | 60,000 | , 6800 | - | 6520 | 6400 (4) |
| | 90,000 | 6810 | 6720 | 6550 | 6610 (1) |
| Average | | 6798 | 6790 | 6588 | 6260 |
| н-6, | Ground | 7190 | 7360 | 7340 | 6870 |
| density, gm/cc 1.69 | . 30,000 | 7300(2) | 7430 | 7360 | 7980 |
| 6-7 ··· 1.00 | 60,000 | 7280 | 7490 | 7550 | 7010 |
| | 90,000 | 7300(3) | 7270 | 7500 | 7000 |
| Average | | 7268 | 7385 | 7438 | 7215 |

Effect of Altitude, Charge Diameter and Degree of Confinement on Detonation Velocity*

*Confined charge in 1/4" steel tube, AISI 1015 seamless, 1" diameter 18" long, and 2" diameter 7" long. All means were determined from sets of five values unless otherwise indicated by (). A 26 gm tetryl booster was used to initiate each charge.

Average Fragment Velocities at Various Altitudes* (e)

| Explosive | Charge Diameter, <u>Inches</u> | Si <u>Ground</u> m/s | mulated Alti <u>30,000</u> m/s | tude, Feet <u>60,000</u> <u>m/s</u> | <u>90,000</u> m/s |
|------------------------|-----------------------------------|----------------------------|--------------------------------------|---|----------------------|
| | | 2940 | 2991 | 6 | |
| gm/cc 1.51 | | - | | | |
| н-6, | 1 | 3461 | 3405 | 3467 | 3563 |
| density, gm/cc 1.71 | 2 | 4603 | 4726 | 4998 | 5288 |

*Outside diameter $\overline{2.54}$; inside diameter $\overline{2.04}$; length $\overline{7}$.

References:

See HBX-1; HBX-3 reference list.

Haleite (Ethylene Dinitramine) (EDNA)

(In recognition of its development as a military explosive $\ensuremath{\mathtt{b}}\xspace$ the

| Composition: | | | |
|--|--|--|---------------|
| % | NO | Molecular Weight: $(C_2H_6N_4O_4)$ 150 |) |
| С 16.0 H ₂ Н 4.0 | | Oxygen Balance: CO, % -32 CO, % -10. | <u>.</u> 5 |
| N 37.3 | | Density: gm/cc Crystal 1.7 | 71 |
| 0 42.7 H ₂ (| $\frac{1}{2}$ $\frac{NO_2}{NO_2}$ | Melting Point: °C Decomposes 175 | + |
| C/H Ratio 0.066 | H | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, | cm 48 | Boiling Point: °C | |
| Sample Wt 20 mg | | Refractive Index, n ^D ₂₀ | |
| Picatinny Arsenal Apparatus Sample Wt, mg | s, in. 14 17 | n ₂₅ | |
| | | n ₃₀ | |
| Friction Pendulum Test: | ······································ | | |
| Steel Shoe | Unaffected | Vacuum Stability lest: | |
| Fiber Shoe | Unaffected | cc/40 Hrs, at 90°C | |
| | | | |
| Rifle Bullet Impact Test: T | rials | ••• | |
| 1 | % | 120°C 1.5 135°C | |
| Explosions | 0 | | |
| Partials 6 | 30 | 150°C 11+ | |
| Burned 2 | 20 | 200 Gram Bomb Sand Pest: | |
| Unaffected 2 | 20 | Sand, gm 52. | 3 |
| Explosion Temperature: | °C | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) | 265 | Minimum Detonating Charge, gm | |
| 1 | 216 | Mercury Fulminate 0,21 | |
| 5 Decomposes | 189 | Lead Azide 0.13 | |
| 10 | 178 | Tetryl | |
| 15 | 173 | | |
| 20 | 170 | Ballistic Mortar, % TNT: (a) 139 | |
| 75°C International Heat Test: | - | Trauri Test, % TNT: (b) 122 | |
| % Loss in 48 Hrs | 0.01 | Plate Dent Test: (c) | |
| | | Method A | |
| 100°C Heat Test: | | Condition Pres | sed |
| % Loss, 1st 48 Hrs | 0.2 | Confined Yes | |
| % Loss, 2nd 48 Hrs | 0.3 | Density, gm/cc 1.50 | |
| Explosion in 100 Hrs | None | Brisance, % TNT 122 | |
| Flammability Index: | 138 | | onfined |
| Hygroscopicity: % | 0.01 | Condition Press Charge Diameter, in. 1.0 | sed |
| Volatility: | Nil | Density, gm/cc 1.49 Rate, meters/second 7570 | |

Haleite (Ethylene Dinitramine) (EDNA)

AMCP 706-177

| Booster Sensitivity Test: Condition | (ð) Pressed | Decomposition Equation: (e) (e) (f) Oxygen, atoms/sec $10^{12.8}$ $10^{12.1}$ 10^{1} |
|--|----------------|---|
| Tetryl, gm | 100 | (Z/sec) Heat, kilocolorie/mole 30.5 37.3 30.4 |
| Wax, in. for 50% Detonation | 2.09 | (AH kcal/mol) |
| Wax, gm | | Temperature Range, °C 184-254 144-1 |
| Density, gm/cc | 1.42 | Phase Liquid Solid Soli |
| Heat of: | | Armor Plate Impact Test: |
| Combustion, cal/gm | 2477 | |
| Explosion, cal/gm | 1276 | 60 mm Mortar Projectile: |
| Gas Volume, cc/gm | 908 | 50% Inert, Velocity, ft/sec |
| Formation, col/gm | 134 | Aluminum Fineness |
| Fusion, cal/gm | | 500-lb General Purpose Bombs: |
| Specific Heat; cal/gm/°C | | |
| •••••••••••••••••••••••••••••••••••••• | | Plate Thickness, inches |
| | | 1 |
| | | 11/4 |
| | | 11/2 |
| | | 13/4 |
| Burning Rate: | | |
| cm/s e c | | Bomb Drop Test: |
| Thermal Conductivity: | | T7, 2000-1b Semi-Armor-Piercing Bomb vs Concrete: |
| cal/sec/cm/°C | | T7, 2000-10 Setti-Athlot-Pletchy Bothb 13 Conclete. |
| Coefficient of Expansion: | | Max Safe Drop, ft |
| Linear, %/°C | | 500-lb General Purpose Bomb vs Concrete: |
| Volume, %/°C | | Height, ft |
| | | Trials |
| Hardness, Mohs' Scale: | | Unaffected |
| | | Low Order |
| Young's Modulus: | | High Order |
| E', dynes/cm² | | |
| E, Ib/inch ² | | 1000-Ib General Purpose Bomb vs Concrete: |
| Density, gm/cc | | |
| | | — Height, ft |
| Compressive Strength: Ib/inch ² | | Trials |
| | | Unaffected |
| Vapor Pressure: | | Low Order |
| °C mm Mercury | | High Order |
| | | |
| | | |
| | | |

AMCP 706-177

| Fragmentation Test: | | Shaped Charge Effectiveness, $TNT = 7$ | 100: |
|--|---|---|-------------------------------|
| 90 mm HE, M71 Projectile, Lot WC- Density, gm/cc Charge Wt, Ib | 91: 1.61 | Glass Cones Steel Hole Volume | Cones |
| Total No. of Fragments: | | Hole Depth Color: | White |
| For TNT For Subject HE | | | |
| 3 inch HE, M42A1 Projectile, Lot KC Density, gm/cc Charge Wt, Ib | - 5: <u>Haleite/wax</u> 1.56 | Principal Uses: | Booster |
| Total No. of Fragments: For TNT 51 ^կ | | Method of Loading: | Pressed |
| For Subject HE Fragment Velocity: ft/sec At 9 ft At 251/2 ft | 600 | Loading Density: gm/cc psi x 5 10 12 15 1.28 1.38 1.41 1.44 Storage: | 10 ³ 20 1.49 |
| Density, gm/cc | | Method | Dry |
| Blast (Relative to TNT): | | Hazard Class (Quantity-Distance) | Class 9 |
| Air: Peak Pressure | | Compatibility Group | |
| Impulse Energy | | Exudation | None |
| Air, Confined: Impulse | | | |
| Under Water: Peak Pressure | | | |
| Impulse Energy | | | |
| Underground: Peak Pressure | | | |
| Impulse Energy | | | |
| | | | |
| | | | |

Compatibility with Metals:

<u>Dry</u> - Copper, brass, aluminum, mild steel, stainless steel, mild steel coated with acidproof black paint, and mild steel plated with copper nickel, cadmium or zinc are unaffected. Magnesium and magnesium-aluminum alloy are slightly affected.

Wet - Copper, brass, mild steel coated with acid-proof black paint, and mild steel plated with copper, cadmium, nickel or zinc are heavily corroded. Aluminum is slightly affected and stainless steel is unaffected.

Impact Sensitivities of Various Crystal Habits:

| Bureau of Mines | Impact | Test, | 2 Kg | Wt: |
|---|--------|-------|------|----------------------------|
| Habit | | | | em |
| lst plate 2nd plate Bi-pyramid Bracydome Sphenoid | | | | 55 55 71 66 46 |

Solubility: gm/100 gm (%) of:

| Water | | Alc | ohol |
|-----------------------------|-------------------------------------|----------------------|------------------------------|
| <u>°c</u> | <u>%</u> | ്പ | % |
| 20 40 60 80 100 | 0.25 0.75 2.13 6.38 >20 | 20 40 60 78 | 1.00 2.46 5.29 10.4 |

Preparation:

(Summary Technical Report of the NDRC, Div 8, Vol 1)

$$\begin{array}{c} \mathrm{CH}_{2}\mathrm{O} + \mathrm{HCN} \rightarrow \mathrm{HO} \ \mathrm{CH}_{2}\mathrm{CN} \\ & (98\%\mathrm{yield}) \\ \mathrm{HO} \ \mathrm{CH}_{2}\mathrm{CN} + \mathrm{NH}_{3} \rightarrow \mathrm{NH}_{2}\mathrm{CH}_{2}\mathrm{CN} + \mathrm{H}_{2}\mathrm{O} \\ & (82\%\mathrm{yield}) \\ \mathrm{NH}_{2}\mathrm{CH}_{2}\mathrm{CN} + \mathrm{2H}_{2} \rightarrow \mathrm{H}_{2}\mathrm{N} \ \mathrm{CH}_{2}\mathrm{CH}_{2}\mathrm{NH}_{2} \\ & (88\%\mathrm{yield}) \end{array}$$

$$\begin{array}{c} \overset{\mathrm{CH}_2 \longrightarrow \mathrm{NH}}{\underset{\mathrm{CH}_2 \longrightarrow \mathrm{NH}_2}{\overset{\mathrm{CH}_2 \longrightarrow \mathrm{H}_2}{\overset{\mathrm{CH}_2 \longrightarrow \mathrm{H}_2}{\overset{\mathrm{CH}_2 \longrightarrow \mathrm{NH}}{\overset{\mathrm{CH}_2 \longrightarrow \mathrm{NH}}{\overset{\mathrm{CH}_2 \longrightarrow \mathrm{H}_2}{\overset{\mathrm{CH}_2 \longrightarrow \mathrm{H}_2}{\overset{\mathrm{CH}_2}}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}{\overset{\mathrm{CH}_2}}{\overset{\mathrm{C$$

Haleite (Ethylene Dinitramine) (EDNA)

$$\begin{array}{c} CH_2 \longrightarrow NH \\ | \\ CH_2 \longrightarrow NH \end{array} \xrightarrow{(CH_2 - N \longrightarrow NO_2)} CO + 2HNO_3 \xrightarrow{(CH_2 - N \longrightarrow NO_2)} CO + 2H \\ | \\ CH_2 \longrightarrow NH \longrightarrow NO_2 \end{array} \xrightarrow{(CH_2 - N \longrightarrow NO_2)} CO + H_2O \xrightarrow$$

The raw materials used in this process are cheap and available; the first three reactions proceed smoothly, rapidly and in good yield (70% overall), and only the third requires high pressures. The reaction of ethylenediamine with carbon dioxide at about $220^{\circ}C$ and 820 atmospheres has been worked out and is more satisfactory for the preparation of ethyleneurea than the use of chlorethyl carbonate or urea and better than the reaction of acetic anhydride and ethylenediamine to yield N,N'-diacetyl-ethylenediamine which can be treated in a way similar to the above to yield Haleite.

Ethyleneurea is very easily nitrated, with strong nitric acid (98%), st ordinary temperature, and in a very short time, and the dinitroethyleneurea produced appears of Lydrolyze, yielding Haleite, immediately after solution in water at 95°C. Both the nitration and hydrolysis are practically quantitative.

Origin:

First described in 1877 by Franchimont and Klobbie (Rec trav chim 7, 17 and 244) but it was 1935 before its value as an explosive was recognized. Standardized during World War II as a military explosive.

Destruction by Chemical Decomposition:

Haleite is decomposed by addition to hot, dilute sulfuric acid. Nitrous oxide, acetaldehyde and ethylene glycol are evolved. Haleite is also decomposed by addition to 5 times its weight of 20% sodium hydroxide.

References: 33

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III</u> - <u>Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, OSRD Report No. 5746, 27 December 1945.

- (b) Report AC-2983/Org Ex 179.
- (c) D. P. MacDougall, <u>Methods of Physical Testing</u>, OSRD Report No. 803, 11 August 1942.

(d) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute for Tetryl in Boosters</u>, NOL Mamo 10,303, 15 June 1949.

(e) R. J. Finkelstein and G. Gamow, <u>Theory of the Detonation Process</u>, NAVORD Report No. 90-46, 20 April 1947.

(f) ^{M.} A. Cook and ^{M.} Taylor Abbeg, "Isothermal Decomposition of Explosives," University of Utah, <u>Ind Eng Chem</u> (June 1956) pp. 1090-1095.

³³See footnote 1, page 10.

Haleite (Ethylene Dinitramine) (EDNA)

| <u>_</u> | <u>1</u> | 2 | 3 | 4 | <u>5</u> | 6 | _7 | 8 | ೨ |
|--|----------------------|--------------------------------------|----------------------|---------------------|------------------------------|-------------|-----------------------------|--------------------------------------|--|
| 1200 1290 1360 1380 1400 1600 | 1231 1451 1651 | 1162 1232 1252 1352 1372 | 1113 1493 1923 | 414 1294 1434 | 1255 1325 1395 1885 | 786 1796 | 897 1737 1797 1937 | 1198 1288 1378 1388 1838 | 1279 1319 1379 1469 1489 2179 |

 $_{\rm (g)}\,$ Also see the following Picatinny Arsenal Technical Reports on Haleite:

HBX-1

| Composition: | Molecular Weight: | 102 |
|---|---------------------------------------|--------------------|
| ⁷⁰ RDX 40 TNT 38 A 7uminum 17 | Oxygen Balance: CO, % CO % | -68 -35 |
| D-2 Wax 5 | Density: gm/cc Cast | 1.72 |
| Calcium Chloride, added 0.5 | Melting Point: "C | |
| C/H Ratio | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | Boiling Point: "C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 16 | Refractive Index, n_{20}^{O} | |
| Sample Wt, mg 21 | n ^D 25 | |
| | n ₃₀ | |
| Friction Pendulum Test: (b) | Vacuum Stability Test: | (a, b) |
| Steel Shoe Unaffected | cc/40 Hrs, at | |
| | 90°C | |
| Rifle Bullet Impact Test: Trials (b) | 100°C 120°C | 0.47 0.98 |
| % | 135°C | - |
| Explosions 73 | 150°C | 11+ |
| Partials | | |
| Burned | 200 Gram Bomb Sand Test: | |
| Unaffected 28 | Sand, gm | 48.1 |
| Explosion Temperature: °C (a) Seconds, 0.1 (no cap used) | Sensitivity to Initiation: | |
| 1 | Minimum Detonating Charge, gm | |
| 5 480 | Mercury Fulminate | |
| 10 | Lead Azide | 0.20 |
| 15 | Tetryl | 0.10 |
| 20 | Ballistic Mortar, % TNT: (d) | 133 |
| | Trauzl Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: | |
| | Method | |
| 100°C Heat Test: (b) | Condition | |
| % Loss, 1st 48 Hrs 0.058 | Confined | |
| % Loss, 2nd 48 Hrs 0.00 | Density, gm/cc | |
| Explosion in 100 Hrs None | Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement | (a, b) None |
| Hygroscopicity: % 30 [°] C, 95% RH, 7 days 2.98 71°C, 95% RH, 7 days 1.13 | Condition Charge Diameter, in. | Cast 1.0 |
| Volatility: | Density, gm/cc Rate, meters/second | 1.69 7224 |

<u>HBX-1</u>

| Poortor Consistivity Test | (c) | Decomposition Equation: |
|--|--|---|
| Booster Sensitivity Test: Condition | Cast | Oxygen, atoms/sec |
| Tetryl, gm | 100 | (Z/sec) |
| Wax, in. for 50% Detonation | 1.25 | Heat, kilocalarie/male (AH, kcal/mal) |
| Wax, gm | | Temperature Range, °C |
| Density, gm/cc | 1.73 | Phase |
| Heat of: | (b) 3882 | Armor Plate Impact Test: |
| Combustion, cal/gm | - | A. |
| Explosion, col/gm | 919 | 60 mm Mortar Projectile: |
| Gas Volume, cc/gm | 758 | 50% Inert, Velocity, ft/sec |
| Formation, col/gm | 758 9•25 | Aluminum Fineness |
| Fusion, cal/gm 78 ⁰ C | 9.25 | 500-lb General Purpose Bombs: |
| Specific Heat: cal/gm/°C | (b) | |
| 30°C | 0.249 | Plate Thickness, inches |
| 50 [°] C | 0.264 | 1 |
| | | 11/4 |
| | | 11/2 |
| | | 13/4 |
| Burning Rate: cm/sec | | |
| | | Bomb Drop Test: |
| Thermal Conductivity: cal/sec/cm/°C 35 [°] C | (b) 0.97 x 10 ⁻³ | T7, 2000-lb Semi-Armor-Piercing Bomb vs Concrete: |
| Coefficient of Expansion: | (b) | Max Safe Drop, ft |
| Linear AllAnch | 46×10^{-4} | 500-lb General Purpose Bomb vs Concrete: |
| 0°C 35°C | 46×10^{-4} 95 x 10 ⁻⁴ | |
| 70°C | 159 x 10 ⁻⁴ | Height, ft |
| Hardness. Mohs' Scale: | | Trials |
| fratuless, wong scale. | | Unaffected |
| Young's Modulus: | (b) | Low Order |
| E, dynes/cm ² | 10.3 x 10^9 | High Order |
| E, Ib/inch ² | 1.49×10^{-7} | 1000-lb General Purpose Bomb vs Concrete: |
| Density, gm/cc | 1.69 | • m |
| | 01 | Height, ft |
| Compressive Strength: Ib/inch ² | See below | Trials |
| | | Unaffected |
| Vapor Pressure: | | Low Order |
| °C mm Mercury | (b) | High Order |
| Compressive Strength: lb/inch ² Density, gm/cc | 1303 1.69 | |
| Ultimate deformation, % | 1.38 | |
| | | |
| | | |

AMCP 706-177

HBX-1

| Fragmentation Test: | (b) | Shaped Charge Effectiveness, TNT = | 100: |
|--|--------------|--|----------------|
| 90 mm HE, M71 Projectile, Lot EGS-1 [.] Density, gm/cc Charge Wt, Ib | -17: | Glass Cones Steel Hole Volume Hole Depth | Cones |
| Total No. of Fragments: For Composition B | 998 | Color: | Gray |
| For Subject HE For 80/20 Tritonal 3 inch ME, M42A1 Projectile, Lot KC-5: Density, gm/cc | 910 616 | Principal Uses: | HE charge |
| Charge Wt, Ib Total No. of Fragments: For TNT For Subject HE | | Method of Loading: | Cast |
| Frogment Velocity: ft/sec | | Loading Density: gm/cc | 1.69 |
| At 9 ft At 25½ ft Density, gm/cc | | Storage: | |
| Blast (Relative to TNT): | (a) | Method Hazard Class (Quantity-Distance) | Dry Class 9 |
| Air: 3.25" diameter sphere Peak Pressure A psi Catenary Impulse NFOC Pendulum | 24.7 19.6 | Compatibility Group | Group I |
| Energy | | Exudation | None |
| Air, Confined: Impulse | | | |
| Under Water: Peak Pressure | | | |
| Impulse Energy | | | |
| Underground: Peak Pressure | | | |
| impulse Energy | | | |
| | | | |
| | | | |

| | Oxygen Balance: | |
|----------------------------|--|--|
| | CO.2 % | -75 |
| | CO % | -49 |
| | Density: gm/cc Cast | 1.84 |
| | Melting Point: °C | |
| | Freezing Point: "C | |
| | Boiling Point: °C | |
| 15 23 | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| | Vacuum Stability Jest | (a, b) |
| Unaffected | cc/40 Hrs, at | |
| | 90°C | |
| (b) | | 0.45 |
| | | |
| | | |
| | | <i>(</i> -) |
| | 200 Gram Bomb Sand lest: Sand, gm | (ъ) 44.9 |
| (a) | Sensitivity to Initiation: Minimum Detonating Charge, gm | |
| | | |
| | | 0.20 |
| | Tetryl | 0.10 |
| | Ballistic Mortar, % TNT: (d) | 111 |
| | Trauzl Test, % TNT: | |
| | Plate Dent lest: Method | |
| (b) | Condition | |
| 0.70 | Confined | |
| 0.00 | Density, gm/cc | |
| None | Brisance, % TNT | |
| | Detonation Rate: Confinement | (a, b) None |
| 7 days 2.01 7 days 0.31 | Condition Charge Diameter, in. | Cast 1.0 |
| | | |
| | 23 Unaffected (b) (a) (b) 0.70 0.00 None 7 days 2.01 | C0 % Density: gm/cc Cast Metting Point: °C Freezing Point: "C Boiling Point: °C Refractive Index, n ^D ₂₀ n ^D ₂₀ vacuum Stability lest: cc/40 Hrs, at 90°C 100°C 120°C 135°C 150°C 200 Gram Bomb Sand lest: Sand, gm (a) Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Terryl Ballistic Mortar, % TNT: Plate Dent lest: Method Condition 0.00 None Detonation Rate: Confinement Condition Condition Ontiment Condition Obtonation Rate |

HBX-3

| Booster Sensitivity Test: Condition Tetryl, gm Wax, in. for 50% Detonation Wax, gm Density, gm/cc | | Decomposition Equation: Oxygen, otoms/sec (Z/sec) Heat, kilocolorie/mole (AH, kcal/mol) Temperature Range, °C Phase |
|--|---|--|
| Heat of: Combustion, col/gm Explosion, col/gm <i>Gas</i> Volume, cc/gm Formation, col/gm Fusion, col/gm Specific Heat: col/gm/°C 30 [°] C 50 [°] C | (b) 4495 877 491 9.30 0.254 0.254 | Armor Plate Impact Test: 60 mm Mortar Projectile: 50% Inert, Velocity, ft/sec A luminum Fineness 500-lb General Purpose Bombs: Plate Thickness, inches I 11/4 11/4 11/2 |
| Burning Rate: cm/sec Thermal Conductivity: col/sec/cm/°C 35 ^o C | (b) 1.70 x 10 ⁻³ | Bomb Drop Test: T7, 2000-Ib Semi-Armor-Piercing Bomb vs Concrete: |
| Coefficient of Expansion: Lineor, ∆ℓ/inch 0°C 35°C 70°C Hardness, Mohs' Scale: | (b) 40 x 10 ⁻⁴ 83 x 10 ⁻⁴ 130 x 10 ⁻⁴ | Max Safe Drop, ft 500-Ib General Purpose Bomb vs Concrete: Height, ft Trials |
| Young's Modulus: E, dynes/cm² E, lb/inch² Density, gm/cc | (b) 11.5 x 10 ⁹ 1.67 x 10 ⁵ 1.81 | Unaffected Low Order High Order 1000-Ib General Purpose Bomb vs Concrete: Height, ft |
| Compressive Strength: lb/inch ² Vapor Pressure: °C mm Mercury <u>Compressive Strength:</u> lb/inch ² Density, gm/cc | See below 1610 1.81 | Trials Unaffected Low Order High Order |
| Ultimate deformation, 🐔 | 1.37 | |

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HBX-3

| Fragmentation Test: | | Shaped Charge Effectiveness, TNT $=$ | 100: |
|--|--------------|--|-----------------|
| 90 mm HE, M71 Projectile, L ot EGS~1~: Density, gm/cc Charge Wt, Ib | 17: | Glass Cones Steel Hole Volume Hole Depth | Cones |
| Total No. of Fragments: For Composition B | 998 | Color: | Gray |
| For Subject HE For 80/20 Tritonal | 476 616 | Principal Uses: | HE charge |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | | | |
| Total No. of Fragments: For TNT | | Method of Loading: | Cast |
| For Subject HE, | | Loading Density: gm/cc | 1.81 |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | | Storage: | |
| Density, gm/cc | | Method | Dry |
| Blast (Relative to TNT): | (a) | – Hazard Class (Quantity-Distance) | Class 9 |
| Air: 3.25" diameter sphere Peak Pressure ∆psi Catenary Impulse NFOC Pendulum Energy | 25.5 20.6 | Compatibility Group Exudation | Group I None |
| Air, Confined: Impulse | | | |
| Under Water: Peak Pressure Impulse Energy | | | |
| Underground: Peak Pressure Impulse | | | |
| Energy | | | |

HBX-1; HBX-3

| Them 1 a dá tra | Moisture, | Acidity, | 100°C Vac | Stab Test Hours | Hygrosco | picity, % RH |
|--|-------------------|----------|------------------------------|----------------------|---------------|-----------------|
| Explosive Composition | 26 | <u>%</u> | CC gas | nours | 30°C | 71°C |
| Standard HBX-1 +0.2% moisture +0.4% moisture +0.6% moisture | 0.73 | 0.011 | 0.47 0.68 0.62 0.50 | 40 40 40 40 | +2.98 | +1.13 |
| 1992 1 without <u>CaCl</u> e +0.2% moisture +8.4% moisture +0.6% moisture | [!] 0.00 | 0.029 | 0.36 0.25 0.23 0.27 | 40 40 40 40 | -0. 06 | -0,25 |
| HBX-1 with silica gel | 0.06 | 0.031 | 0.73 | 40 | +0.08 | +0.04 |
| Standard HBX-3 +0.2% moisture +0.4% moisture +0.6% moisture | 0.54 | 0.012 | 0.45 0.47 0.43 0.41 | 40 40 40 40 | +2.01 | +0.31 |
| HDX 3 without CaCl +8:2% moisture +0.6% moisture +0.6% moisture | 0.02 | . 0.049 | 0.46 0.26 0.26 0.20 | 40 40 40 40 | -0.06 | -0.29 |
| HBX-3 with silica gel | 0.04 | 0.100 | 0.45 | 40 | +0.09 | +0.05 |
| <u>Standard H-6</u> +0.2% moisture +0.4% moisture +0.6% moisture | 0.71 | 0.017 | 0.47 0.88 0.63 0.65 | 40 40 40 40 | +2.01 | +1.77 |
| H-6 without CaCl +0.2% moisture +0.4% moisture +0.6% moisture | 0.03 | 0.082 | 0.40 0.10 0.25 0.23 | 40 40 40 40 | -0.06 | -0.25 |
| II 6 with silica gel | 0.05 | 0.028 | 0.43 | 40 | +0.09 | +0.06 |

The Stability of HEX Compositions Made With and Without Desiccants and Containing Added Moisture

* All samples were ground to 20/100 mesh size, 7 days before tests. Silica gel used was Fisher Scientific Company, Lot 541492, through 100 mesh U. S. Standard Sieve.

1

Preparation:

HBX explosive mixtures are prepared by melting TNT in a steam-jacketed melt kettle equipped with a mechanical stirrer. Water-wet RDX is added slowly with stirring and heating until all the water is evaporated. Aluminum is added, and the composition is stirred until uniform. D-2 wax and calcium chloride are then added. The desensitizer wax, also known as Composition D-2, consists of 84% paraffin and other waxes, 14% nitrocellulose and 2% lecithin. The mixture is cooled from approximately 95° to 100°C to a temperature considered suitable for casting (the lowest practicable pour temperature). HBX can also be made by adding the calculated amount of TNT to Composition B to obtain the desired proportion of RDX/TNT. The appropriate weights of the other ingredients are added to complete the mixture.

Origin:

Developed during World War 11, as relatively insensitive mixtures, by adding 5% desensitizer to Torpex II, for high blast explosive applications.

References: ³⁴

(a) 0. E. Sheffield, <u>Blast Properties of Explosives Containing Aluminum or Other Metal</u> Additives, PATR No. 2353, November 1956.

(b) S. D. Stein, G. J. Horvat and O. E. Sheffield, <u>Some Properties and Characteristics</u> of HBX-1, HBX-3 and H-6, PATR No. 2431, June 1957.

(c) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute for Tetryl in Boosters</u>, NOL Memo. 10,303, 15 June 1949.

(d) S. R. Walton, <u>Report on the Program to Develop an Improved HBX-Type Explosive</u>, NAVORD Report No. 1502, 26 July 1950.

(e) A. W. O'Brien, Jr., C. W. Plummer, R. P. Woodburn and V. Philipchuk, Detonation Velocity Determinations and Fragment Velocity Determinations of Varied Explosive Systems and Conditions, National Northern Corporation Final Summary Report MNC-F-13, February 1958 (Contract DAI-19-020-501-0RD-(P)-58).

(f) Also see the following Picatinny Arsenal Technical Reports on HBX Explosives: 1756, 2138, 2169.

³⁴See footnote 1, page 10.

<u>HEX-24</u>

| Composition: % | | Molecular Weight: | 47.6 |
|---|--------------|---|--------------------|
| Potassium Perchlorate (17 microns) Aluminum, atomized (20 microns) | 32 48 | Oxygen Balance: CO, % CO % | -42 - 14 |
| RDX (through 325 mesh) Asphaltum (through 100 mesh) | 16 4 | Apparent Apparent Pressea at 20,000 psi Melting Point: "C | 1.39 2.1 |
| C/H Ratio | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 16 24 | Boiling Point: °C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| Steel Shoe | Detonates | cc/40 Hrs, at | |
| Fiber Shoe | Unaffected | 90°C | |
| Rifle Bullet Impact Test: Trials % Explosions Partiols | | 100°C 120°C 135°C 150°C | 1.25 |
| Burned | | 200 Gram Bomb Sand Test: | |
| Unaffected | | Sand, gm | 12.5 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) | | Sensitivity to Initiation: Minimum Detonating Charge, gm | |
| 1 5 520 | | Mercury Fulminate Lead Azide | 0.20 |
| 15 | | Tetryl | 0.25 |
| 20 | | Ballistic Mortar, % TNT: | |
| | | Trauzl Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | | Plate Dent Test: Method | |
| ∣00°C Heat Test: | | Condition | |
| % Loss, 1st 48 Hrs | 0.15 | Confined | |
| % Loss, 2nd 48 Hrs | 0.00 | Density, gm/cc | |
| Explosion in 100 Hrs | None | Brisance, % TNT | |
| lammability Index: | | Detonation Rate: Confinement | |
| Hygroscopicity: % | None | Condition Charge Diameter, in. | |
| Volatility: | None | Density, gm/cc Rate, meters/second | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: |
|--|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: Gray |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: HE filler for small caliber projectiles |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pressed |
| Fragment Velocity: ft/sec | Loading Density: gm/cc Pressed at 20,000 psi 2.1 |
| At 9ft At 25½ ft Density, gm/cc | Storoge: Method Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation None |
| Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Enerav Flame Temperature, ^O K 2552 Activation Energy, kcal 20.4 Temp, ^O C 450 to 570 | Static Tests: 20 mm T215E1 Projectile: PA Peak Pressure, psi 55 NFCC 20" Blast Cube 44 AFG 24" Blast Cube 44 Static Tests: 20 mm M97 Projectile: 20 mm M97 Projectile: 12.4 Exclose 46 Duration, microsec 533 AFG 24" Blast Cube 36 24 32 Heat of: Combustion, cal/gm 1858 Gas volume, cc/gm 159 |
| Specific reaction | |

| Composition: % | Molecular Weight: | 47.6 | | |
|---|--|------------------------|--|--|
| Pctassium Perchlorate 32 (17 microns) Aluminum, flaked (1 micron) 48 | Oxygen Balance: <i>CO</i> , % <i>CO</i> % | -42 -3 ¹ | | |
| RDX (through 325 mesh)16Asphaltum (through 100 nesh)4 | Density: gm/cc Apparent Pressed at 20,000 psi | 0.69 | | |
| | Melting Point: "C | | | |
| C/H Ratio | Freezing Point: "C | | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | Boiling Point: °C | | | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | | | |
| Friction Pendulum Test: Steel Shoe Partially detonates Fiber Shoe Unaffected | Vacuum Stability Test: cc/40 Hrs, at 90°C | | | |
| Rifle Bullet Impact Test: Trials % Explosions Partials | - 100°C 120°C 135°C 150°C | 1.52 | | |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm | 23.7 | | |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) 1 5 545 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl | 0.20 0.25 | | |
| 15 20 | Ballistic Mortar, % TNT: | | | |
| 75°C International Heat Test: % Loss in 48 Hrs | Trauzi lest, % TNT: Plate Dent Test: Method | | | |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | | | |
| Flammability Index: | Detonation Rote: Confinement | | | |
| Hygroscopicity: % | Condition Charge Diameter, in. | | | |
| Volatility: | Density, gm/cc Rate, meters/second | | | |

HEX-48

| Fragmentation Test: | Shaped Charge Effectiveness, TNT $=$ 100: |
|--|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: Gray |
| For Subject HE | Principal Uses: HE filler for small caliber projectiles |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pressed |
| Fragment Velocity: ft/sec | Loading Density: gm/cc Pressed at 20,000 psi 1.62 |
| At 9 ft At 25½ ft | Storage: |
| Density, gm/cc | Method Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation None |
| Air, Confined: Impulse | Static Tests:20 mm T215E1 Projectile:PA Peak Pressure, psi77NFOC 20" Blast Cube45APG 24" Blast Cube42 |
| Under Water: Peak Pressure Impulse | <u>Static Tests:</u> <u>20 mm M97 Projectile:</u> HEX-48 TNT Tetryl |
| Energy Underground: Peak Pressure | Fosboro psi 17.3 2.8 3.5 Catenary-psi 43 28 28 Duration, microsec 517 560 530 APG 24" Blast Cube 29 10 |
| ImpulseEnergyFlame Temperature, OK2382Activation Energy, kcalComp, OCSpecific reactionrate, k7.84 x 10 | Heat of:Combustion, cal/gm4119Explosion, cal/gm1735Gas Volume, cc/gm200 |

AMCP 706-177

HEX-48

Cook-Off Tests: (c)

| _ | | | | _ | | Г |
|-------|----------------|---|-----------------------------|----|-----------|---|
| _ | Projectile No. | , | cut-Off Temp ^O C | | Cook-Off | |
| ; | 1 | | 170 | | Yes (198) | • |
| | 2 | | 150 | İ | 77~ | ī |
| • | 3 | | 155 | | Yes (190) | • |
| ' | 1. | | 150 to 175 | ł. | No | |

20 mm T215E1 HEX-48 Loaded Projectiles With Dye-Coated RDX Top-Off

National Northern Projectile Load:

195

3 1

ļ

| | | | | | <u>Avg. No.</u> <u>Round</u> | of Penetra in Zone 65 | tions_per |
|---|------------|--------|----------------|----|---------------------------------|--------------------------|--------------------|
| , | Projectile | Filler | Altitude, Feet | 26 | 0.020" | 0.040" | 0.051" |
| - | T215E1 | HEX-48 | Ground | | 352 | 264 | 282 |
| | | | 60 ,000 | : | 676 | 432 | (⁻ 388 |

The fragment penetration test records numbers of complete penetrations of aluminum panels of various thicknesses at 2.5 feet from the static detonation. The total penetrations recorded on the 24ST-3 aluminum panels occurred with the projectile nose always pointed toward $^{\circ}$ and the base toward 180° .

The test data indicate that on the thicker panels, 0.040" and 0.051," the HEX-48 loaded T215El projectile produced more complete fragment penetrations at ground and altitude than MOX-2B loaded T282El and EX8 Mod 0 projectiles.

ti

The HEX compositions were prepared by blending the appropriate weight of the dry ingredients in a Patterson-Kelly twin-shell blender for at least 30 minutes.

An alternate procedure for 100 to 200 gram batches used a "Cradle-Roll" mixing device. This device consisted of a half-barrel type container constructed of wood and lined with an electrical conductive material. A plastic roll was allowed to move over the ingredients by remote control action of the container. The roll action prevented caking of the mix but had no adverse effect on the particle size of the ingredients. The period of time required to obtained a uniform and intimate mixture was approximately fifteen minutes.

Origin:

The development of "slow-burning" explosive mixtures which would produce increased blast effects in enclosed or nearly enclosed spaces directed attention to their use for possible military application. In 1950 Picatinny Arsenal developed a high capacity filler for 20mm projectiles consisting of 85/10/5 RDX/aluminum/desensitizer which was more powerful than standard tetryl filler. However, in comparison with MOX type explosives, there was little doubt as to the superior performance of the MOX mixture. HEX (high energy explosive) mixtures were developed at Picatinny Arsenal in 1953 (Ref a) as superior high blast compositions suitable for use in small Caliber projectiles.

References: 35

(a) O. E. Sheffield and E. J. Murray, <u>Development of Explosives—Metallized Explosives—</u> <u>High Blast Fillers for Small Caliber Shell</u>, Picatinny Arsenal Memorandum Report No. MR-49, 21 December 1953.

(b) 0. E. Sheffield, <u>Properties of MOX-Type Explosive Mixtures</u>, PAIR No. 2205, October 1955.

(c) National Northern Corporation, Letter from Dr. C. M. Saffer, Jr., to Commanding Officer, Picatinny Arsenal, 12 June 1957.

³⁵See footnote 1, page 10.

| Composition: | Molecular Weight: $(C_{1l_4} \mathbb{H}_6 \mathbb{N}_8 \mathbb{O}_{1l_4})$ |
|---|--|
| % 0 0 C 33.0 C C H 1.2 NH NH | Oxygen Balance: CO, % -53.4 CO % - 9.4 |
| 21.9 0 ₂ N - 1.0 ₂ 0 ₂ N | Density: gm/cc |
| 43.9 | Melting Point: °C Decomposes 302 |
| C/H Ratio 0.797 NO ₂ NO, | Freezing Point: °C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | Boiling Point: "C |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 15 Sample Wt, mg 12 | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ |
| Friction Pendulum lest: Steel Shoe Unaffected Fiber Shoe Unaffected Rifle Bullet Impact Test: Trials & Explosions Partials | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C 0.40 120°C 135°C 150°C |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm 52.1 |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) 1 5 384 10 15 20 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide 0.30 Tetryl 0.25 Ballistic Mortar, % TNT: |
| | Trauzl lest, % TNT: |
| 75°C International Heat Test: % Loss in 48 Hrs 100°C Heat Test: % Loss, 1st 48 Hrs 0.07 % Loss, 2nd 48 Hrs 0.05 | Plate Dent Test: Method Condition Confined Density, gm/cc |
| Explosion in 100 Hrs None | Brisance, % TNT |
| Flammability Index: | Detonation Rate:, Confinement |
| Hygroscopicity: % 25 ⁰ C, 90% RH 0.19 | Condition Charge Diameter, in. |
| Volatility: | Density, gm/cc Rate, meters/second |

2,4,6,2',4',6'-Hexanitro-oxanilide (HNO)

AMCP 706-177

| Fragmentation Test: | Shaped Charge Effectiveness, TNT $=$ | 100: |
|--|--|-------------|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, lb | Glass Cones Steel Hole Volume Hole Depth | Cones |
| Total No. of Fragments: For TNT | Color: Almo | st white |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Igniter powder; compositions | pyrotechnic |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pressed and e | xtruded |
| | Loading Density: gm/cc | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc | Storage: Method | Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | None |
| Air, Confined: Impulse | | |
| Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | | |

2,4,6,2',4',6'-Hexanitro-oxanilide (HNO)

Solubility in the following substances:

| Solvent | |
|----------------------|--|
| Nitrobenzene | <3 gm in 100 cc, at 23°C ∼ 5 gm in 100 cc, at 210°C |
| Water | 0.10 gm in 100 cc, at 100°C |
| Alcohol (Ethyl) | Insoluble |
| Acetone | Insoluble |
| Benzene | Insoluble |
| Butyl acetate | Insoluble |
| Carbon tetrachloride | Insoluble |
| Dimethylformamide | Very soluble |
| Ether (Ethyl) | Insoluble |
| Acetic Acid | Insoluble |
| Nitric Acid | Soluble |
| Crystalline form | Long rectangular glistening plates from nitrobenzene |

Preparation:

To prepare hexanitro-oxanilide, first prepare tetranitro-oxanilide as described herein under the entry "2,4,2',4'-Tetranitro-oxanilide (TNO)."

A 1.5 liter round bottom flask is equipped with a stirrer of the type which causes a downward swirl. The flask is jacketed for hot and cold water. 187 grams of nitric acid of specific gravity 1.49 (commercial grade) is placed into the flask and 100 grams of sulphuric acid is added to the nitric acid under agitation. The mixed acid is cooled to 10° C. 29.2 grams of tetranitro-oxanilide is slowly added to the mixed acid under rapid agitation maintaining the temperature at 8° - 10° C. After the addition of the TNO is completed (approximately 25 minutes) the temperature is raised to 85° C over a period of 2 hours and held at 85° - 90° C for one hour. The hexanitro-oxanilide (HNO) "slurry" is filtered on a Buchner funnel and purified as explained under "Tetranitro-oxanilide."

Origin:

A. G. Perkin in 1892 obtained hexanitro-oxanilide directly by heating to boiling a solution of tetranitro-oxanilide in a mixture of sulfuric and nitric acids. He also prepared the same compound from oxanilide by the action of a boiling mixture of fuming nitric and sulfuric acids (J Chem Soc <u>61</u>, 462 (1892)).

References: 36

(a) L. Gowen and R. Dwiggens, <u>Case Gun Ignition Studies</u>, NAVORD Report No. 2321, 13 June 1952.

(b) D. Dubrow and J. Kristal, <u>Substitution of Tetranitro Oxanilide and Hexanitro Oxanilide</u> <u>for Tetranitro Carbazole</u>, PA Pyrotechnic Research Laboratory Report 54-TF1-88, 20 December 1954.

(c) S. Livingston, <u>Preparation of Tetranitro Carbazole</u>, PA Chemical Research Laboratory Report 136,330, 11 April 1951.

(d) S. Livingston, Development of Improved Ignition Type Powders, PATR No. 2267, July 1956.

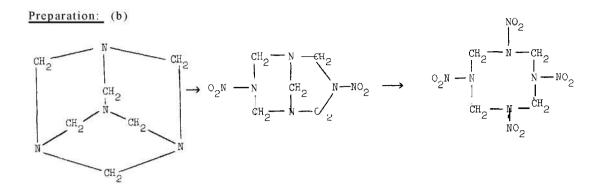
³⁶See footnote 1, page 10.

| Composition: | Molecular Weight: $(C_{4}H_{8}N_{8}O_{8})$ 296 |
|--|---|
| $\begin{bmatrix} C & 16.2 & O_2 N - N & N - NO_2 \\ H & 2.7 & H_2 C & CH_2 \\ H & 2.7 & H_2 C & CH_2 \end{bmatrix}$ | Oxygen Balance: 00, % -21.6 CO % 0.0 |
| $\begin{array}{ c c c c c c c c c c c c c c c c c c c$ | Density: gm/cc Crystal 1.90 |
| 0 43.2 | Melting Point; °C Capillary method 273 Koffer Micro Hot Stage 280 |
| C/H Ratio 0.095 | Freezing Point: "C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 32 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 9 Sample Wt, mg 23 | Boiling Point: "C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ |
| Friction Pendulum Test: Steel Shoe Explodes Fiber Shoe Unaffected | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C 0.37 |
| Rifle Bullet Impact Test: Trials % Explosions | 100°C 0.37 120°C 0.45 135°C |
| Partials Burned | 150°C 0.62 200 Gram Bomb Sand Test: |
| Unaffected | Sand, gm 60.4 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 380 1 5 327 10 306 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide 0.30 Tetryl |
| 15 20 | Ballistic Mortar, % TNT: 150 |
| | Trauzi Test, % TNT: 145 |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method |
| 100°C Heat Test: % Loss, 1st 48 Hrs 0.05 % Loss, 2nd 48 Hrs 0.03 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT |
| Flammability Index: | Detonation Rate: Confinement |
| Hygroscopicity: % 30 ^o C, 95% RH (c) 0.00 Volatility: | Condition Charge Diameter, in. Density, gm/cc Rate, meters/second 9124 |

beta-HMX

| Booster Sensitivity Test: Condition Tetryl, gm Wax, in. for 50% Detonation Wax, gm Density, gm/cc Heat of: Combustion, cal/gm (e) 1356 Gas Volume, cc/gm | Decomposition Equation: Oxygen, otoms/sec (Z/sec) Heat, kilocolorie/mole (AH, kcal/mol) Temperature Range, °C Phase Liquid Armor Plate Impact lest: 60 mm Mortar Projectile: 50% inert, Velocity, ft/sec |
|--|--|
| Formation, cal/gm (e) -60.5 Fusion, cal/gm | Aluminum Fineness 500-lb General Purpose Bombs: |
| Specific Heat: col/gm/°C Recrystallized (g) <u>°c</u> <u>°c</u> -75 0.153 85 0.288 0 0.228 90 0.290 25 0.248 100 0.295 50 0.266 125 0.307 75 0.282 150 0.315 | Plate Thickness, inches 1 1¼ 1¼ 1½ 1¾ |
| cm/sec | Bomb Drop Test: |
| col/sec/cm/°C | 17, 2000-Ib Semi-Armor-Piercing Bomb vs Concrete: |
| Coefficient of Expansion: Linear, %/°C | Max Safe Drop, ft 500-lb General Purpose Bomb ♥ Concrete: |
| Volume, %/°C | Height, ft Trials |
| Hardness' Mohs' Scale: (e) 2.3 | Unaffected Low Order |
| Young's Modulus: E', dynes/cm² E, lb/inch² | High Order |
| E, 10/inch* Density, gm/cc | 1000-Ib General Purpose Bomb ♥ Concrete: |
| Compressive Strength: Ib/inch ² | Height, ft Trials Unaffected |
| Vapor Pressure: "C mm Mercury | Low Order High Order |
| | |

beta-HMX



Two men are required to regulate the addition of reagents and control the temperature during the initial stage addition; one man can complete the procedure. A 1-liter 5-necked flask is used, the center neck for an efficient stirrer, one side neck for a thermometer, and the other necks for burrettes and a gas outlet (to water trap). The flask is placed in a pan with steam and cold water inlets, for temperature control.

Five cc of acetic anhydride and 250 cc glacial acetic acid are poured into the flask and the temperature brought to $45 \pm 1^{\circ}$ C, and held there for the duration of the entire reaction. The reagents (a solution of 33.6 gn hexamine in 55 gn of glacial acetic acid, 100 cc of acetic anhydride and 40 cc of a solution of 42.3/57.7-ammonium nitrate/98% nitric acid) are then added simultaneously, continuously and equivalently over a 25-minute period. The reaction mixture is aged 15 minutes.

The second stage reagents (60 cc of 42.3/57.7, ammonium nitrate/98% nitric acid and 150 cc acetic anhydride) are then added simultaneously, continuously and equivalently over a 25-minute period. The mixture is aged 65 minutes, poured into 1.5 liter of water and simmered on a steam bath for 12 hours. Cool, filter and dry the RDX-HMX precipitate (yield 73% HMX).

The RDX is destroyed, leaving HMX, as follows: 1025 gm of the crude product are placed in a solution of 15 gm sodium tetraborate decahydrate in 5 liters of water, heated to boiling with agitation, and 5 N NaOH added at the rate of 3 cc/min. When about 730 cc have been added the pH increases sharply from a little over 8.7 to over 9.7 which corresponds to complete destruction of the RDX. Filter the HMX from the hot mixture; yield 612 gm, mp 279.5°-280.5°C. Recrystallization from nitromethane yields material melting at $281^{\circ}-282^{\circ}C$.

Origin:

Was discovered as an impurity (by-product) in the nitration of hexamethylene-tetramine to form RDX. It is now manufactured directly by the process described above and has valuable use in explosive systems.

Removal of RDX from HMX-RDX Mixtures and Recovery of a RDX-HMX Mixture (This procedure appears suitable for use with mixtures containing 80% or more HMX):

beta-HMX

Procedure:

500 grams of HMX containing 12.25% RDX are placed in a 1500 cc beaker, 500 cc of acetone is added and the slurry is agitated for several minutes at room temperature. Before complete settling, the RDX-HMX-acetone solution is decanted.

To the residual HMX-RDX, another 500 cc of acetone is added. The slurry is heated on the steambath and while boiling, agitated for several minutes. The boiling RDX-HMX-acetone solution is decanted. The residual HMX is now washed with cold acetone into a funnel. This HMX is now taken up in 95% alcohol, filtered and dried. Yield 353.9 gn or 70.78%.

All the acetone extracts are combined and evaporated to dryness. Yield 137.5 gn or 26.5%.

Yield Balance:

| Pure HMX obtained - 353.9 gn Total RDX-HMX mixture recovered - | 70. 788 |
|---|----------------|
| 137.5 gm Samples taken during process - | 26.50% |
| 2.4 gn Loss during process | 0.48% 2.24% |
| Total | 100.00% |

Various samples were analyzed for RXD content:

| 1. | Crude | HMX | 12.25% RDX |
|-----|---------|------------------------|------------|
| 2. | After | first acetone washing | 6.0% RDX |
| 3. | After | second acetone washing | 2.0% RDX |
| 4. | After | third acetone washing | 0.0% RDX |
| RDX | -HMX sa | ample recovered | 54.5% RDX |

Preparation of Fine Particle-size HMX by the Aspirator Method:

- 1. Dissolve 1100 gm HMX in 4400 cc of dimethyl sulfoxide.
- 2. Filter the HMX solution.
- 3. Connect a clean aspirator to the water line.
- 4. Place a 55 gallon clean drum under the aspirator.
- 5. Fasten a polyethylene tubing, long enough to reach easily to the bottom of the HMXdimethyl sulfoxide container, to the side intake of the aspirator.
- 6. Fasten to the bottom of the aspirator another polyethylene tube long enough to reach to the bottom of the 55 gallon drum.
- Open the water faucet and then place the polyethylene tube in the HMX container. 7.
- 8. White milky fine HMX separates out in the drum. Total duration of run is approximately 7 minutes.
- 9. After all the HMX solution is sucked out of the container, the water is turned off.
- 10. The material is filtered and water washed.
 11. If dry HMX is required, the material can be alcohol and ether washed.

A more efficient method to recover the RDX-HMX mixture:

- 1. Filter the combined hot acetone extracts.
- 2. Pour while agitating the filtered extracts into at least 4 times its volume of water.
- 3. Filter and dry, etc.

beta-HMX

Color:

White

Storage:

| Method | Dry |
|----------------------------------|--------------------------------|
| Hazard Class (Quantity-Distance) | Class 9 |
| Compatibility Group | Group L (dry) Group M (wet) |
| Exudation | None |

References: 37

(a) O. E. Sheffield, E. J. Murray, A. L. Rosen and B. W. Kanouse, <u>Properties of HMX</u>, PA Chemical Research Laboratory Report No. 52-IML-23, 7 April 1952.

(b) W. E. Bachmann, The Preparation of HMX, OSRD Report No. 1981, 3 November 1943.

(c) & Livingston, Characteristics of Explosives HMX and DPMN, PAIR No. 1561, 6 September 1945.

(a) R. J. Finkelstein and G. Gemow, <u>Theory of the Detonation Process</u>, NAVORD Report No. 90-46, 20 April 1947.

(c) 0. H. Johnson, <u>HMX as a Military Explosive</u>, NAVORD Report No. 4371, 1 October 1956.

(f) Also see the following Picatinny Arsenal Technical Reports on HMX:

| <u>1</u> | 3 | <u>6</u> | <u>7</u> | <u>9</u> |
|----------|------|----------|----------|--------------|
| 1741 | 2183 | 2016 | 1737 | 1709 2059 |

(g) C. Lenchitz, W. Beach and R. Valicky, <u>Enthalpy Changes. Heat of Fusion and Specific</u> <u>Heat of Basic Explosives</u>, PATR No. 2504, January 1959.

³⁷See footnote 1, page 10.

| Composition: % | | Molecular Weight: | 91 |
|---|------------|--|-------------|
| HMX | 49 | Oxygen Balance: CO ₂ % CO % | - 51 -27 |
| TMT | 29 | | |
| Aluminum | 22 | Density: gm/cc Cast | 1.90 |
| | | Melting Point: "C | |
| C/H Ratio | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | | Boiling Point: "C | |
| Sample Wt 20 mg | 17 | Refractive Index, n ⁰ ₂₀ | |
| Picatinny Arsenal Apparatus, in. Sample Wt, mg | 25 | n ₂₅ | |
| | - | n ₃₀ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| Steel Shoe | Unaffected | cc/40 Hrs, at | |
| Fiber Shoe | Unaffected | 90°C | |
| Rifle Bullet Impact Test: 10 Trials , | 76 | 100°C | |
| <u>3/16" Steel</u> | 1/8" Al | 120°C | 0.37 |
| Explosions 90 | 50 | 135°C 150°C | |
| Partiais | | 150 C | |
| Burned lo | | 200 Gram Bomb Sand Test: | |
| Unaffected 0 | 50 | Sand, gm | 61.3 |
| Explosion Temperature: | °C | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) | | Minimum Detonating Charge, gm | |
| | | Mercury Fulminate | |
| 5 Flames erratically | 370 | Lead Azide | 0.30 |
| 10 15 | | Tetryl | |
| 20 | | Ballistic Mortar, % TNT: | 120 |
| | | Trauzl Test, % TNT: | |
| 75°C International Heat Test: | | Plate Dent Test: | |
| % Loss in 48 Hrs | | Method | |
| 100°C Heat Test: | | Condition | |
| % Loss, 1st 48 Hrs | | Confined | |
| % Loss, 2nd 48 Hrs | | Density, gm/cc | |
| Explosion in 100 Hrs | | Brisance, % TNT | |
| | | Detonation Rate: | |
| Flammability Index: | | Confinement | None |
| | | Condition | Cast |
| Hygroscopicity: % | | Charge Diameter, in. | 1.0 |
| Volatility: | | Density, gm/cc | 1.90 |
| volatinty. | | Rate, meters/second | 7866 |

HTA-3

| Booster Sensitivity Test: | | Decomposition Equation: |
|--|-----------|---|
| Condition | | Oxygen, otoms/sec |
| Tetryl, gm | | (Z/sec) |
| Wax, in. for 50% Detonation | | Heat, kilocolorie/mole (AH, kcal/mol) |
| Wax, gm | | Temperature Range, °C |
| Density, gm/cc | | Phase |
| | | |
| Heat of: | 3687 | Armor Plate Impact Test: |
| Combustion, cal/gm | 1190 | |
| Explosion, cal/gm | - | 60 mm Mortar Projectile: |
| Gas Volume, cc/gm | 680 | 50% Inert, Velocity, ft/sec |
| Formation, col/gm | | Aluminum Fineness |
| Fusion, cal/gm | | |
| Specific Heats californ (°C | | 500-Ib General Purpose Bombs: |
| Specific Heat: col/gm/°C 32'' to 74 ^o C | 0,245 | Plate Thickness, inches |
| | | |
| | | |
| | | 11/4 |
| | | 11/2 |
| | | 18/4 |
| Burning Rate: | | |
| cm/s ec | | Bomb Drop Test: |
| Thermal Conductivity: | | |
| cal/sec/cm/°C | | T7, 2000-Ib Semi-Armor-Piercing Bomb vs Concrete: |
| | | Max Safe Drop, ft |
| Coefficient of Expansion: Linear, %/°C | | 500 lb Conorol Dumono Pomb un Conorolou |
| | | 500-lb General Purpose Bomb vs Concrete: |
| Volume, %/°C | | Height, ft |
| | | Trials |
| Hardness, Mohs' Scale: | | Unaffected |
| | | Low Order |
| Young's Modulus: | | High Order |
| E, dynes/cm ² | | |
| E, Ib/inch ² | | 1000-Ib General Purpose Bomb vs Concrete: |
| Density, gm/cc | | |
| Compressive Strength: lb/inch ² | 2260 | Height, ft |
| Compressive Strength: ID/Inch* | See below | Trials |
| | | Unaffected |
| Vapor Pressure: | | Low Order |
| °C mm Mercury 2 | * | High Order |
| Compressive Strength: 1b/inch ² Average (10 tests) | 2260 | |
| High | 2530 | Ultimate Deformation: % |
| Low | 1910 | Average (10 tests) 2.81 High 3.22 |
| | | L_{OW} 2.52 |
| * | | $n_{ataly} (3 \text{ gm}) \text{ prograd} at 3 tons (6.000 \text{ lb}) total$ |

* Test specimen 1/2" x 1/2" cylinder (approximately 3 gm) pressed at 3 tons (6,000 lb) total load or 30,000 psi with a 2 minute time of dwell.

<u>HTA-3</u>

| Fragmentation Test: | Shaped Charge Effectiveness, TNT = 100: | |
|--|--|---------|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, lb | Glass Cones Steel Cones Hole Volume Hole Depth | |
| Total No. of Fragments: For TNT | Color: | Gray |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc | Principal User: HE projectile and bomb | filler |
| Charge Wt, Ib | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: | Cast |
| - | Loading Density: gm/cc | 1.90 |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | |
| Density, gm/cc | Method | Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 |
| Air: Peak Pressure | Compatibility Group | Group I |
| Impulse Energy | Exudation | None |
| Air, Confined: Impulse | Work to Produce Rupture:ft-lb/inch3Average (10 tests)2.77High3.39 | , |
| Under Water: Peak Pressure Impulse Energy | Low 2.40 Efflux Viscosity, Saybolt Seconds: | 24.8 |
| Underground : Peak Pressure Impulse Energy | | |
| ~ | *Test specimen 1/2" x 1/2" cylinder (mately 3 gm) pressed at 3 tons (6,00 total load or 30,000 psi with a 2 m time of dwell. | 0 1b) |

| | Modulus | of | Elasticity: | Ŷ |
|--|---------|----|-------------|---|
|--|---------|----|-------------|---|

| | | lb/inch ² |
|---|---------|----------------------|
| | Average | 89,200 |
| 1 | High | 97,400 |
| * | Low | 76,300 |

* Test specimen 1/2" x 1/2" cylinder (approximately 3 gm) pressed at 3 tons (6,000 lb) total load or 30,000 psi with a 2 minute time of dwell.

Setback Sensitivity Test: (a)

| Critical Pressure | 119,000 psi * |
|-------------------|---------------|
| Density, gm/cc | 1.92 |

* Pressure below which no initiation is obtained and above which an increasing percentage of initiations can be expected as the setback pressure increases.

Preparation:

Procedure similar to that used for Torpex.

References: 38

(a) 1st Indorsement from Chief, Explosives Development Section, to Chief, Explosives Research Section, Picatinny Arsenal, dated 12 May 1958. Subject: "Properties of Octols and HTA-3."

(b) R. Brown and R. Velicky, <u>Heat Capacity of HTA-3</u>, Picatinny Arsenal General Laboratory Report No. 58-H1-509, 5 May 1958.

³⁸See footnote 1, page 10.

Lead Azide

| Composition: | Molecular Weight: (PbN ₆) 291 |
|--|--|
| % N 28.8 N = N = N - Pb - N = N = N | Oxygen Balance: 0, % -5:5 |
| Pb 71.2 | Density: gm/cc Crystal 4.80 Destrinated 4.38 |
| | Melting Point: "C Decomposes |
| C/H Ratio | Freezing Point: °C |
| Impact Sensitivity, 2 Kg Wt: Pure Bureau of Mines Apparatus, cm 10 17 | Boiling Point: °C |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 3 5 | Refractive Index, n ^D ₂₀ |
| Sample Wt, mg 30 28 | n ⁰ 25 n ₃₀ |
| Friction Pendulum Test: | - |
| Steel Shoe Exp 10 des | Vacuum Stability Test: <u>Dextrinated</u> cc/40 Hrs, at |
| Fiber Shoe Explodes | 90°C |
| Rifle Bullet Impact Test: Trials | 100°C 1.0 120°C 0.07 |
| % Explosions | 135°C |
| Partials | 150°C |
| Burned | 200 Gram Bomb Sand Test: |
| Unaffected | Sand am Black powder fuse 19.0 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 396 | Sensitivity to Initiation: Minimum Detonating Charge, gm |
| 1 356 5 Explodes 340 | Mercury Fulminate |
| 5 Explodes 340 10 335 | Lead Azide |
| 15 335 | Tetryl |
| 20 335 | Ballistic Mortar, % TNT: |
| 75°C International Heat Test: | Trauzl Test, % TNT : (a) 39 |
| % Loss in 48 Hrs | Plate Dent Test: Method |
| 100°C Heat Test: | Condition |
| % Loss, 1st 48 Hrs 0.34 | |
| % Loss, 2nd 48 Hrs 0.05 | Density, gm/cc Brisance, % TNT |
| Explosion in 100 Hrs None | |
| Flammability Index: | Detonation Rate: <u>Pure Lead Azide</u> Confinement |
| Hygroscopicity: % Dextrinated Not Dextrinated 30°C, 90% RH 0.8 0.03 | Condition Pressed Charge Diameter, in. |
| Volatility: | Density, gm/cc 2.0 3.0 4.0 Rate, meters/second 4070 4630 5180 |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: |
|---|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: White-buff |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Detonators, priming compositions, and commercial blasting caps |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pressed |
| Fragment Velocity: ft/sec | Loading Density: gm/cc p s i x 10 ³ 3 5 10 15 2.62 2.71 2.96 3.07 |
| A t 25½ ft Density, gm/cc | Storage: Method Wet |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 |
| Air: Peak Pressure Impulse Energy | Compatibility Group Group M (wet) Exudation None |
| Air, Confined: Impulse | <u>Compatibility with Metals:</u> Dry lead azide does not react with or cor- rode steel, iron, nickel, aluminum, lead, zinc, copper, tin or cadmium. It does not |
| Under Water: Peak Pressure Impulse Energy | affect coatings of acid-proof black paint, oil, NRC compound or shellac. Lead azide in the presence of moisture corrodes zinc and copper; and with copper, it forms the extreme. ly sensitive and dangerous copper azide. |
| Underground: Peak Pressure | Specific Heat: cal/gm/ ^O C |
| Impulse Energy <u>Heat of:</u> Combustion, cal/gm 6 30 | -50 0.110 0 0.110 25 0.110 50 0.110 |
| Explosion, cal/gm 367 Gas Volume, cc/gm 308 Formation, cal/gm -346 | Thermal Conductivity: cal/sec/cm/°C (Pure)1.55 x 10~4 |

Lead Azide

Compatibility with Metals:

Dry: Steel, iron, nickel, aluminum, lead, zinc, copper, tin, stainless steel, brass and bronze were unaffected by six years' contact with dry lead azide at ambient temperature and 50°C. Monel, chrome-nickel and Inconel were unaffected under the same conditions' in two and one-half years.

<u>Wet:</u> Copper and zinc are rapidly attacked by moist lead azide, while aluminum is not attacked in 24 hours. Monel, chrome-nickel and Inconel are not attacked by lead azide $(\frac{1}{2}\%)$ moisture) after 29 months' exposure at ambient temperature and 50°C, and J-1 magnesium-aluminum alloy is very slightly corroded.

| Sample Tested | Lead Azide Dry | <u>p</u> | <u>Azide</u> lus Water | Lead A plu 20% Wa | S | Lead Azide plus 20% Ethyl Alba- |
|---|---------------------------|---|------------------------------|-------------------------|------------------|---------------------------------------|
| Friction Pendulum T | est: | | | | | |
| (All IA dextrinated) |) | | | | | |
| Shoe | Fiber | F iber- | Steel- | Fiber | Steel | Fiber |
| No. of Trials Explosions Cracklings Unaffected | 1 1 0 | $ \begin{array}{c} 10 \\ 0 \\ 0 \\ 10 \end{array} $ | 12 0 2 10 | 10 0 0 10 | 4 1 2 1 | 1 1 0 0 |
| Impact Sensitivity, | 2 Kg Wt: | | | | | |
| (All IA dextrinated) | | | | | | |
| PA Apparatus, inc | ches 4 | 9 | | | 9 | 4 |
| Activation Energy: | (c) | | | | | |
| Kcal/mole Induction Period, | seconds | 23.74 0.5-10 | | | | |
| Initiating Efficienc | y, Grams Requi | ired to Giv | ve Complet | e Initiati | ions of: | |
| | | Dextrinate | ed Azide (| gm) | | |
| TNT 0.25 Tetryl 0.10 RDX 0.05 PEIN 0.02 | | | | | | |
| Sensitivity to Stati | c Discharge, J | oules (Pu | e Lead Az | ide) (b) | | 0.0070 |

Lead Azide

| Compatibility of Dextrinated Lead Azide with Black | Powder: |
|--|---------|
| 100°C Vacuum Stability Test, cc/40 hr: | |

| Sample Wt (g | <u>m)</u> | Material | cc |
|----------------------|-----------------------|---|----------------------|
| 1.0 1.0 2.0 | | Lead Azide Black Powder 50/50,Lead Azide/Black Powder | 0.50 0.38 1.26 |
| Solubility of Pure I | Lead Azide; gm/100 gn | n of Water: | |
| <u>°a</u> | | <u>K</u> | |
| 20 | | 0.05 | |

Preparation of Lead Azide (Dextrinated): (du Pont procedure)

2 Na – N = N = N + Pb $(NO_3)_2 \rightarrow Pb(N_3)_2 + 2 NaNO_3$

<u>Lead nitrate solution</u>: This is prepared by dissolving 164 lbs lead nitrate and 8.25 lbs dextrine in deioni'zed water, the solution allowed to settle, and sodium hydroxide added to bring the solution to a pH of 5.4. The final concentration of the solution is then adjusted to 7.4% lead nitrate, 0.375% dextrine by addition of deionized water.

The lead azide is precipitated at a solution temperature of $160^{\circ}F$, using 60 parts lead nitrate and 50 parts sodium azide solution. The latter is added to the former in 23 minutes, under agitation (no baffles are used in the precipitation vessel), the mixture cooled to room temperature in 12 minutes, and allowed to settle 10 minutes. The mother liquor is decanted and the remaining slurry washed before packing.

Origin:

First prepared in 1891 by T. Curtius (Ber 24, 3345-6) by adding lead acetate to a solution of sodium or ammonium azide. F. Hyronimus (French Patent 384,792) should be credited with the first attempt in 1907 to use lead azide with some success in the explosive industry. Its commercial manufacture started in Europe before World War II and in the United States since 1931 as military or commercial grade "dextrinated" lead azide.

Destruction by Chemical Decomposition:

Lead azide can be decomposed by

(1) mixing with at least five times its weight of a 10% solution of sodium hydroxide and allowing the mixture to stand for 16 hours. Decant the supernatant solution of sodium azide and drain into the soil.

(2) dissolving in a 10% solution of ammonium acetate and adding a 10% solution of sodium or potassium bichromate until no more lead chromate is precipitated.

(3) wetting with 500 times its weight of water, slowly adding 12 times its weight of 25% sodium nitrite, stirring, and then adding 14 times its weight of 36% nitric or glacial acetic acid. A red color produced by the addition of ferric chloride solution indicates Lead Azide is still present.

Lead Azide

(4) dissolving in 50 times its weight of 15% ceric ammonium nitrate. The azide is decomposed with the evolution of nitrogen.

References: 39

(a) Ph. Naoum, Z ges Schiess Sprengstoffw, 181, 229, 267 (27 June 1932).

(b) F. W. Brown, D. H. Kusler and F. C. Gibson, <u>Sensitivity of Explosives to Initiation</u> by Electrostatic Discharges, U. S. Dept of Int, Bureau of Mines, RI 3852, 1946.

(c) C. Lenchitz, <u>Ice Calorimeter Determination of Enthalpy and Specific Heat of Eleven</u> Organometallic Compounds, PATR #2224, November 1955.

(d) Also see the following Picatinny Arsenal Technical Reports on Lead Azide:

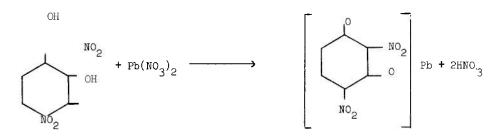
| 0 | <u>1</u> | 2 | <u>3</u> | <u>1</u> | <u>5</u> | 6 | <u>7</u> | <u>8</u> | 2 |
|----------------------------------|----------------------------|--|---|--|----------------------------|---|--|---|--|
| 550 580 600 760 1450 | 561 861 1451 1651 | 832 852 882 932 1132 1152 1352 1372 | 393 1393 1493 2093 21 33 | 534 784 824 944 2164 2204 | 255 525 1325 1485 | 326 856 866 1316 1486 1556 | 567 637 657 707 1737 2227 | 628 708 748 788 838 1388 1528 1838 2198 | 609 719 749 769 849 999 2179 |

³⁹See footnote 1, page LO.

| Composition: | Molecular Weight: (PbC6H2N206) 405 | | | |
|--|--|--|--|--|
| $ \begin{array}{c} & & & \\ & & \\ & & \\ & & \\ & H & & 0.5 \\ & N & & 6.9 \\ & & & & \\ & & & \\ & & & & \\ & & & \\ & & & & \\ & & & & \\ & & & \\ & & & & $ | Oxygen Balance: CO, % -32 CO % - 8 | | | |
| 0 23.7 Pb 51.1 | Density: gm/cc _{Crystal} 3.2 | | | |
| | Melting Point: "C | | | |
| C/H Ratio 0.549 | Freezing Point: "C | | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 1 kg wt 30 | Boiling Point: "C | | | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg 20 | Refractive Index, n_{20}^{D} n_{23}^{D} n_{30}^{D} | | | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C | | | |
| Rifle Bullet Impact Test: Trials % Explosions Partio Is | - 100°C 120°C (73 minutes) Exp Modes 135°C 150°C | | | |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sond, gm Black powder fuse 20 | | | |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) 1 5 Explodes 265 10 15 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl | | | |
| 20 | Ballistic Mortar, % TNT: | | | |
| 75°C International Heat Test: % Loss in 48 Hrs | TrouzI Test, % TNT: Plate Dent Test: Method | | | |
| 100°C Heat Test: % Loss, 1st 48 Hrs 0.20 % Loss, 2nd 48 Hrs 0.02 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT | | | |
| Flammability Index: | Detonation Rote: Confinement | | | |
| Hygroscopicity: % 30°C, 90% RH 0.73 | Condition Charge Diameter, in. | | | |
| Volatility: | Density, gm/cc Rate, meters/second | | | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | |
|---|---|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, 1b | Glass Cones Steel Cones Hole Volume Hole Depth | |
| Total No. of Fragments: For TNT | Color: Red or yellow | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, lb | Principal Uses: Electric detonators | |
| Total No, of Fragments: For TNT | Method of Loading: Pressed | _ |
| For Subject HE | Loading Density: gm/cc | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | _ |
| Density, gm/cc | Method Wat | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) $Class 9$ | |
| Air: Peak Pressure Impulse | Compatibility Group Exudation None | |
| Energy Air, Confined: Impulse | Initiating Efficiency: 0.4 gn LDNR does not initiate tetryl pressed at 3000 psi. | |
| Under Water: Peak Pressure Impulse Energy | Heat of: Explosion, cal/gm 270 | |
| Underground: Peak Pressure Impulse Energy | | |

Preparation:



To a solution of 5 grams of purified dinitroresorcin and 2.65 grams of anhydrous sodium carbonate in 500 cc of boiling water is added slowly a solution of 10 grams of lead nitrate dissolved in 60 cc of boiling water. The reaction mixture is constantly stirred during the addition of the lead salt and for about an hour afterward while the solution is allowed to cool to room temperature. The precipitate is filtered and washed thoroughly first with water and then with alcohol and ether. It is dried in a steam oven.

Origin:

2,4-dinitroresorcin was described in the 1881 edition of Beilstein (Beil VII, 885). The same compound was described in more detail by Weselsky, Benedikt and Hübl in 1882 (M 11, 323). The lead salt of 2,4-dinitroresorcinol appears to have been prepared between World War I and World War II by treating resorcinol with nitrous acid and oxidizing the resulting dinitrosoresorcinol to dinitroresorcinol. Lead nitrate solution was then added to a solution of the 2,4-dinitroresorcinol to which sodium carbonate had been added to form the soluble sodium salt (J. D. Hopper, PATR No. 480, March 1934). The LDNR exists in two forms differing in physical characteristics but possessing similar explosive properties. These forms are red and orange in color (K. S. Warren, PATR 1448, September 1944).

References: 40

(a) See the following Picatinny Arsenal Technical Reports on Lead 2,4-Dinitroresorcinate:

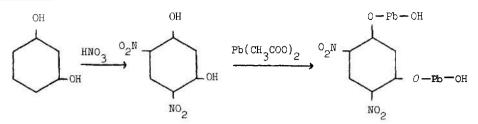
| <u>o</u> | <u>3</u> | <u>4</u> | 8 | <u>9</u> |
|------------|----------|----------|--------------|-------------|
| 480 580 | 453 | 1004 | 1328 1448 | 859 1079 |

⁴⁰See footnote 1, page 10.

| Compositions | Molecular Weight: (PboCcHi, NoCa) 646 |
|--|--|
| Composition: | Molecular Weight: (Pb ₂ C ₆ H ₄ N ₂ O ₈) 646 |
| $^{\%}$ 0 - Pb - 0H C 11.2 H 0.6 $_{2}N$ 0H N 4.3 $_{2}N$ 0H | Oxygen Balance: -20 CO % - 5 |
| 0 19.8 Pb 64.1 0 - Pb - OH | Density: gm/cc |
| Υ NO ₂ | Melting Point: °C 213 |
| C/H Ratio 0.177 | Freezing Point: "C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 1 kg wt 60 | Boiling Point: °C |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg 20 | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ |
| Friction Pendulum Test: | Vacuum Stability Test: |
| Steel Shoe | cc/40 Hrs, at |
| Fiber Shoe | 90°C |
| Rifle Bullet Impact Test: Trials % | 100°C 120°C |
| Explosions | 135°C |
| Partials | 150°C |
| Burned | 200 Gram Bomb Sand Test: |
| Unaffected | Sand powder fuse 15 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Explodes 295 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide |
| 15 | Tetryl |
| 20 | Ballistic Mortar, % TNT: |
| 75%0 https:// | Traurl Test, % TNT: |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method |
| 100°C Heat Test: | Condition |
| % Loss, 1st 48 Hrs 0.4 | Confined |
| % Loss, 2nd 48 Hrs 0.0 | Density, gm/cc |
| Explosion in 100 Hrs None | Brisance, % TNT |
| Flammability Index: | Detonation Rate: Confinement |
| Hygroscopicity: % | Condition Charge Diameter, in. |
| Volatility: | Density, gm/cc Rate, meters/second |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | |
|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | |
| Total No. of Fragments: For TNT For Subject HE | Color: Red or yellow Principal Uses: Electric detonators | |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pressed | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc | Loading Density: gm/cc Storage: Method Wet | |
| Blast (Relative to TNT): Air: Peak Pressure Impulse | Hazard Class (Quantity-Distance) Class 9 Compatibility Group Exudation None | |
| Energy Air, Confined: Impulse Under Water: Peak Pressure | Initiating Efficiency: 0.4 gm LDNR Basic does not initiate tetryl pressed at 3000 psi. | |
| Impulse Energy | | |
| Underground: Peak Pressure Impulse Energy | | |





(a) One hundred grams of pure resorcin is fused in a porcelain casserole and immediately poured on a glass plate. After cooling, the cake is ground in a mortar to pass a U. S. Standard No. 6 mesh screen. Four hundred grams of 98 percent nitric acid in a one pint capacity Dewar jar is stirred mechanically while carbon dioxide snow is added in small pieces. When the temperature falls to -20° C, 40 grams of the granulated resorcin is added in small quantities. Simultaneous addition of solid carbon dioxide as required prevents a rise of temperature of more than 5 degrees throughout the entire experiment. Five minutes after the last portion of resorcin is introduced, the mixture is further cooled to minus 50° C, and finally drived, weight 43.6 grams. The crude 4,6-DNR is purified by first dissolving the product in an aqueous 5 percent sodium hydroxide solution (17.4 grams of sodium hydroxide in 340 cc of water). The resulting solution is then neutralized by gradually adding it to a boiling solution of 21.4 grams of 98 percent sulphuric acid in 150 cc of water. The resulting precipitate of 4,6-DNR is filter and air-dried. Yield, 27.5 grams (37.8 percent of the theoretical).

(h) Five hundredths (0.05) mole (18.96 grams) of lead acetate is dissolved in 67 cc of warm water, into which is gradually stirred 0.10 mole (4.0 grams) of sodium hydroxide dissolved in 67 cc of water. Stirring is continued for five minutes. After settling, the white lead hydroxide is washed by decantation three times with 100 cc portions of distilled water, and used immediately for the next operation.

(c) A 0.0278 mole (5.56 grams) quantity of the 4,6-DNR prepared under (a) above, is dispersed in 270 cc of water by vigorously beating with a motor stirrer. After heating this dispersion to 90°C, the 0.05 mole of lead hydroxide prepared above in slurry form is introduced in **small** portions. Agitation is continued for three hours at 90°C. The basic lead 4,6-DNR is washed once by decantation, and again on the filter with alcohol. After drying overnight in a desiccator charged with calcium chloride, the product weighs 15.6 grams.

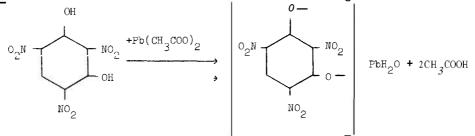
Origin:

Roth the 2,4- and 4,6-dinitroresorcin were described in some detail by Weselsky, Benedikt and Hübl in 1882 (M 11, 323). Typke prepared the 4,6-dinitroresorcin in 1883 by hydrolyzing the nitration product of resorcin diacetate (Ber 16, 551). A more direct and economical method of preparation suitable for production scale manufacture was developed during World War II by the British (Ministry of Supply Pouch Item W-154-21a, "Manufacture of 4,6-Dinitroresorcin and Lead 4,6-Dinitroresorcinate"). This procedure consisted of preparing 4,6dinitroresorcinol by direct nitration of granulated resorcin and allowing the product in slurry to react with an excess of lead hydroxide at 90° C. This basic salt can be prepared in two forms: (1) a micro-crystalline, yellow, low-density form and (2) a denser, brick-red form. Both products have the same chemical composition and the same sensitivity to impact (PATR 1448, September 1944).

| Composition: NO2 | Molecular Weight: (PbC ₆ H N 0) 468 |
|--|---|
| $ \begin{array}{c c} & & & & & & & \\ C & & 15.4 & & & & \\ H & & 0.6 & & & & \\ N & & 9.0 & & & & \\ \end{array} $ | Oxygen Balance: -19 CO % 2 |
| 0 30.8 Pb 44.2 | Density: gm/cc Crystal 3.02 |
| NO | Melting Point: "C Explodes 260-310 |
| C/H Ratio 0.320 | Freezing Point: "C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 17 | Boiling Point: "C |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 3; (8 oz wt) 8 Sample Wt, mg 22 | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ |
| Friction Pendulum Test: Steel Shoe Detonates Fiber Shoe Detonates | Vacuum Stability Test: cc/40 Hrs, at 90°C |
| Rifle Bullet Impact Test: Trials | 100°C 0.4 120°C 0.3 |
| % Explosions Portials | 135°C 150°C |
| Burned Unaffected | 200 Grom Bomb Sand Test: Sand, gm 24 Black bowder_fuse |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) 1 5 Explodes 282 10 276 15 272 20 267 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Trace* Lead Azide Trace* * <.001 gm, alternative Ballistic Mortar, % TNT: |
| | Trauzi Test, % TNT: (a) 40 |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method |
| 100°C Heat lest: % Loss, 1st 48 Hrs 0.38 % Loss, 2nd 48 Hrs 0.73 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT |
| Flammability Index: | Detonation Rate: Confinement |
| Hygroscopicity: % 25 ^o C, 100% RH 0.05 30 ^o C, 90% RH 0.02 | Condition Charge Diameter, in. |
| Volatility: | Density, gm/cc 2.9 Rate, meters/second 5200 |

| Fragmentation lest: | Shaped Charge Effectiveness, TNT : | = 100: | | | | |
|---|---|----------------------------------|--|--|--|--|
| <i>90</i> mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | | | | | |
| Total No. of Fragments: For TNT | Color: Orange-reddish | brown | | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Igniting charge, and ingredient of priming compositions | | | | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: | Pressed | | | | |
| Fragment Velocity: ft/sec | Loading Density: gm/cc | | | | | |
| At 9 ft At 25½ ft | Storage: | | | | | |
| Density, gm/cc | Method | Wet | | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 | | | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | Group M (wet) None | | | | |
| Air, Confined: Impulse | Activation Energy: kcal/mol | 75.39 | | | | |
| Under Water: Peak Pressure Impulse Energy | Induction Period, sec <u>Specific Heat: _cal/cm/°C</u> | 0.5-10 (c) | | | | |
| Underground: Peak Pressure Impulse Energy <u>Heat of:</u> Combustion, cal/gm 1251 Explosion, cal/gm 457 | -50 0 25 50 | 0.141 0.158 0.164 0.167 | | | | |
| Explosion, cal/gm 457 Gas Volume, cc/gm 368 Formation, cal/gm -92 | | | | | | |

Preparation:



Dissolve 14.4 gn lead nitrate and 1 cc of 36% acetic acid in 320 cc distilled water. Dissolve 4 gn 2,4,6-trinitroresorcinol and 1.73 gn sodium carbonate in 80 cc distilled water. Add the lead acetate solution to the trinitroresorcinol solution, under agitation, keeping the temperature at 70° - 75° C and continue stirring for 3 hours at this temperature. Cool to 20° C in 5 hours. Evaporate the solution to 1/3 its volume, cool, filter and wash the product well with water (to neutrality).

| Sensitivity to Static Discharge, joules: (b) | | | | | |
|--|-------------------------|--|--|--|--|
| Loss in Weight at 105°C; % | | | | | |
| 3 hours 6 hours 9 hours | 0.02 0.23 0.23 | | | | |
| Effect of Storage for 2 Months at 80°C, on: | | | | | |
| Explosion Temperature Test Value Sand Test Value Sensitivity to Initiation | N i 1 N i 1 N i 1 | | | | |
| Solubility, gm/100 gm (%) in: | | | | | |
| Glycol Diacetate | | | | | |

| Glycol | Diacetate |
|----------------|-----------|
| °C | Z |
| 20 - 25 | 0.1 |

Origin:

First described in 1914 by von Hurtz and found to be a relatively poor initiator by Wallbaum in comparison to other primary explosives. (2 ges Schiess Sprengstoffw (2, 126, 161, 197, 1939)). Moisak showed that lead styphnate could be used as an insulating (cover) material for lead azide providing protection from mechanical and chemical influences and, at the same time, increasing the detonating ability of the total charge (Transactions of Butlerov Inst Chem Tech Kasan (Russia) (2, 81-5, 1935).

Lead Styphnate

Destruction by Chemical Decomposition:

Lead sty-phnate is decomposed by dissolving it in at least 40 times its weight of 20% sodium hydroxide or 100 times its weight of 20% ammonium acetate and adding a solution of sodium dichromate, equal to half the weight of styphnate and 10 parts of water.

References: 41

(a) Report AC-956/Org Ex 74.

(b) F. W. Brown, D. H. Kusler and F. C. Gibson, Sensitivity of Explosives to Initiation by Electrostatic Discharges, U. S. Dept of Int, Bureau of Mines, RI 3852, 1946.

(c) C. Lenchitz, Ice Calorimeter Determination of Enthalpy and Specific Heat of Eleven Organometallic Compounds, PAIR No. 2224, November 1955.

(d) Also see the following Picatinny Arsenal Technical Reports on Lead Sty-phnate:

| <u>o</u> | 1 | 2 | <u>3</u> | <u>4</u> | 6 | ユ | 8 | 9 |
|--------------|----|--------------|---------------------|----------|------|---------------------|-----|------|
| 1450 2220 | 11 | 1352 2032 | 45 3 2093 | 2164 | 1316 | 407 1737 2077 | 318 | 2179 |

⁴¹See footnote 1, page 10,

| Composition: | Molecular Weight: (C ₆ H ₈ N ₆ 0 ₁₈) 452 |
|--|---|
| % ^{CH} 2 ^{ONO} 2 | Oxygen Balance: |
| c 15.9 ⁰ 2 ^{NOCH} | CO, % 7.1 |
| н 1.8 ^о 2 ^{Nocн} | CO % 28.3 |
| N 18.6 HCONO ₂ | Density: gm/cc 1.73 |
| $\frac{\text{HCONO}_2}{2}$ | Melting Point: °C 112-113 |
| C/H Ratio 0.133 | Freezing Point: "C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 11 | Boiling Point: "C Decomposes 150 |
| Sample Wt 20 mg | Refractive Index, n ^D ₂₀ |
| Picatinny Arsenal Apparatus, in. 4 | n ^D ₂₅ |
| Sample Wt, mg 11 | n ₃₀ |
| Friction Pendulum Test: | |
| Steel Shoe Detonates | Vacuum Stability Test: cc/40 Hrs, at |
| Fiber Shoe Unaffected | 90°C |
| | 100°C |
| Rifle Bullet Impact Test: Trials | 120°C |
| % | 135°C |
| Explosions | 150°C |
| Partials Burned | 200 Over Death Oracl Test |
| Unaffected | 200 Gram Bomb Sand Test: Sand, gm 68.5 |
| | |
| Explosion Temperature: "C | Sensitivity to Initiation: |
| Seconds, 0.1 (no cap used) 160-170 (a) | Minimum Detonating Charge, gm Mercury Fulminate |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | |
| 10 | Lead Azide 0.06 Tetryl |
| 15 | |
| 20 | Ballistic Mortar, % TNT: |
| | Trauzl Test, % TNT: (c) 172 |
| 75°C International Heat Test: % Loss in 48 Hrs 0.4 | Plate Dent Test: |
| | Method |
| 100°C Heat Test: | Condition |
| % Loss, 1st 48 Hrs | Confined |
| % Loss, 2nd 48 Hrs | Density, gm/cc |
| Explosion in 100 Hrs (Frothed) 48 hours | Brisance, % TNT |
| | Detonation Rate: (d) |
| Flammability Index: | Confinement Yes |
| where we apply and put to the | Condition Pressed |
| Hygroscopicity: % 30 ^o C, 90% RH 0.17 | Charge Diameter, in. 0.5 |
| Volatility: | Density, gm/cc 1.73 |
| volatinty. | Rate, meters/second 8260 |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | | | | |
|---|---|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, ≀b | Glass Cones Steel Cones Hole Volume Hole Depth | | | | |
| Total No. of Fragments: For TNT | Color: | | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Secondary charge in detonators (ref i), and in blasting caps designed to be initiated by a fuse (ref j) | | | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pressed | | | | |
| | Loading Density: gm/cc | | | | |
| Fragment Velocity: ft/sec At 9 ft At 251/ ₂ ft | Storage: | | | | |
| Density, gm/cc | Method Dry | | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 | | | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation None | | | | |
| Air, Confined: Impulse | <u>65.5[°]C KI Test:</u> Minutes 6 | | | | |
| Under Water: Peak Pressure | Heat of: (e, f, g) | | | | |
| Impulse Energy | Combustion, cal/gm 1515 1525 Explosion, cal/gm 1390 1454 1468 1520 Formation, cal/gm 337 345 366 | | | | |
| Underground: Peak Pressure | | | | | |
| Impulse Energy | | | | | |
| | | | | | |

Solubility:

- a. Insoluble in water.
- b. Slightly soluble in cold alcohol (2.9 gm at 13°C).
- c. Slightly soluble in ether (4 gm at 9° C).
- d. Very soluble in hot alcohol.

Preparation: (Laboratory Method) (k)

a. Cool to below 0° C, 50 gm of 98%-100% nitric acid placed in a 300 milliliter Erlenmeyer Pyrex flask provided with a thermometer and immersed in an ice-salt mixture.

b. Introduce in small portions, 10 gm of d-mannitol, while swirling the flask to break up any lumps of mannite which might form. Keep the temperature below $0^{\circ}C_{\bullet}$.

c. After solution is complete, add 100 gm of concentrated sulfuric acid from a dropping funnel, swirling the flask in an ice-salt mixture to keep the temperature below 0°C.

d. Filter the resulting porridge-like slurry through a filter paper previously hardened by treatment with mixed acid.

e. Rinse the precipitate directly on the filter with water followed by dilute aqueous sodium carbonate and finally with water. (The resulting crude mannitol hexanitrate gives 18.2% N as determined by the nitrometer.)

f. Dissolve the crude mannitol hexanitrate in boiling alcohol and filter through a waterheated funnel.

 $g_{\rm .}$ Bring the filtrate to boiling and gradually add hot water until the appearance of the first turbidity.

h. Cool in an ice-salt bath, separate and dry the crystals. (Yield should be about 23 gm of material, melting at $112^{\circ}-113^{\circ}$ C and having 18.58% N, the nitrogen being determined by the nitrometer. Theoretical yield would be 24.8 gm.)

Origin:

Mannitol hexanitrate was discovered in 1847 by Ascanio Sobrero who recommended it as a substitute for mercury fulminate in percussion caps (Comp rend, 1847, 121). It is the hexanitric ester of d-mannitol which is widely distributed in nature, particularly in the plant Fraxinus ornus. N. Sokoloff, a Russian chemist, investigated the explosive properties of HM and recommended in 1878 a method of preparation. Mannitol hexanitrate was thoroughly studied by Berthelot, Sarran and Vieille, Domonte, Menard, Strecker, Tichanowich (Ph. Naoum, Nitroglycerin and Nitroglycerin Explosives, Baltimore, 1928, pp. 156, 247-250), and particularly by J. H. Wigner (Ber <u>36</u>, 796 (1903)). More recent data have been reviewed by Guastalla and Racciu ("Modern Explosives," Industria Chimica <u>8</u>, 1093-1102 (1933)).

References:⁴²

(a) G. C. Hale, Abstract of Available Information on the Preparation and Explosive Properties of Hexanitromannite, PA Special Report No. 238, 30 July 1925.

⁴²See footnote 1, page 10.

(b) C. A. Taylor and W. H. Rinkenbach, "Sensitiveness of Detonating Compounds to Frictional Impact, Impact, and Heat," J. Frank Inst 204, 369-76 (1927).

(c) Ph. Naoum, Z ges Schiess - Sprengstoffw (Munich), pp. 181, 229, 267 (27 June 1932).

- (d) H. Kast, Z angew Chem, <u>36</u>, 74 (1923).
- (e) A. Schmidt, Z ges Schiess Sprengstoffw 29, 262, (1934).

Landolt and Börnstein, E III, p. 2914.

(f) A. Marshall, <u>Explosives, Their Manufacture, Properties, Tests, and History</u>, Vol 111, London (1932) p. 39. Ph. Naoum, <u>Nitroglycerin and Nitroglycerin Explosives</u>, Baltimore, (1928), pp. 156, 247-250.

(g) A. Schmidt, Z ges Schiess - Sprengstoffw 29, 262 (1934) G. Fleury, L. Brissand and P. Lhoste, "Structure and Stability of Nitric Esters," Comp rend 224, 1016-18 (1947). W. R. Tomlinson, Jr., Fundamental Properties of High Explosives. Thermodynamic Relations for Use in the Estimation of Explosive Properties, PATR No. 1651, 22 April 1947.

- (h) Sarran and Vielle, Mém poudr 2, 161 (1884-1889).
- (i) E. von Hurtz, U. S. Patent 1,878,652 (20 September 1932).
- (j) L. A. Burrows, U. S. Patent 2,427,899 (23 September 1947).

(k) B. T. Fedoroff, <u>Handbook of Explosives and Related Items</u>, Picatinny Arsenal (unpublished).

(1) O. E. Sheffield, Literature Survey on Mannitol Hexanitrate, PA Chemical Research Laboratory Report No. 52-TMI-16, 23 January 1952.

(m) Also see the following Picatinny Arsenal Technical Reports on Mannitol Hexanitrate:

| 2 | 4 | ح | <u>6</u> |
|------|----------|----|----------|
| 1352 | 24 64 | 85 | 6 |

| Composition: % | Molecular Weight: $(HgC_2N_2O_2)$ 285 |
|--|--|
| $\begin{array}{ccc} & 8.4 & & 0 - \mathbf{N} = \mathbf{C} \\ \mathbf{N} & 9.8 & & \mathbf{Hg} \end{array}$ | Oxygen Balance: -17 CO, % -5.5 |
| 0 	 11.2 	 0 - N = C | Density: gm/cc Crystal 4.43 |
| нд 70.6 | Melting Point: "C Decomposes |
| C/H Ratio | Freezing Point: "C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 5; (1 kg wt) 35 | Boiling Point: "C |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 2; (11b wt) 4 Sample Wt, mg 30 | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ |
| Friction Pendulum Test: Steel Shoe Explodes Fiber Shoe Exp 1 odes | Vacuum Stability Test: cc/40 Hrs, at 90 °C |
| Rifle Bullet Impact Test: Trials % Explosions PartioIs | - 100°C Explodes 120°C 135°C 150°C |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand gm Black powder fuse 21.4 |
| Explosion Temperature : "C Seconds, 0.1 (no cap used) 263 1 239 5 Explodes 10 199 15 194 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl Ballistic Mortar, % TNT: |
| 20 190 | |
| 75°C International Heat Test: % Loss in 48 Hrs 0.18 | Trauzi Test, % TNT: (a) >1 Plate Dent Test: Method |
| 100°C Heat Test: Exploded in 16 hours % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT |
| Flammability Index: | Detonation Rate: Confinement |
| Hygroscopicity: % 30 ⁰ C, 90% RH 0.02 | Condition Pressed Charge Diameter, in. |
| Volatility: | Density, gm/cc 2.0 3.0 4.0 Rate, meters/second 3500 4250 5000 |

| Fragmentation Test: | Shaped Charge Effectiveness, TNT $=$ 100: |
|--|---|
| 90 mm HE, M71 Projectile, Lot WC-91: | Glass Cones Steel Cones |
| Density, gm/cc | Hole Volume |
| Charge Wt, Ib | Hole Depth |
| Total No. of Fragments: | Colore William Annual |
| For TNT | Color: White to gray |
| For Subject HE | Principal Uses: Detonators and ingredient of |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | priming compositions |
| Density, gm/cc | |
| Charge Wt, Ib | |
| Total No. of Fragments: | Method of Loading: psi x 10 ³ |
| For TNT | <u>3</u> 5 10 12 15 20 |
| For Subject HE | 3.00 3.20 3.60 3.70 3.82 4.00 |
| | Loading Density: gm/cc |
| Fragment Velocity: ft/sec | |
| At 9 ft At 25½ ft | Storage: |
| Density, gm/cc | |
| | Method Wet |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 |
| Air: | Compatibility Group Group M (wet) |
| Peak Pressure | |
| Impulse | Exudation None |
| Energy | |
| Air, Confined: | Stab Sensitivity: |
| Impulse | Density Firing Point (inch-ounces) gm/cc 0 <u>5</u> 505 1005 |
| Under Water: | 3.91 3.2 4.3 5.5 |
| Peak Pressure | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| Impulse | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ |
| Energy | Activation Energy: |
| | kcal/mol 29.81 |
| Underground: Peak Pressure | Induction Period, sec 0.5-10 |
| Impulse | Heat of: |
| Energy | Combustion, cal/gm 938 Explosion, cal/gm 427 |
| | Gas Volume, cc/gm 243 Formation, cal/gm -226 |
| | Specific Heat: $cal/gm/^{\circ}C$ 1.1 |
| | Thermal Conductivity: |
| | 1100000000000000000000000000000000000 |
| | |

Mercury Fulminate

Initiating Efficiency; Grams Required to Give Complete Initiation of:

| | Fulminate, gm |
|--------|---------------|
| INT | 0.25 |
| Tetryl | 0.20 |
| RDX | 0.19 |
| PEIN | 0.17 |

Compatibility with Metals:

<u>Dry:</u> Reacts rapidly with aluminum and magnesium. Reacts slowly with copper, zinc, brass and bronze. Iron and steel are not affected.

Wet: Reacts immediately with aluminum and magnesium. Reacts rapidly with copper, zinc, brass and bronze. Iron and steel are not affected.

| Sensitivity to | Static Discharge, | Joules: (b |) 0.025 |
|----------------|-------------------|------------|---------|
|----------------|-------------------|------------|---------|

| The | Effect | of | Storage | at | 50 ⁰ C | (Dry) | on | the | Purity | of' | Mercury | Fulminate |
|-----|--------|----|---------|----|-------------------|-------|----|-----|--------|-----|---------|-----------|

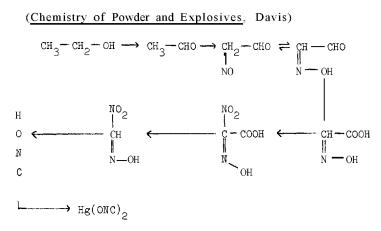
| Months Storage | <u>.979</u> | Recrystall <u>980</u> | ized Lots <u>981</u> | <u>982</u> | Uncrystall 505.6-7/31 | ized Lots 505.3-5/11 |
|----------------------|-------------------------|--------------------------|-------------------------|-------------------------|--------------------------|-------------------------|
| 0 | 99•75 | 99•77 | 99•79 | 99.79 | 98.86 | 98.7 |
| 4 | 99 • 3 8 | 99.45 | 99•54 | 99•47 | 95+95 | 98.7 |
| 8 9 | | | | | 94.95 | 97.4 |
| 10 12 13 14 | 98.74 98.26 98.22 | 99.56 | 97.49 | 99.06 98.79 | 90.65 | 94.9 |
| 15 16 | 97.52 97.00 | 99•30 98•66 | 99.30 99.01 | 98.19 97.75 96.69 | 83.76 | |
| 17 18 23 26 | 95.70 94.81 | 98.58 98.58 | 98.46 | 95 . 99 | 79,99 74.52 63.80 | |

Chemistry:

Mercuric f'ulminate readily decomposes in the presence of aqueous solutions, chlorides, carbonate and many other materials. Due to the presence of small amounts of mercury, formed by exposure to light or elevated temperatures, it readily forms amalgams with copper, brass and bronze, thus components containing these metals must be protectively coated if used with fulminate.

| °C | de Pe |
|----|----------|
| 12 | 0.07 |
| 49 | 0.18 |

Preparation:



Five gn mercury is dissolved in 25 cc of nitric acid (sp gr 1.42) without agitation, and this solution poured into 50 cc of 90% ethyl alcohol, resulting in a vigorous reaction, attended by evolution of white fumes and subsequent appearance of fulminate crystals. Red fumes then appear as precipitation of the product accelerates, and then white fumes again are evolved as the reaction moderates. After about 20 minutes the reaction is over; water is added, and the crystals are repeatedly washed, by decantation, with water to remove all acidity. The product is purified, rendered white, by solution in strong ammonium hydroxide, followed by reprecipitation with 30% acetic acid.

Origin:

Mercury fulminate was first prepared by John K. von Lowenstern (1630-1703) and in 1800 its preparation and properties were first described in detail by Edward Howard in a paper presented to the Royal Society of London (Phil Trans, 204 (1800). It was 1867 before the compound was used as an initiating agent, when Alfred Nobel invented the blasting cap and used mercury fulminate to detonate nitroglycerin (British Patent 1345 (1867)).

Destruction by Chemical Decomposition:

Mercury fulminate is decomposed by adding it, while stirring, to at least 10 times its weight of 20% sodium thiosulfate. Some poisonous cyanogen gas may be evolved.

References: 43

(a) Ph. Naoum - Z ges Schiess-Sprengstoffw (Munich), pp. 181, 229, 267 (27 June 1932).

(b) F. W. Brown, D. H. Kusler, and F. C. Gibson, Sensitivity of Explosives to Initiation by <u>Electrostatic Discharges</u>, U. S. Dept of Int, Bureau of Mines, RI 3852, 1946.

⁴³See footnote 1, page 10.

| -/ | 11150 | see the | 10110 1115 | ricatinny | 7 ti Senta | i i com | litear rept | 5115 01 | ricicary | 1 armina o |
|----|---|---------------------------|--|---|---|--|---|---|---------------------------------------|---|
| | <u>o</u> | <u>1</u> | 2 | <u>3</u> | <u>1</u> | 5 | <u>6</u> | <u>7</u> | 8 | <u>9</u> |
| | 250 480 510 550 610 680 760 1220 1450 | 301 381 561 1651 | 132 452 522 782 882 932 1192 1352 1372 1722 2032 | 23 203 433 833 1183 1393 2093 | 144 294 534 624 694 784 874 1104 | 65 105 255 285 365 415 425 1325 1365 | 266 366 556 866 986 1316 1486 1556 2146 | 277 297 407 537 567 637 857 1737 | 28 78 278 318 788 1838 | 199 609 749 849 999 1079 1389 2179 |

(c) Also see the following Picatinny Arsenal Technical Reports on Mercury Fulminate:

AMCP 706-177 Metriol Trinitrate (MTN) Liquid (or Trimethylolethane Trinitrate)

| Composition: % | Molecular Weight: (C ₅ H _a N ₃ 0 _a) 255 | | | | |
|---|---|--|--|--|--|
| $\begin{array}{cccc} & 23.5 & o_2 \text{NO} - \text{CH}_2 \\ \text{H} & 3.5 & o_2 \text{NO} - \text{CH}_2 \\ \text{N} & 16.6 \\ \text{O} & 56.4 \end{array} \qquad \begin{array}{c} c - c \text{H}_3 \\ c_2 \text{NO} - c \text{H}_2 \end{array}$ | Oxygen Balance: - 35 CO, % - 3 | | | | |
| $0.0 - CH_2 - C - CH_3$ N 16.6 | Density: gm/cc Liquid 1.47 | | | | |
| $o_{2}^{NO-CH_{2}}$ | Melting Point: "C – 3 | | | | |
| C/H Ratio 0.150 | Freezing Point: °C | | | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 47; (11b wt) 4 Sample Wt 20 mg | Boiling Point: °C | | | | |
| Picatinny Arsenal Apparatus, in. Sample Wt, mg 20 | Refractive Index, n ^D ₂₀ n ^D ₂₃ 1.4752 n ^O ₃₀ | | | | |
| Friction Pendulum Test: Steel Shoe Explodes Fiber Shoe Rifle Bullet Impact Test: Trials % Explosions | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C cc/gm 1.9 120°C 135°C | | | | |
| Partio Is Burned Unaffected | 150°C 200 Gram Bomb Sand Test: Sand, gm 43.7 | | | | |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) 1 5 Ignites 235 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl | | | | |
| 15 20 | Ballistic Mortar, % TNT: (a) 136 | | | | |
| | Trauzi Test, % TNT: (b) 140 | | | | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method | | | | |
| 100°C Heat Test: % Loss, 1st 48 Hrs 2.5 % Loss, 2nd 48 Hrs 1.8 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT | | | | |
| Flammability Index: | Detonation Rate: Confinement | | | | |
| Hygroscopicity: % 30 ⁰ C, 90% RH 0.07 | Condition Charge Diameter, in. Density, gm/cc Rate, meters/second | | | | |
| Volatility: 60°C, mg/cm ² /hr 24 | | | | | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | | | | |
|--|--|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | | | | |
| Total No. of Fragments: For TNT | Color: Oily, slightly turbid | | | | |
| For Subject HE 3 inch HE , M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Ingredient of rocket and double base propellants | | | | |
| Total No. of Fragments: For TNT | Method of Loading: | | | | |
| For Subject HE | Loading Density: gm/cc | | | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | | | | |
| Density, gm/cc | Method Liquid | | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | | | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | | | | |
| Air, Confined: Impulse | Solubility in Water, gm/100 gm, at: | | | | |
| Under Water: Peak Pressure | 25°C < 0.015 60°C < 0.015 | | | | |
| Impulse | Heat of: | | | | |
| Energy | Combustion, cal/gm 2642 | | | | |
| Underground: Peak Pressure | Hvdrolvsis, % Acid: | | | | |
| Impulse Energy | 10 days at 22°C 0.018 5 days at 60°C 0.115 | | | | |
| | | | | | |
| | | | | | |
| | | | | | |

Preparation:

Metriol (trimethylolmethylmethane) is obtained by the following procedure, based on work by Hosaeus (Annalen 276, 76 (1893):

Into a 5 liter round bottom flask is weighed 2700 gms of water. To this are added 267 gms of 36% formaldehyde and 60 gms of propionaldehyde. The mixture is stirred for a few seconds. To the mixture is added 150 gms of calcium oxide previously slaked with 600 gms of water. The mixture is heated in boiling water for four hours, and then allowed to cool spontaneously overnight. After filtering off the insoluble calcium hydroxide, the solution is heated and treated with a saturated aqueous solution of oxalic acid to precipitate all the calcium. The precipitated calcium oxalate is filtered off, and the pale-yellow filtrate concentrated as much as possible on the steam bath to a thick lemon-yellow syrup. After dissolving in absolute alcohol, the solution is filtered and concentrated in the steam bath to about twice the volume of the concentrated syrup. The solution is then chilled in a cold box to hasten crystallization. After allowing it to warm up to just above 0°C, the mixture is filtered. The resulting product is not sufficiently pure and is recrystallized from absolute alcohol. The melting point of the product (40.3 gm) is then about $196^{\circ}C$ (Hosaeus gives $199^{\circ}C$).

Metriol is nitrated by carefully mixing it with 3.5 parts of $65/3.5 \text{ HNO}_3/\text{H}_2SO_4$ maintained at 20°C, stirring for 30 minutes, cooling to 5°C, and pouring the reaction mixture on ice. It is extracted with ether, water-washed, and adjusted to pH 7 by shaking with a sodium bicarbonate solution and again water-washed three times. It is then dried with calcium chloride, filtered, and freed of ether by bubbling with dry air until minimal rate of loss in weight is attained. The yield is 88% of the theoretical. The product has a nitrate-nitrogen content of 16.35% (calculated: 16.47%). Its refractive index at 25°C is 1.4752.

Origin:

MTN, according to Italian sources, was first prepared and patented by Bombrini-Parodi-Delfino Company of Italy under the name "metriolo." A German Patent of 1927 also describes the preparation and gives some properties. This compound was known in France before World War II under the name of "Nitropentaglycerin" and Burlot and Thomas determined its heat of combustion (Ref b).

References: 44

(a) A. H. Blatt, <u>Compilation of Data on Organic Explosives</u>, OSRD Report No. 2014, 29 February 1944.

(b) E. Burlot and M. Thomas, Mem poudr 29, 262 (1939).

(c) Also see the following Picatinny Arsenal Technical Reports on Metriol Trinitrate: 1616 and 1817.

⁴⁴See footnote 1, page 10.

<u>Minol-2</u>

| Composition : % | Molecular Weight: | 71 |
|--|--|-----------------------------|
| Ammonium Nitrate 40 | Oxygen Balance: O, % CO % | - 3 ⁸ - 20 |
| | Density: gm/cc | 1.62-1.68 |
| Aluminum 20 | Melting Point: "C | |
| C/H Ratio | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: | Boiling Point: "C | |
| Bureau of Mines Apparatus, cm 35 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 13 Sample Wt, mg 17 | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability lest: cc/40 Hrs, at 90°C | |
| Rifle Bullet Impact lest: Trials % Explosions Partials | 100°C 120°C 135°C 150°C | 2.1 |
| Burned Unaffected | 200 Gram Bomb Sand lest: Sand, gm | 21 · 27 · |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Ignites 435 10 15 | Sensitivity to Initiation: Minimum Detonating Charg Mercury Fulminate Lead Azide Tetryl | ie, gm |
| 20 | Ballistic Mortar, % TNT: (a | a) 143 |
| | | b) 165 |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent lest: (c Method | c) B |
| 100°C Heat lest: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | Pressed No 1.73 66 |
| Flammability Index: 100 | Detonation Rate: (c Confinement | None |
| Hygroscopicity: % | Condition Charge Diameter, in. | Cas t 1.6 |
| Volatility: | Density, gm/cc Rate, meters/second | 1.68 58 20 |

<u>Minol-2</u>

| Booster Sensitivity Test: Condition | (e) Pressed | Decomposition Equation: |
|--|--|---|
| | | Oxygen, atams/sec (Z/sec) |
| Tetryl, gm | 100 | Heat, kilocalorie/mole |
| Wax, in. for 50% Detonation | 1.46 | (ΔH, kcal/mal) |
| Wax, gm | | Temperature Range, °C |
| Density, gm/cc | 1.74 | Phase |
| Heat of: | (f) | Armor Plate Impact Test: (f) |
| Combustion, cal/gm | 3160 | |
| Explosion, cal/gm | 1620 | 60 mm Mortar Projectile: |
| Gas Volume, cc/gm | | 50% Inert, Velocity, ft/sec 828 |
| Formation, cal/gm | | Aluminum Fineness |
| Fusion, cal/gm | | |
| | | 500-lb General Purpose Bombs: |
| Specific Heat: col/gm/°C | | |
| At -5°C | 0.30 | Plate Thickness, inches |
| Density, gm/cc | 1.74 | 1 |
| | | 11/4 |
| | | 11/2 |
| | | - 134 |
| Burning Rate: | | • /4 |
| cm/sec | | |
| | | Bomb Drop Test: |
| Thermal Conductivity: col/sec/cm/°C | (b) 16.5 x 10 ⁻⁴ 1.74 | T7, 2000-Ib Semi-Armor-Piercing Bomb vs Concrete: |
| Density, gm/cc | 1./4 | Max Safe Drop, ft |
| Coefficient of Expansion: Linear, %/°C | | |
| | | 500-lb General Purpose Bomb vs Concrete: |
| Volume, %/°C | | Height, ft |
| Hardness, Mohs' Scale: | | Trials |
| Hardness, Mons Scale. | | Unaffected |
| Young's Modulus: | (b) | Low Order |
| E', dynes/cm ² | 5.03 x 10 ¹⁰ | High Order |
| E, Ib/inch ² | 0.73×10^{6} | |
| Density, gm/cc | 1.66 | 1000-lb General Purpose Bomb vs Concrete: |
| | | Height, ft |
| Compressive Strength: Ib/inch ² (b) | 1910-2070 | Trials |
| Density, gm/cc | 1.68 | Unaffected |
| Vapor Pressure: | | |
| "C mm Mercury | | |
| - ···································· | | High Order |
| | | |
| | | |
| | | |

| Fragmentation Test: | | Shaped Charge Effectiveness, $TNT = 100$: | | |
|---|-----------|--|---------------------------------|--|
| 90 mm HE, M71 Projectile, L Density, gm∕cc Charge Wt, Ib | | | l Cones | |
| Total No. of Fragments: For TNT | | Color: | Gray | |
| For Subject HE | | Principal Uses: Bombs and depth | charges | |
| 3 inch HE, M42A1 Projectile, Density, gm/cc Charge Wt, Ib | Lot KC-5: | | | |
| Total No. of Fragments: For TNT | | Method of Loading: | Cast | |
| For Subject HE | | Loading Density: gm/cc 1 | .62-1.68 | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | | Storage: | | |
| Density, gm/cc | | Method | Dry | |
| Blast (Relative to TNT); | | Hazard Class (Quantity-Distance) | Class 9 | |
| Air: | | Compatibility Group | Group I | |
| Peak Pressure | 115 | | | |
| Impulse | 116 | Exudation | | |
| Energy | 133 | | | |
| Air, Confined: Impulse | 90 | Preparation: Minol is a castable mixture | consisting of | |
| Under Water: Peak Pressure | 108 | 40 percent TNT, 40 percent an and 20 percent powdered alumin fore can be prepared by addin | num and there- | |
| Impulse | 126 | gredients to molten TNT at 90 | ^O C under agita- | |
| Energy | 140 | tion. Minol also can be prep 25 parts of aluminum to 100 p amatol previously prepared. | ared by adding arts of 50/50 | |
| Underground : Peak Pressure | 134 | amator previously prepared. | | |
| Impulse | 139 | | | |
| Energy | 147 | | | |
| | | | | |

Minol-2

Origin:

Minols are British ternary explosives developed during World War 11. There are three formalations:

| Composition. %: | Minol-1 | Minol-2 | Minol-3 |
|------------------|---------|---------|---------|
| TWL | 48 | 40 | 42 |
| Ammonium Nitrate | 42 | 40 | 38 |
| Aluminum | 10 | 20 | 20 |

References: 45

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>. Part III - Miscellaneous <u>Sensitivity Tests</u>; <u>Performance Tests</u>, OSRD Report No. 5746, 27 December 1945.

(b) Philip C. Keenan and Dorothy Pipes, <u>Table of Military High Explosives</u>, Second Revision, NAVORD Report No. 87-46, 26 July 1946.

(c) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(a) G. H. Messerly, <u>The Rate of Detonation of Various Explosive Compounds</u>, OSRD Report No. 1219, 22 February 1943.

M. D. Hurwitz, The Rate of Detonation of Various Compounds and Mixtures, OSRD Report No. 5611, 15 January 1946.

(e) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute for</u> Tetryl in Boosters, NL Mamo 10,303, 15 June 1949.

(f' Committee of Div 2 and 8, NDRC, <u>Report on HBX and Tritonal</u>, OSRD No. 5406, 31 July 1945.

(g) W. R. Tomlinson, Jr., <u>Blast Effects of Bomb Explosives</u>, PA Technical Div Lecture, 9 April 1948.

(h) Also see the following Picatinny Arsenal Technical Reports on Minol-2: 1585 and 1635.

 $^{\rm 45}See$ footnote 1, page IO.

| Composition: | | Molecular Weight: | 40.6 |
|--|------------------------------|--|--------------|
| % Oxidizing agent (Ammonium Perchlorate) Aluminum, atomized Cupric Oxide | 35.0 26.2 | Oxygen Balance: CO, % CO % | -44 -37 |
| Magnesium, atomized Other ingredient (Tetryl) | 26.2 9.7 | Density: gm/cc Pressed | 2.0 |
| Other ingredient (Tetryl) Calcium Stearate | 1.9 1.0 | Melting Point: "C | |
| Graphite, artificial C/H Ratio | 1.0 | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 13 22 | Boiling Point: °C Refractive Index, n ^D ₂₀ n ^D ₂₃ n ^D ₃₀ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| Steel Shoe | Detonates | cc/40 Hrs, at | |
| Fiber Shoe | Unaffected | 90°C | |
| Rifle Bullet Impact Test: Trials % Explosions | | 100°C 120°C 135°C 150°C | 0.47 |
| Partials | | | |
| Burned Unaffected | | 200 Gram Bomb Sand Test: Sand, gm | 10.6 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 285 10 15 20 | | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl Ballistic Mortar, % TNT: | 0.20 0.25 |
| 20 | | TrauzI Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs Discoloration, fumes, odor 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | None 0.10 0.01 None | Plate Dent Test: Method Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | | Detonation Rate: Confinement | |
| Hygroscopicity: % | | Condition Charge Diameter, in. Density, gm/cc | |
| Volatility: | | Density, gm/cc Rate, meters/second | |

_

<u>MOX-1</u>

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 10$ | 00: | | |
|---|---|---|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth Color: Gray powder mixture Principal Uses: Small caliber antiaircraft projectiles | | | |
| Total No. of Fragments: For TNT | | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | | | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: | Pressed | | |
| Fragment Velocity: ft/sec | Loading Density: gm/cc A t 30,000 ps i | ~ 2.0 | | |
| At 9 ft At 25½ ft | Storage: | | | |
| Density, gm/cc | Method | Dry | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Bureau of Explosives Classifi Exudation | Group I cation Class A | | |
| | Heat of: | | | |
| Air, Confined: Impulse Under Water: | Combustion, cal/gm Explosion, cal/gm Gas volume, cc/gm | 4087 2087 212 | | |
| Peak Pressure Impulse Energy | Performance Tests: 20 mm T215E1 Projectile: | | | |
| Underground: Peak Pressure Impulse | NFOC Pressure Cube APG Blast Cube Activation Energy: | 35 40 | | |
| Energy | kcal/mol Temp, °C Time to ignition, seconds | 12.5 300 to 380 1.78 x 10 ⁻⁴ | | |
| | | | | |

MOX-2B

| Coyorition: | | Molecular Weight: | 42 |
|---|--------------------------|--|------------|
| Oxidizing agent (Ammonium Perchlorate) Aluminum, atomized Cupric Oxide | 35.0 52.4 | Oxygen Balance: CO, % CO % | -49 -43 |
| Magnesium, atomized | | Density: gm/cc Pressed | 2.0 |
| Other ingredients* Calcium Stearate Graphite, artificial | 9.7 1.9 1.0 | Melting Point: °C | |
| *5.8% RDX and 3.9% TNT coated pe | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | | Boiling Point: "C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. | 12 | Refractive Index, n ^D ₂₀ n ^D ₂₅ | |
| Sample Wt, mg | 24 | п ₂₅ П ₃₀ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| Steel Shoe | Unaffected Unaffected | cc/40 Hrs, at 90°C | |
| Fiber Shoe | Onarrected | | 0.21 |
| Rifle Bullet Impact Test: Trials | | 120°C | |
| % | | 135°C | |
| Explosions Partials | | 150°C | |
| Burned | | 200 Gram Bomb Sand Test: | |
| Unaffected | | Sand, gm | 11.5 |
| | | Sensitivity to Initiation: Minimum Detonating Charge, gm | |
| 1 | | Mercury Fulminate | |
| 5 375 | | Lead Azide | 0.20 |
| 10 | | Tetryl | 0.20 |
| 15 20 | | Ballistic Mortar, % TNT: | |
| | | TrauzI Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs Discoloration, fumes, odor | None | Plate Dent Test: Method | |
| 100°C Heat Test: | | Condition | |
| % Loss, 1st 48 Hrs | 0.27 | Confined | |
| % Loss, 2nd 48 Hrs | 0.12 | Density, gm/cc | |
| Explosion in 100 Hrs | None | Brisance, % TNT | |
| Flammability Index: | | Detonation Rate: Confinement Condition | |
| Hygroscopicity: % | | Charge Diameter, in. | |
| Volatility: | | Density, gm/cc Rate, meters/second | |

MOX-2B

| Fragmentation Test: | | | Shaped Charge Effectiveness, $TNT = 100$: | |
|--|--------------------|--------------------|---|----------------------------------|
| 90 mm HE, M71 Projectile, Density, gm/cc Charge Wt, Ib | Lot WC-91: | | Glass Cones Steel Cones Hole Volume Hole Depth | |
| Total No. of Fragments: For TNT | | Color: | Gray | |
| For Subject HE | | | Principal Uses: HE filler for small ca | liber |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | | projectiles | | |
| Total No. of Fragment s: For TNT For Subject HE | | | Method of Loading: | Pressed |
| | | | Loading Density: gm/cc | 2.0 |
| Fragment Velocity: ft/sec At 9 ft | | | | |
| At 25½ ft | | | Storage: | |
| Density, gm/cc | | | Method | Dry |
| Blast (Relative to TNT): | | | Hazard Class (Quantity-Distance) | Class 9 |
| Air: Bare Charge: Peak Pressure | <u>EW*</u> 1.02 | $\frac{EV*}{1.34}$ | Compatibility Group Bureau of Explosives Class A | Group I |
| Impulse | 1.08 | 1.41 | Exudation | None |
| Energy Density, gm/cc Air, Confined: Impulse | | 1.96 | Heat of: | 4494 |
| Cased Charge in Air:** | | | Combustion, cal/gm Explosion, cal/gm Gas volume, cc/gm | 4484 1472 221 |
| Peak Pressure | 1.09 | 1.44 | Performance Tests: | 221 |
| Impulse Energy | 1.16 | 1.53 | 20 mm T215El Projectile: | |
| Density, gm/cc | | 1.98 | NFOC Pressure Cube | 29 |
| Underground: Peak Pressure | | | APG Blast Cube | 30 |
| Impulse | | | Aviation Energy: | |
| Energy *EW, equivalent weight a EV, equivalent volume a | | | kcal/mol Temp, °C 340 to Time to ignition, seconds 1.39 | 7.6 470 x 10 ⁻² |
| **Strong paper-base pheno | lic case. | | | |

MOX-2B

Effect of Altitude, Charge Diameter and Degree of Confinement on Detonation Velocity* (Reference g)

| _ | | | | | |
|---|--------|---------------|------------------|---------|--------------|
| | Ground | - All and and | | 4730 | |
| 1 | 30,000 | | Charge would not | 4530(3) | Charge would |
| | | | | | |

*Confined charge in 1/4" steel tube, AISI 1015 seamless, 1" diameter 18" long, and 2" diameter 7" long. All means were determined from sets of five values unless otherwise indicated by (). A 26 gm tetryl booster was used to initiate each charge.

Average Fragment Velocity at Various Altitudes* (g)

| | Explosive | Charge Diameter, Inches | Ground m/s | 30,000 m/s | <i>60,000</i> m/s | 3 | 90,000 m/s | IT |
|---|--------------|----------------------------|---------------|---------------|----------------------|---|----------------------|----|
| ſ | MOX-2B, | ' 1 | 2012 | ** | ** | ٠ | ** | - |
| | density, 207 | 2 | 3314 | 3351 | 3247 | | ** | I |

*Outside diameter 2.54"; inside diameter 2.04"; length 7".

**Charge would not propagate detonation.

MOX-3B

| Composition: | Molecular Weight: | 45.6 |
|---|--|------|
| O%idizing agent (Potassium Nitrate) 18 | Oxygen Balance: | |
| Aluminum, atomized 50 Cupric Oxide | CO, % | -52 |
| Magnesium, atomized | CO % | -43 |
| Other ingredients*32Calcium Stearate**2.0 | Density: gm/cc Pressed | 2.0 |
| Graphite, artificial** 1.0 *29.1% RDX, 0.9% wax, and 2.0% TNT. | Melting Point: "C | |
| **Per cent added. | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | Boiling Point: "C | |
| Sample Wt 20 mg | Refractive Index, n ^D ₂₀ | |
| Picatinny Arsenal Apparatus, in. 17 Sample Wt. mg 24 | n ^D ₂₅ | |
| Sample Wt, mg 24 | n ₂₀ | |
| Friction Pendulum Test: | Vacuum Stability Test: | |
| Steel Shoe Unaffected | cc/40 Hrs, at | |
| Fiber Shoe Unaffected | 90°C | |
| Rifle Bullet Impact Test: Trials | 100°C | 0.57 |
| % | 120°C | |
| Explosions | 135°C | |
| Partials | 150°C | |
| Burned | 200 Gram Bomb Sand Test: | |
| Unaffected | Sand, gm | 33.2 |
| Explosion Temperature: °C | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) | Minimum Detonating Charge, gm | |
| 1 5 5 510 | Mercury Fulminate | |
| 5 540 10 | Lead Azide | 0.20 |
| 15 | Tetryl | 0.15 |
| 20 | Ballistic Mortar, % TNT: | - |
| | Trauzi Test, % TNT: | |
| 75°C International Heat Test: | Plate Dent Test: | |
| Discoloration, fumes, odor None | Method | |
| 100°C Heat Test: | Condition | |
| % Loss, 1st 48 Hrs 0.35 | Confined | |
| % Loss, 2nd 48 Hrs 0.13 | Density, gm/cc | |
| Explosion in 100 Hrs None | Brisance, % TNT | |
| | Detonation Rate: | |
| Flammability Index: | Confinement | |
| | Condition | |
| Hygroscopicity: % | Charge Diameter, in. | |
| I | J | |
| Volatility: | Density, gm/cc | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT=$ 100: | | |
|--|---|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel C Hole Volume Hole Depth | Cones | |
| Total No. of Fragments: For TNT | Color: Gray powder | mixture | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principol Uses: Small caliber ant projectiles | iaircraft | |
| Total No. of Fragments: For TNT | Method of Loading: | Pressed | |
| For Subject HE Fragment Velocity: ft/sec | Loading Density: gm/cc A t 30,000 psi | ~ 2.0 | |
| At 9 ft At 25½ ft Density, gm/cc | Storage: | | |
| | Method | Dry | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Bureau of Explosi | Group I ves Class A | |
| Air, Confined: Impulse | <u>Heat of:</u> Combustion, cal/gm Explosion, cal/gm | 4331 980 | |
| Under Water: Peak Pressure Impulse Energy | Gas volume, cc/gm Performance Tests: 20 mm T215El Projectile: | 232 | |
| Underground: Peak Pressure | NFOC Pressure Cube APG Blast Cube | 37 52 | |
| Impulse Energy | Temp, ^{OC} due Time to ignition, niti | es not included to erratic ig- on under condi- s of test. | |
| | | | |

MOX-4B

| Composition: | Molecular Weight: | 48 |
|--|---|------------|
| %Oxidizing agent (Barium Nitrate)18Aluminum, atomized50Cupric OxideMagnesium, atomized | Oxygen Balance: CO, % CO % | -53 -43 |
| Other ingredients*32Calcium Stearate**2.0 | Density: gm/cc Pressed | 2.0 |
| Graphite, artificial** 1.0 | Melting Point: °C | |
| *29.1% RDX, 0.9% wax, and 2.0% TNT. **Per cent added. | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 78 | Boiling Point: "C | |
| Sample Wt 20 mg | Refractive Index, n ^D ₂₀ | |
| Picatinny Arsenal Apparatus, in. 18 Sample Wt, mg 26 | n ₂₅ | |
| | n ₃₀ | |
| Friction Pendulum Test: Steel Shoe Sparks Fiber Shoe Unaffected | Vacuum Stability Test: cc/40 Hrs, at 90°C | |
| | 100°C | 0.67 |
| Rifle Bullet Impact Test: Trials | 120°C | 0.07 |
| % Explosions | 135°C | |
| Partials | 150°C | |
| Burned | | |
| Unaffected | 200 Gram Bomb Sand Test: Sand, gm | 22.6 |
| Endering Transactions IIO | | 33.6 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) | Sensitivity to Initiation: Minimum Detonating Charge, gm | |
| 1 | Mercury Fulminate | |
| 5 610 | Lead Azide | 0.20 |
| 10 | Tetryl | 0.15 |
| 15 | | |
| 20 | Ballistic Mortar, % TNT: | |
| 75°C International Heat Test: | Trauzl Test, % TNT: | |
| % Loss in 48 Hrs | Plate Dent Test: | |
| Discoloration, fumes, odor None | Method | |
| 100°C Heat Test: | Condition | |
| % Loss, 1st 48 Hrs 0.22 | Confined | |
| % Loss, 2nd 48 Hrs 0.12 | Density, gm/cc Brisance, % TNT | |
| Explosion in 100 Hrs None | | |
| Flammability Index: | Detonation Rate: Confinement | |
| Hygroscopicity: % | Condition Charge Diameter, in. | |
| Volatility: | Density, gm/cc Rate, meters/second | |

| Fragmentation Test: | Shaped Charge Effectiveness, TNT = 100: |
|---|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, lb | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: Gray powder mixture |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Small caliber antiaircraft projectiles |
| Total No. of Fragments: For TNT | Method of Loading: Pressed |
| For Subject HE' | Loading Density: gm/cc A t 30,000 psi |
| At 9 ft At 25½ ft | Storage: |
| Density, gm/cc | Method Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 |
| Air: Peak Pressure Impulse Energy | Compatibility Group I Bureau of Explosives Class A |
| Air, Confined: Impulse Under Water: Peak Pressure | Heat of:Combustion, cal/gm4392Explosion, cal/gm709Gas volume, cc/gm208 |
| Impulse Energy | Performance Tests: 20 mm T215El Projectile: |
| Underground: Peak Pressure Impulse Energy | NFOC Pressure Cube43APG Blast Cube53Aviation Energy:100kcal/molValues not includedTemp, °Cdue to erratic igni-Time to ignition, secondstion under conditions of test. |
| | |

<u>MOX-6</u>B

| Composition: | | Molecular W eigh t: | 43 |
|--|--|--|--------------|
| % Oxidizing agent Aluminum, atomized Cupric Oxide Magnesium, atomized Other ingredients* Calcium Stearate Graphite, artificial *28.7% RDX coated, 0.9% wax. C/H Ratio | 49.2 19.7 29.6 1.5 | Øxygen Balance: CO % Density: gm/cc Melting Point: "C Freezing Point: "C | -50 -42 |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | | Boiling Point: °C Refractive Index, n ^D 20 n ^D 25 n ^D 30 | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe Rifle Bullet Impact Test: Trials % Explosions | Unaffected Unaffected | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C 120°C 135°C | 0.43 |
| Partials Burned Unaffected Explosion Temperature: "C | | 150°C 200 Gram Bomb Sand Test: Sand, gm Sensitivity to Initiation: | 10.8 |
| Seconds, 0.1 (no cap used) 1 5 510 10 15 20 | | Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl Ballistic Mortar, % TNT: | 0.20 0.16 |
| 75°C International Heat Test: % Loss in 48 Hrs Discoloration, fumes, odor 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | 0.02/10 gm 0.00 0.00 0.00 None | Trauzl Test, % TNT: Plate Dent Test: Method Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: Hygroscopicity: % 30°C, 90% RH, two weeks Volatility: | 0.79 | Detonation Rate: Confinement Condition Charge Diameter, in. Density, gm/cc Rate, meters/second | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: |
|--|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: Gray powder mixture |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Small caliber antiaircraft projectiles |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pressed |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Loading Density: gm/cc A t 30,000 psi -2.0 Storage: |
| Density, gm/cc | Method Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 |
| Air: Peak Pressure Impulse Energy | Compatibility Group Group I Bureau of Explosives Class A |
| Air, Confined: Impulse Under Water: | Heat of:Combustion, cal/gm4293Explosion, cal/gm750Contact750 |
| Peak Pressure Impulse | Gas volume, cc/gm 204 Activation Energy: |
| Energy Underground: Peak Pressure Impulse Energy | kca 1/mo 1 Temp, °C Values not included due to erratic igni- tion under conditions seconds of test. |
| | |

Preparation:

The various ingredients used in the preparation of MOX explosives are coated separately as follows:

Dichromated Atomized Aluminum - Seventy-five grams of chemically pure grade sodium dichromate is dissolved in 1500 milliliters of water at 100° C under mechanical agitation. Six hundred grams of the atomized aluminum powder is added gradually (2 to 3 minutes) and stirring is continued for half an hour. The dichromated metal is filtered, washed with water (15 to 20 times) until the washings show only a slight cloudiness with silver nitrate. The water-wet product is then dried in an oven at 50°C. The dried material is hand-rolled to reduce any conglomerates, and blended before use.

Wax-Coated RDX - Eighteen grams of molten Be Square Special Wax (manufacturer's 180° to 185 Fahrenheit grade amber) is added to 582 grams of finely divided RDX (water precipitated from acetone solution) in a water slurry under mechanical agitation. The temperature of the wax-RDX slurry is maintained above the melting point of the wax (about 90°C). The stirring is continued for half an hour. After cooling to 50°C, the wax-coated RDX is recovered by filtration in a Büchner funnel and dricd in air. The RDX thus coated and presumed to be 3% waxed RDX or a 97/3 RDX/wax mixture is hand-rolled to crush any conglomerates formed, and blended by hand before use.

<u>INT-Coated Barium Nitrate</u> - Thirty grams of TNT in alcohol solution is added to 270 grams of barium nitrate in an alcohol slurry under agitation. The temperature of the TNT-barium nitrate mixture is maintained at 80° C and stirring is continued until most of the alcohol is evaporated. The coated material is spread in a thin layer on a tray to dry in air overnight. The barium nitrate thus coated, with 10% TNT is reduced to an intimate mixture by hand-rolling ard blending before use.

<u>INT-Coated Potassium Nitrate</u> - The TNT-coated potassium nitrate is prepared by the same procedure as is used for coating barium nitrate.

<u>RDX/INT-Coated Ammonium Perchlorate</u> - The ammonium perchlorate is coated by dissolving the appropriate weights of RDX and TNT in hot alcohol. After adding the ammonium perchlorate, the slurry is stirred until most of the solvent is evaporated. The treated ammonium perchlorate is spread on a tray to dry overnight. Agglomerates formed during the process are crushed by hand-rolling and blending the mixture before use.

<u>HNT-Coated RDX</u> - Sixty grams of molten TNT are added to a water slurry of 540 grams of finely divided RDX (water precipitated from acetone solution) under mechanical agitation. The temperature of the TNT-RDX slurry is maintained at about 90°C and stirring is continued for half an hour. After cooling to about 50°C, the TNT-coated RDX is recovered by filtration. The RDX thus treated, and presumed to be 10% coated or a 90/10 RDX/TNT mixture, is further blended by hand after rolling to crush any aggregates formed during the process.

The MOX explosive mixtures are prepared by blending the appropriate weights of the dry ingredients in a Patterson-Kelly twin-shell blender for at least 30 minutes.

Origin:

MOX type explosive mixtures were developed beginning in 1950 by National Northern, technical. division of the National Fireworks Ordnance Corporation, West Hanover, Massachusetts. References: 46

(a) A. O. Mirarchi and A. T. Wilson, <u>Development of MOX Explosives for Improved 20 mm</u> <u>Amunition</u>, Navy Contract Nord-10975, Task 1, National-Fireworks Ordnance Corporation, First Yearly Summary, August 1950 to August 1951.

(b) A. T. Wilson, <u>Development of MOX Explosives: Various Oxidants in MOX</u>, First Progress Report NFOC-6, Navy Contract Nord-12382, National Fireworks Ordnance Corporation, December 1952.

(c) A. O. Mirarchi, <u>Properties of Explosives: Theory of the MOX Explosion</u>, First Progress Report NFOC-10, Navy Contract NOrd-11393, National Fireworks Ordnance Corporation, December 1952.

(d) A. O. Mirarchi, Properties of Explosives: MOX Explosives in Various Atmospheres, First Progress Report NFOC-9, Navy Contract NOrd-11393, National Fireworks Ordnance Corporation, 1952.

(e) A. T. Wilson, <u>Development of MOX Explosives</u>: <u>Composition Variations</u>, First Progress Report NFOC-7, Navy Contract NOrd-12382, National Fireworks Ordnance Corporation, 1952.

(f) A. T. Wilson, Development of MOX Explosives: Various Oxidants in MOX, Second Progress Report NFOC-14, Navy Contract Nord-13684, National Fireworks Ordnance Corporation, October 1953.

(g) A. W. O'Brien, Jr., C. W. Plummer, R. P. Woodburn and V. Philipchuk, Detonation Velocity Determinations and Fragment Velocity Determinations of 'Varied Explosive Systems and Conditions, National Northern Corporation Final Summary Report NNC-F-13, February 1958 (Contract DAI-19-020-501-ORD-(P)-58).

(h) P. Z. Kalanski, <u>Air Blast Evaluation of MOX-2B Cased and Bare Charges</u>, NAVORD Report No. 3755, 5 April 1956.

(i) Also see the following Picatinny Arsenal Technical Reports on MOX Explosives: 1935, 1969, 2204, 2205.

⁴⁶See footnote 1, page 10.

| Composition: / % H O | Molecular Weight: | (272,39) _n |
|---|---|-----------------------|
| $\begin{array}{c} c \\ H \\ H \\ N \\ 12.60 \end{array} \xrightarrow{26.46} H_{2} \xrightarrow{1}_{X} \xrightarrow{H}_{H} \xrightarrow{H}_{X} \xrightarrow{H}_{H} $ | Oxygen Balance: CO, % CO % | -35 0.6 |
| $\begin{array}{c} 0 \\ X=0NO_2 \end{array}$ | Density: gm/cc | |
| | Melting Point: "C | Decomposes |
| C/H Ratio 0.23 | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg W t: Bureau of Mines Apparatus, cm ⁸ | Boiling Point: °C | |
| Sample Wt 20 mg | Refractive Index, n ^D ₂₀ | |
| Picatinny Arsenal Apparatus, in. 3 Sample Wt, mg 5 | n ⁰ ₂₅ | |
| | n ^o ₃₀ | |
| Friction Pendulum Test: | Vacuum Stability Test: | |
| Steel Shoe Fiber Shoe | cc/40 Hrs, at 90°C | 0.17 |
| | 100°C | 1.0 |
| Rifle Bullet Impact Test: Trials | 120°C 16 hours | 11.+ |
| % Explosions | 135°C | |
| Partials | 150°C | |
| Burned | 200 Gram Bomb Sand Test: | |
| Unaffected | Sand, gm | 45.0 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Decomposes 170 | Sensitivity to Initiation: Minimum Detonating Charge, grr Mercury Fulminate Lead Azide | 0.10 |
| 10 | Tetryl | 0.10 |
| 15 | | |
| 20 | Ballistic Mortar, % TNT: | |
| 75"C International Heat Test: | Trauzl Test, % TNT: | |
| % Loss in 48 Hrs | Plate Dent Test: Method | |
| 100°C Heat Test: | Condition | |
| % Loss, 1st 48 Hrs | Confined | |
| % Loss, 2nd 48 Hrs | Density, gm/cc | |
| Explosion in 100 Hrs | Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement | |
| Hygroscopicity: % 30°C, 90% RH 3 | Condition Charge Diameter, in. | |
| Volatility: 60°C, mg/cm ² /hr 0.0 | Density, gm/cc Rate, meters/second | |

| Composition: / % H O | Molecular Weight: (286.34 |) _n |
|--|---|----------------|
| $\begin{array}{c c} & 25.29 \\ H & 2.52 \\ N & 13.45 \end{array} \begin{array}{c} H \\ H_{21} \\ H \\ H \\ H \end{array}$ | Oxygen Balance: -29 CO % 4.7 | |
| 0 58.74 0 X | Density: gm/cc | |
| | Melting Point: °C Decompose | es |
| C/H Ratio 0.23 | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 9 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 3 Sample Wt, mg 5 | Boiling Point: "C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 0'.42 90°C 0'.42 100°C 1.5 | |
| Rifle Bullet Impact Test: Trials % Explosions Partials | 120°C ll.+ 135°C 150°C | |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm 49.0 | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 230 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminote Lead Azide 0.10 Tetryl | |
| 15 20 | Ballistic Mortar, % TNT: 125 | |
| 75°C International Heat Test: % Loss in 48 Hrs | Trausl Test, % TNT: Plate Dent Test: Method | |
| 100°C Heat Test: 0.3 % Loss, 1st 48 Hrs 0.0 % Loss, 2nd 48 Hrs 0.0 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement | |
| Hygroscopicity: % 30°C, 90% RH ~2 | Condition Charge Diameter, in. | |
| Volatility: 60°C, mg/cm ² /hr 0.0 | Density, gm/cc1.20Rate, meters/second7300 | |

| Composition: | Molecular Weight: | (297.15) _n |
|---|--|-----------------------|
| $\begin{array}{c c} C & 24.25 \\ H & 2.37 \\ N & 14.14 \end{array} \xrightarrow{H_2C}_{H} H \\ X \\ X \\ H \end{array}$ | Oxygen Balance: CO, % CO % | -24 8 |
| 0 59.24 0 H X=ONO ₂ | Density: gm/cc | 1.65-1.70 |
| | Melting Point: "C | Decomposes |
| C/H Ratio 0.23 | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 8 | Boiling Point: "C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 3 Sample Wt, mg 5 | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C 14 hours | 1.46 11.+ |
| Rifle Bullet Impact Test: Trials % Explosions Partials | 120°C 16 hours 135°C 150°C | 11.+ |
| Burned Unaffected | 200 Grom Bomb Sand Test: Sand, gm | 52.3 |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) 1 5 | Sensitivity to Initiation: Minimum Detonating Charg Mercury Fulminate Lead Azide | e, gm 0.10 |
| 10 15 20 | Tetryl Ballistic Mortar, % TNT: | |
| 20 | Trauzl Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method | |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement | |
| Hygroscopicity: % 30°C, 90% RH ≁ 1 | Condition Charge Diameter, in. | |
| Volatility: 60° C, mg/cm ² /hr 0.0 | Density, gm/cc Rate, meters/second | |

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| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: |
|---|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: White |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Pyroxylin (12%N), blasting explosives; pyrocellulose (12.60% N), smokeless powder; guncotton (13.35% N minimum), propellants |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: |
| | Loading Density: gm/cc |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: |
| Density, gm/cc | Method Wet (8% to 30% water) |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 12 |
| Air: Peak Pressure Impulse | Compatibility Group Group M (wet) Exudation None |
| Energy Air, Confined: Impulse | Heat of: Combustion, cal/gm 2409* 2313** 2228*** Explosion, cal/gm 855* 965** 1058*** Gas Volume, cc/gm 919* 883** 853*** |
| Under Water: Peak Pressure Impulse Energy | Formation, cal/gm 617* 561** 513*** * 12.6% N ** 13.45% N |
| Underground: Peak Pressure | *** 14.14% N Vapor Pressure: |
| Impulse Energy | <u>^oC</u> <u>mm Mercury</u> |
| | 25 0.00 60 0.00 |

Nitrocellulose (NC)

| Solubility in Water, gm/100 gm, at: | 12.6% N | 13.45%n | 14.0% N |
|---|---|---------------------------------------|-------------------------------------|
| 25°C 60°C | Insoluble Insoluble | Insoluble Insoluble | Insoluble Insoluble |
| Solubility, gm/100 gm, 25 ⁰ C, in: | | | |
| Ether Alcohol | Insoluble Very slight- ly soluble | Insoluble Practically insoluble | Insoluble Insoluble |
| 2:1-Ether:Alcohol | Soluble | Slightly soluble (6%-11%) | Practically insoluble (1 + %) |
| Acetone | Soluble | Soluble | Soluble |
| 240-Hour Hydrolysis Test, <u>³/₂ Nitric Acid</u> | 1.22 | 1.03 | |

Preparation of Nitrocellulose from Cotton Linters:

(Laboratory Procedure)

<u>Nitration</u>: Second cut cotton linters, previously dried to a moisture content of less than 0.5%, are nitrated by immersion in mixed acid under the following conditions:

Ratio of Mixed Acid to cotton 55 to 1

Composition of Mixed Acid (approximate)

- a. for 12.6% N: H₂SO₄ 63.5%, HNO₃ 21%, H₂O 15.5%
- b. for 13.4% N: H2SO4 68%, HNO3 22%, H2O 10.0%

Temperature of acid at the start 34° C

Time of nitration 24 minutes

During the nitration period the mixture is turned over occasionally to keep the acid homogeneous. The mixture is then filtered on a Buchner funnel with suction for about three minutes and then drowned rapidly with strong hand stirring in at least 50 volumes of cold water. After the nitrocellulose has settled, most of the water is decanted and fresh water added. The nitrocellulose-water mixture is boiled and the acidity adjusted to 0.25% to 0.50% as H_2SO_4 . The sour boil is continued for at least 24 hours for pyrocellulose and at least 40 hours for gun-cotton. Additional boiling with changes of water are made in accordance with the governing specification (JAN-N-244).

<u>Pulping:</u> The nitrocellulose is then pulped in a laboratory Holland-type paper beater. Enough sodium carbonate is added to keep the reaction faintly alkaline to phenolphthalein. Pulping is continued to the desired degree of fineness.

<u>Poaching:</u> After washing the nitrocellulose from the beater, the mixture is filtered and the product boiled for 4 hours with fresh water while stirring mechanically. From time to time a little sodium carbonate solution is added to maintain the mixture faintly alkaline to phenolphthalein. The water is decanted and the boiling continued. According to the specification, the total boiling treatment with poaching is as follows:

- 4 hours boiling with or without sodium carbonate
- 2 hours boiling without sodium carbonate
- 1 hour boiling without sodium carbonate

1 hour boiling without sodium carbonate.

Each boil is followed by settling and change of water.

<u>Washing:</u> The nitrocellulose is then washed by mechanical agitation with water. A minimum of two washes are given. If a sample taken after the water washes gives a minimum test of 35 minutes in the 65.5° C Heat Test and 30 minutes in the $13^{4}.5^{\circ}$ C Heat Test, the nitrocellulose is satisfactorily stabilized. Otherwise additional washes should be given.

Orinin:

Cellulose occurs in nature. It is wood fiber, cell wall and the structural material of all plants. Cotton fiber is pure cellulose. Nitrocellulose was discovered about 1847 by C. F. Schonbein at Basel and R. Bottger at Frankfort-on-the-Main independently of each other when cotton was nitrated. T. J. Pelouze had nitrated paper earlier (1838) and was probably the first to prepare nitrocellulose.

Pyroxylin or collodion, which is soluble in a mixture of ether and ethanol, contains from 8% to 12% nitrogen. It is used in the manufacture of celluloid and in composite blasting explosives.

<u>Pyrocellulose</u>, a type of nitrocellulose of 12.6% nitrogen content, completely soluble in a mixture of 2 parts ether and one part ethanol, was developed by Mendeleev (1891-1895). This material, when colloided, formed the first smokeless powder for military use in the United States (1898).

<u>Guncotton</u> for military purposes today contains a minimum of 13.35% nitrogen. It is only slightly soluble in ether-ethanol, but completely soluble in acetone. Principal use is in flashless powders and as flame carriers. 14.14% N nitrocellulose represents a theoretical limit.

In the manufacture of propellants, there is used a mixture of pyrocellulose and guncotton (blended nitrocellulose) of 13.15% to 13.25% nitrogen content.

Destruction by Chemical Decomposition:

Nitrocellulose is decomposed by adding it, with st rring, to 5 times its weight of 10% sodium hydroxide heated to 70° C. Stirring is continued for 15 minutes after all the nitrocellulose has been added.

References: 47

(a) See the following Picatinny Arsenal Technical Reports on Nitrocellulose:

⁴⁷See footnote 1, page 10.

Nitrocellulose (NC)

| <u>o</u> | <u>1</u> | 2 | <u>3</u> | 4 | 5 | 6 | 2 | 8 | 9 |
|---|---|--|---|--|---|--|--|--|---|
| 10 390 420 660 730 960 1020 1150 1190 1210 1240 1300 1320 1350 1410 1430 1490 1580 1660 1810 1830 1990 2210 | $\begin{array}{c} 41\\ 101\\ 231\\ 351\\ 551\\ 831\\ 851\\ 971\\ 1031\\ 1041\\ 1071\\ 1151\\ 1201\\ 1221\\ 1331\\ 1351\\ 1391\\ 1421\\ 1501\\ 1421\\ 1501\\ 1541\\ 1681\\ 1691\\ 1731\\ 1811\\ 1831\\ 1851\\ 1931\\ 1961\\ 1991\\ 2071\\ 2101\\ 2101\\ 2201\end{array}$ | 72 332 402 422 542 572 652 662 752 802 952 1012 1032 1142 1242 1362 1392 1642 1852 1912 1992 2022 2102 | 13 33 43 133 233 253 273 653 673 683 773 963 1023 1273 1443 1653 1813 1863 1973 1973 | $\begin{array}{c} 4\\ 24\\ 114\\ 174\\ 194\\ 334\\ 394\\ 724\\ 804\\ 1024\\ 1054\\ 1074\\ 1274\\ 1304\\ 1374\\ 1394\\ 1394\\ 1394\\ 1394\\ 1394\\ 1394\\ 1394\\ 1394\\ 1394\\ 1394\\ 1394\\ 1394\\ 1394\\ 1394\\ 1394\\ 1394\\ 1394\\ 1454\\ 1814\\ 2144\end{array}$ | $\begin{array}{c} 125\\ 475\\ 485\\ 555\\ 965\\ 1025\\ 1265\\ 1265\\ 1265\\ 1275\\ 1375\\ 1915\\ 1915\\ 1955\\ \end{array}$ | 86 576 586 796 916 1026 1026 1206 1256 1276 1316 1516 1556 1616 1786 2056 | 167 327 407 717 787 987 1187 1297 1267 1297 1427 1447 1487 1587 1637 1717 1827 1827 1827 1827 1637 2107 2137 | 8 198 208 278 388 408 588 758 758 758 758 758 128 128 128 128 128 128 1248 1348 1348 1348 1528 1638 1638 1638 1898 1918 2098 2208 | 19 29 69 169 279 499 659 669 709 739 779 809 1399 1399 1399 1349 1399 1449 1619 1799 1869 2119 2189 |

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| $\%$ Oxygen Balance: CO $\%$ 3.5 CO $\%$ 3.5 CO $\%$ H2.2 $HC = ORO_2$ H2.2 $HC = ORO_2$ J18.5 $H_2C = ORO_2$ O63.4 1.592 C/H Ratio 0.109Pressing Point: "CImpact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, in: Sample Wt, 20 mg15Friction Pendulum Test: Steel ShoeExplodesFiber ShoeIstrict TrialsFride Builet Impact Test: TrialsTrialsVacuum Stability Test: Co $\%$ 1.6O'C co/gm/16 hrs1.6Unaffected0Burned0Unaffected0Burned0Seconds, 0.1 (no cap used)1Seconds, 0.1 (no cap used)11520Trauzi Test; $\%$ TNT: (a)100°C Heat Test: % Loss, 1st 48 Hrs3.6% Loss, 1st 48 Hrs3.6% Loss, 1st 48 Hrs3.5Explosion 100 HrsNoneFleer StoceCondition Confined100°C Heat Test: % Loss, 1st 48 Hrs3.6% Loss, 1st 48 Hrs3.5Explosion 100 HrsNoneFleer StoceCondition Confined100°C Heat Test: % Loss, 1st 48 Hrs3.5Explosion 100 HrsNoneFleer Millity Index:Detonation Rate: ConfinedConfined % Loss, 1st 48 Hrs3.5Explosion 100 HrsNoneFleer Millity Index:0.06Volatility: Index:0.06Condition </th <th>Composition :</th> <th>Molecular Weight: (CHNO) 227</th> | Composition : | Molecular Weight: (CHNO) 227 |
|--|---|---|
| 0 63.4 Melting Point: *C Stable form 15:2 C/H Ratio 0.109 Freezing Point: *C Impact Sensitivity, 2 kg Wt: Bureau of Mines Apparatus, cm 15 Sample W1 20 mg 1 Pricatinny Arsenal Apparatus, in. 1 lb vt Steel Shoe Explodes Fiber Shoe Explodes Riffe Bullet Impact Test: Trials Steel Shoe 100 Partials 0 Burned 0 Unaffected 0 Steplosion Temperature: *C Seconds, 0.1 (no cap used) 15 Story of the Hrs 16 20 Explodes 21 5 Explosion Temperature: *C Seconds, 0.1 (no cap used) Marting Wortar, % TNT: 15 20 75°C International Heat Test: % Loss, 1st 48 Hrs % Loss, 1st 48 Hrs 3-6 % Loss, 1st 48 Hrs 3-6 % Loss, 1st 48 Hrs 3-5 Explosion In 100 Hrs None Flate Dent Test: Confined % Loss, 1st 48 Hrs 3-5 <tr< td=""><td>с 15.9 _{Н2}С оло₂</td><td>CO₂% 3.5 CO% 24.5</td></tr<> | с 15.9 _{Н2} С оло ₂ | CO ₂ % 3.5 CO% 24.5 |
| 0 63.4 Maring Foint C_STABLE Torm 13.2 C/H Ratio 0.109 Freezing Point: "C Bioling Point: "C Becommoses 14.5 Bureau Of Mines Apparatus, cm 15 Barlau Of Mines Apparatus, in, 1 lb vt 1 Refractive Index, ng 1.4732 Picatinny Arsenal Apparatus, in, 1 lb vt 1 ng 1.4732 ng Friction Pendulum Test Steel Shee Explodes 50°C cc/gm/6 hrs 1.6 Fiber Shoe %00 135°C 120°C 135°C Partials 0 100°C cc/gm/6 hrs 1.1 11 Rifle Builet Impact Test: Trials 120°C 135°C 120°C Burned 0 200 Gram Bomb Sand Test: 1.1 140 Seconds, 0.1 (no cap used) 1 5 Explodes 222 10 181 140 75°C International Heat Test: % 0.48 181 140 140 75°C International Heat Test: % 1.6 140 140 75°C International Heat Test: % 1.6 140 75°C International Heat Test: %.6 3.6< | N 18.5 $H_2 C - ONO_2$ | |
| Impact Sensitivity, 2 Kg Wt: 15 Bureau of Mines Apparatus, cm 15 Sample Wt 20 mg 10 vt Picatinny Arsenal Apparatus, in, 1 lb vt 1 Sample Wt, mg 1.45 Friction Pendulum Test: steel Shoe Explosions 100 Riffe Bullet Impact Test: Trials Partials 0 Burned 0 Uaffected 0 Banded Solution 150°C Seconds, 0.1 (no cap used) 10 1 5 Explosion Temperature: °C Seconds, 0.1 (no cap used) Mercury Fulminate 1 Lead Azide 1 3.6 20 Ballistic Mortar, % TNT: (a) 140°C 140 75°C International Heat Test: 3.6 % Loss, 1st 48 Hrs 3.6 % Loss, 1st 48 Hrs 3.6 % Loss, 2nd 48 Hrs 3.5 Explosion in 100 Hrs Nonc Plate Dent Test: Condition % Loss, 2nd 48 Hrs 3.5 % Loss, 2nd 48 Hrs 3.5 | 0 63.4 | Melting Point: °C Labile form 13.2 |
| Bureau of Mines Apparatus, cm 15 Sample WI 20 mg 10 vt 1 Picatinny Arsenal Apparatus, in. 1 lb vt 1 Sample WI, mg ng 1.4732 Pricatinny Arsenal Apparatus, in. 1 lb vt 1 Sample WI, mg ng 1.4713 Pricationy Arsenal Apparatus, in. 1 lb vt 1 Sample WI, mg 1 1 Friction Pendulum Test: Stell Shoe Explodes Fiber Shoe 00°C cc/gm/6 hrs 1.6 No°C cc/gm/16 hrs 1.6 100°C cc/gm/16 hrs 1.6 Do°C cc/gm/16 hrs 1.6 100°C cc/gm/16 hrs 1.6 Partials 0 Damed 0 Unaffected 0 Seconds, 0.1 (no cap used) Minimum Detonating Charge, gm Mercury Fulminate Lead Azide 12 1 20 Trauzi Test, % TNT: (b) 75°C International Heat Test: 3.6 % Loss, 1st 48 Hrs 3.6 % Loss, 2nd 48 Hrs | C/H Ratio 0.109 | Freezing Point: "C |
| Sample Wt 20 mg 1.4732 Picatinny Arsenal Apparatus, in, 1 1b vt, 1 1 Sample Wt, mg n2 Friction Pendulum Test: steel Shoe Steel Shoe Explodes Fiber Shoe 90°C cc/gm/16 brs Rifle Builet Impact Test: Trials 90°C cc/gm/16 brs 1.4713 Rifle Builet Impact Test: Trials 90°C cc/gm/16 brs 1.4713 100°C cc/gm/16 brs 1.4713 110°C 100°C | | Boiling Point: "C Decomposes 145 |
| Sample Wt, mg It is 1.441.3 Friction Pendulum Test: Na Steel Shee Explodes Fiber Shee Explodes Fiber Shee 1.6 Rifle Bullet Impact Test: Trials Rifle Bullet Impact Test: Trials 0 100°C Partials 0 Burned 0 Unaffected 0 Seconds, 0.1 (no cap used) Minimum Detonating Charge, gm 1 5 5 Explodes 20 Explosion Temperature: * °C 5 Explodes 20 Seconds, 0.1 (no cap used) 1 5 5 Explodes 20 Trauzl Test, % TNT: (a) 14 140 75°C International Heat Test: % % Loss, 1st 48 Hrs 3.6 % Loss, 2nd 48 Hrs 3.5 Explosion in 100 Hrs None Plate Dent Test: Method % Loss, 2nd 48 Hrs 3.5 Explosion in 100 Hrs None Elamability Index: Detonation Rate: Condition Liquid Charge Diameter, in. 0.39 0.41 Condition | Sample Wt 20 mg | Refractive Index, n ^D ₂₀ 1.4732 |
| Priction Pendulum Test: Steel Shoe Explodes Fiber Shoe Explodes Rifle Bullet Impact Test: Trials Rifle Bullet Impact Test: Trials Barned 0 Burned 0 Unaffected 0 Burned 0 Unaffected 0 1 5 Explosion Temperature: "C Seconds, 0.1 (no cap used) Minimum Detonation: 1 5 20 Explodes 20 Ballistic Mortar, % TNT: 75°C International Heat Test: 3.6 % Loss, 1st 48 Hrs 3.6 % Loss, 2nd 48 Hrs 3.5 Explosion In 100 Hrs None Plate Dent Test: Method % Loss, 2nd 48 Hrs 3.5 Explosion In 100 Hrs None Plate Dent Rate: Confined Confined Glass 9 0.06 Chrage Diameter, in. 0.39° C, 90% RH 0.06 Volatility: 60°C, mg/cm2/hr 0.11 0.14 | | n ₂₅ 1.4713 |
| Steel Shoe Explodes Cc/40 Hs, at 90°C cc/gm/16 hrs 1.6 Rifle Bullet Impact Test: Trials 0 100°C cc/gm/16 hrs 1.1+ Rifle Bullet Impact Test: Trials 0 135°C 135°C Explosions 100 150°C 200 Gram Bomb Sand Test: 5 Unaffected 0 200 Gram Bomb Sand Test: 5 Unaffected 0 200 Gram Bomb Sand Test: 5 Unaffected 0 200 Gram Bomb Sand Test: 5 Seconds, 0.1 (no cap used) Mercury Fulminate Lead Azide 1 1 5 Explodes 222 Ballistic Mortar, % TNT: (a) 140 75°C International Heat Test: % Loss, 1st 48 Hrs 3.6 Condition Condition 100°C Heat Test: % Loss, 1st 48 Hrs 3.6 Density, gm/cc Brisance, % TNT % Loss, 1st 48 Hrs 3.6 Confined Density, gm/cc Glass Steel Condition Condition Condition Condition Condition 1.25 Volatility: 60°C, mg/cm2/hr 0.11 | | n ₃₀ |
| Fiber Shoe 90°C cc/gm/6 hrs 1.6 Rifle Bullet Impact Test: Trials 1.6 Rifle Bullet Impact Test: 700 135°C Explosions 100 150°C Partials 0 200 Gram Bomb Sand Test: Unaffected 0 200 Gram Bomb Sand Test: Unaffected 0 200 Gram Bomb Sand Test: Seconds, 0.1 (no cap used) 1 5 1 5 Explodes 222 10 15 20 Sensitivity to Initiation: 15 20 Mercury Fulminate Lead Azide 10 15 20 Trauzl Test, % TNT: (a) 140 75°C International Heat Test: % Loss, ist 48 Hrs 3.6 Onition Condition % Loss, ist 48 Hrs 3.6 Density, gm/cc Brisance, % TNT Estiguid Etonation Rate: Condition Liquid Liquid Liquid Liquid Condition 100°C Heat Test: 0.06 Onesity, gm/cc 1.6 1.6 % Loss, 1st 48 Hrs 3.5 Explosion in 100 Hrs None Detonation Rate: <td></td> <td>Vacuum Stability Test:</td> | | Vacuum Stability Test: |
| Rifle Bullet Impact Test: Trials 100°C cc/gm/16 hrs 11+ Rifle Bullet Impact Test: % 135°C 135°C Explosions 100 150°C 200 Gram Bomb Sand Test: 200 Gram Bomb Sand Test: Unaffected 0 200 Gram Bomb Sand Test: Sand, gm Liquid method 51.5 Explosion Temperature: "C Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate 10 15 20 Ballistic Mortar, % TNT: (a) 140 75°C International Heat Test: 3.6 Method 101 140 100°C Heat Test: 3.6 Onfined Condition Steel % Loss, 1st 48 Hrs 3.6 Density, gm/cc Brisance, % TNT Estive Confined Steel % Loss, 2nd 48 Hrs 3.5 Explosion in 100 Hrs None Detonation Rate: Condition Liquid Liquid Hygroscopicity: % 30°C, 90% RH 0.06 Charge Diameter, in. 0.39 1.25 Volatility: 60°C, mg/cm2/hr 0.11 11 Steel Condition Liquid | | cc/40 Hrs, at |
| Rifle Bullet Impact Test: Trials 120°C Burned 0 135°C Burned 0 200 Gram Bomb Sand Test: Unaffected 0 200 Gram Bomb Sand Test: Unaffected 0 200 Gram Bomb Sand Test: Unaffected 0 Sensitivity to Initiation: Seconds, 0.1 (no cap used) Minimum Detonating Charge, gm 1 5 Explodes 15 Explodes 222 10 15 Ballistic Mortar, % TNT: (a) 15 140 Trauzl Test; % TNT: (b) 181 75°C International Heat Test: 3-6 20 % Loss, 1st 48 Hrs 3-6 2-5 % Loss, 2nd 48 Hrs 3-5 Brisance, % TNT Flammability Index: Detonation Rate: Condition Flammability Index: 0.06 Charge Diameter, in. 0-39 Hygroscopicity: % 30°C, 90% RH 0.06 Charge Diameter, in. 0-39 1.25 | Fiber Shoe | $-100^{\circ}C cc/gm/16 hrs 11+$ |
| Explosions 100 100 100 ° Partials 0 150 °C Burned 0 200 Gram Bomb Sand Test: Sand, gm 1 Unaffected 0 Sensitivity to Initiation: Minimum Detonating Charge, gm 51.5 Explosion Temperature: "C Sensitivity to Initiation: Mercury Fulminate 6 1 5 Explodes 222 Mercury Fulminate 15 20 Ballistic Mortar, % TNT: (a) 140 75°C International Heat Test: % Loss in 48 Hrs 3.6 Plate Dent Test: Method 181 70°C Heat Test: 9 Loss, 1st 48 Hrs 3.6 % Loss, 2nd 48 Hrs 3.5 Brisance, % TNT Explosion in 100 Hrs % Loss, 2nd 48 Hrs 3.5 Brisance, % TNT Ensity, gm/cc Flammability Index: 0.06 Condition Liquid Hygroscopicity: % 30°°C, 90% RH 0.06 Charge Diameter, in. 0.39 1.25 Volatility: 60°C, mg/cm2/hr 0.11 0.11 0.11 | Rifle Bullet Impact Test: Trials | |
| Partials0 $150^{\circ}C$ Burned0 $200 \text{ Gram Bomb Sand Test:}$ Sand, gm Liquid method 51.5 Explosion Temperature:"CSensitivity to Initiation: Minimum Detonating Charge, gm 1 5Explodes 222 Lead AzideMercury Fulminate Lead Azide 10 15 20 Taul Test, % TNT: (a) 15 20 Trauzl Test, % TNT: (b) 181 Plate Dent Test: Method $Condition$ Condition $00^{\circ}C$ Heat Test: 3.6 $\%$ Loss, 1st 48 Hrs 3.6 9.5 Loss, 2nd 48 Hrs 3.6 3.5 Explosion in 100 Hrs 0.06 Flammability Index:Detonation Rate: ConfinementCondition LiquidLiquid LiquidHygroscopicity: $30^{\circ}C$, 90% RH 0.06 0.39 1.25 | | 135°C |
| Burned 0 200 Gram Bomb Sand Test: Unaffected 0 Sand, gm Liquid method 51.5 Explosion Temperature: "C Sensitivity to Initiation: Minimum Detonating Charge, gm 1 5 Explodes 222 Mercury Fulminate Lead Azide 10 15 16 Tetryl Tetryl 181 75°C International Heat Test: % Loss, 1st 48 Hrs 3.6 Onition Condition % Loss, 1st 48 Hrs 3.6 Density, gm/cc Brisance, % TNT Detonation Rate: Flammability Index: Detonation Rate: Condition Liquid Liquid Hygroscopicity: % 30°C, 90% RH 0.06 Onition Liquid Liquid Hygroscopicity: 60°C, mg/cm2/hr 0.11 0.11 Density, gm/cc 1.6 1.6 | | 150°C |
| Unaffected 0 Sand, gm Liquid method 51.5 Explosion Temperature: "C Sensitivity to Initiation: Minimum Detonating Charge, gm 1 5 Explodes 222 Minimum Detonating Charge, gm 1 5 Explodes 222 10 15 20 Ballistic Mortar, % TNT: (a) 75°C International Heat Test: % Loss, 1st 48 Hrs 3.6 % Loss, 1st 48 Hrs 3.6 Density, gm/cc % Loss, 2nd 48 Hrs 3.5 Brisance, % TNT Flammability Index: Detonation Rate: Confinement Flammability Index: 0.06 Charge Diameter, in. 0.39 Volatility: 60°C, mg/cm2/hr 0.11 0.11 | | 200 Orem Damb Cand Test |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 1 5 5 Explodes 10 15 20 16 75°C International Heat Test: % Loss in 48 Hrs 3.6 % Loss, 1st 48 Hrs 3.6 % Loss, 1st 48 Hrs 3.6 % Loss, 1st 48 Hrs 3.6 % Loss, 2nd 48 Hrs 3.5 Explosion in 100 Hrs Flammability Index: Planemability Index: Play Order Detonation Rate: Condition Liquid Hygroscopicity: % 30°C, 90% RH 0.06 Volatility: 60°C, mg/cm2/hr 0.11 | | |
| Seconds, 0.1 (no cap used) Minimum Detonating Charge, gm 1 5 Explodes 222 10 Mercury Fulminate Lead Azide 10 Trauzl Test, % TNT: (a) 140 75°C International Heat Test: % Loss in 48 Hrs Plate Dent Test: Method % Loss, 1st 48 Hrs 3.6 Condition Condition 100°C Heat Test: % Loss, 1st 48 Hrs 3.5 Explosion in 100 Hrs None Flammability Index: Detonation Rate: Condition Liquid Liquid Hygroscopicity: % 30°C, 90% RH 0.06 0.11 0.11 0.11 | | |
| 1 5 Explodes 222 10 15 20 15 20 Ballistic Mortar, % TNT: (a) 140 75°C International Heat Test: % Loss in 48 Hrs (b) 181 75°C International Heat Test: % Loss in 48 Hrs 3.6 Ornical Condition 100°C Heat Test: Method 100°C Heat Test: % Loss, 1st 48 Hrs 3.6 Onfined | | |
| 5 Explodes 222 10 Tetryl 15 Ballistic Mortar, % TNT: (a) 140 20 Trauzl Test, % TNT: (b) 181 75°C International Heat Test: Plate Dent Test: Method % Loss in 48 Hrs 3.6 Condition Condition 100°C Heat Test: Method Condition Condition % Loss, 1st 48 Hrs 3.6 Density, gm/cc Brisance, % TNT % Loss, 2nd 48 Hrs 3.5 Brisance, % TNT Explosion in 100 Hrs Detonation Rate: Flammability Index: Detonation Rate: Condition Liquid Liquid Hygroscopicity: % 30°C, 90% RH 0.06 Charge Diameter, in. 0.39 1.25 Volatility: 60°C, mg/cm2/hr 0.11 Density, gm/cc 1.6 1.6 | | |
| $\begin{array}{c c c c c c c c } 10 & Tetryl & Tetryl & \\ 15 & & \\ 20 & & & \\ 20 & & & \\ \hline \end{array}$ $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | | |
| 15 20 Ballistic Mortar, % TNT: (a) 140 75°C International Heat Test: 75°C International Heat Test: (b) 181 75°C International Heat Test: % Loss in 48 Hrs 9 181 75°C Heat Test: Method 100°C Heat Test: Method 100°C Heat Test: 0.06 Condition | 10 | |
| 20 Trauzi Test, % TNT: (b) 181 75°C International Heat Test: % Loss in 48 Hrs Plate Dent Test: Method Plate Dent Test: Method 100°C Heat Test: % Loss, 1st 48 Hrs 3.6 Condition % Loss, 1st 48 Hrs 3.6 Density, gm/cc % Loss, 2nd 48 Hrs 3.5 Brisance, % TNT Flammability Index: Detonation Rate: Condition Condition Flammability Index: 0.06 Condition Hygroscopicity: % 30°C, 90% RH 0.06 Charge Diameter, in. 0.39 Volatility: 60°C, mg/cm2/hr 0.11 Density, gm/cc 1.6 | 15 | |
| 75°C International Heat Test: Plate Dent Test: % Loss in 48 Hrs 3.6 100°C Heat Test: Condition % Loss, 1st 48 Hrs 3.6 % Loss, 2nd 48 Hrs 3.5 Explosion in 100 Hrs None Flammability Index: Detonation Rate: Condition Liquid Hygroscopicity: % 30°C, 90% RH 0.06 Volatility: 60°C, mg/cm2/hr 0.11 0.11 | 20 | |
| % Loss in 48 Hrs Plate Dent Test: Method 100°C Heat Test: % Loss, 1st 48 Hrs 3.6 % Loss, 1st 48 Hrs 3.6 % Loss, 2nd 48 Hrs 3.5 Explosion in 100 Hrs None Flammability Index: Detonation Rate: Confinement Glass Steel Condition Liquid Hygroscopicity: % 30°C, 90% RH 0.06 Volatility: 60°C, mg/cm2/hr 0.11 0.11 | 75°C International Heat Test: | |
| 100 C Hear rest: 3.6 Confined % Loss, 1st 48 Hrs 3.5 Density, gm/cc % Loss, 2nd 48 Hrs 3.5 Brisance, % TNT Explosion in 100 Hrs None Detonation Rate: Flammability Index: Confinement Glass Steel Hygroscopicity: 30°C, 90% RH 0.06 Charge Diameter, in. 0.39 1.25 Volatility: 60°C, mg/cm2/hr 0.11 Density, gm/cc 1.6 1.6 | | |
| % Loss, 1st 48 Hrs 3.6 Confined % Loss, 2nd 48 Hrs 3.5 Density, gm/cc Explosion in 100 Hrs None Brisance, % TNT Flammability Index: Detonation Rate: Confinement Hygroscopicity: 30°C, 90% RH 0.06 Volatility: 60°C, mg/cm2/hr 0.11 | 100°C Heat Test: | Condition |
| % Loss, 2nd 48 Hrs 3.5 Density, gm/cc Explosion in 100 Hrs None Brisance, % TNT Flammability Index: Detonation Rate: Confinement Class Hygroscopicity: % 30°C, 90% RH 0.06 Charge Diameter, in. 0.39 Volatility: 60°C, mg/cm2/hr 0.11 | | |
| Explosion in 100 H/s None Flammability Index: Detonation Rate: Confinement Hygroscopicity: % 30°C, 90% RH 0.06 Volatility: 60°C, mg/cm2/hr 0.11 | , | |
| Flammability Index: Confinement Glass Steel Hygroscopicity: % 30°C, 90% RH 0.06 Condition Liquid Liquid Volatility: 60°C, mg/cm2/hr 0.11 Density, gm/cc 1.6 1.6 | Explosion in 100 Hrs None | Brisance, % TNT |
| Hygroscopicity: % 30°C, 90% RH 0.06 Condition Liquid Liquid Volatility: 60°C, mg/cm2/hr 0.11 Density, gm/cc 1.6 | Flammability Index: | |
| Hygroscopicity: % 30°C, 90% RH 0.06 Charge Diameter, in. 0.39 1.25 Volatility: 60°C, mg/cm2/hr 0.11 Density, gm/cc 1.6 1.6 | | |
| Volatility:60°C, mg/cm2/hr0.11Density, gm/cc1.6 | Hygroscopicity: % 30 ⁰ C, 90% RH 0.06 | |
| | | |
| I Rate meters/second 1600-1000 7700 | volatility: 60° C, mg/cm ² /hr 0.11 | Rate, meters/second 1600-1900 7700 |

| Booster Sensitivity Test: | | Decomposition Equation: | 17.3 | 10 ^{19.2} |
|--|------------|---------------------------------------|--------------------|--------------------|
| Condition | | Oxygen, otoms/sec (Z/sec) | 10 ^{17•3} | 10 -2.2 |
| Tetryl, gm Wax, in. for 50% Detonation | | Heat, kilocolorie/mole | 41.4 | 45.0 |
| Wax, m. for 50% Detonation Wax, gm | | (AH, kcal/mol) | | |
| | | Temperature Range, °C | 90-135 | 125-150 |
| Density, gm/cc | | Phase | Liquid | Liquid |
| Heat of: | - | Armor Plate Impact Test: | | |
| Combustion, cal/gm | 1616 | · · · · · · · · · · · · · · · · · · · | | |
| Explosion, cal/gm | 1600 | 60 mm Mortar Projectile: | | |
| Gas Volume, cc/gm | 715 | 50% Inert, Velocity, ft, | /sec | |
| Formation, col/gm | 400 | Aluminum Fineness | | |
| Fusion, col/gm Detonation, cal/gm | 1486 | | | |
| Specific Heat: col/gm/°C | | 500-1b General Purpose Bo | ombs: | |
| Liquid | 0.356 | Plate Thickness, inches | | |
| Solid | | 1 | | |
| 30114 | 0.315 | 11/4 | | |
| | | 11/2 | | |
| | | 13/4 | | |
| Burning Rate: | | 1-74 | | |
| cm/sec | | | | |
| | | Bomb Drop Test: | | |
| Thermal Conductivity: | | | iensies Death | . O an analas |
| col/sec/cm/°C | | T7, 2000-Ib Semi-Armor-P | vercing Bomb v | s Concrete: |
| Coefficient of Expansion: | | Max Safe Drop, ft | | |
| Linear, %/°C | | 500-Ib General Purpose Be | omb vs Concre | te: |
| Volume, %/°C | | | | |
| volume, <i>by</i> C | | Height, ft | | |
| Hardness, Mohs' Scale: | | Trials | | |
| | | Unaffected | | |
| Young's Modulus: | | Low Order | | |
| E', dynes/cm ² | | High Order | | |
| E, lb/inch ^a | | | | |
| Density, gm/cc | | 1000-lb General Purpose B | omb vs Concret | e: |
| Commenceire Dimentity II (1 - 1 - 1 | | Height, ft | | |
| Compressive Strength: Ib/inch ² | | Trials | | |
| | | Unaffected | | |
| Vapor Pressure: | | Low Order | | |
| <u>oc</u> <u>mm_Mercury</u> <u>oc</u> | mm Mercury | High Order | | |
| 0.00025 60 | 0.0188 | | | |
| 30 0.00083 70 | 0.043 | | | |
| | | | | |
| <u>°C</u> <u>mm Mercury</u> <u>°C</u> 20 0.00025 60 | 0.0188 | Low Order | | |

| Fragmentation Test: | Shaped Charge Effectiveness | , TNT = 100: | | | |
|--|--|---------------------|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91 : Density, gm/cc Charge Wt, Ib | Glass Cones Hole Volume Hole Depth | Steel Cones | | | |
| Total No. of Fragmenis: For TNT | Color: | Colorless | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Propellant ingredient, demoli- tion explosive ingredient, grenade burster ingredient | | | | |
| Total No. of Fragments: For TNT | Method of Loading: | | | | |
| For Subject HE | Loading Density: gm/cc | | | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | | | | |
| Density, gm/cc | Method With acctone generally no | | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-D | istance) Class 9 | | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | | | | |
| Air, Confined: Impulse | Heat of Transition, cal Transition: | 1/gm: | | | |
| Under Water: Peak Pressure | Liquid → labile Labile → stable Liquid → stable | 5.2 28.0 33.2 | | | |
| Impulse Energy | Hydrolysis, % Acid: | | | | |
| Underground: Peak Pressure Impulse | 10 days at 22°C 5 days at 60°C 82.1°C KI Test: | < 0.002 0.005 | | | |
| Energy | Minutes | 10+ | | | |
| | | | | | |

| Sample Wt, Temperatur Time, hour Volume of | re, ^o C 65 rs 20 | 1.6 | 75 40 nil |
|---|--|-----|-----------------|
| Viscosity: (| 2) | | |
| ° _C | Centipoises | | |
| 10 20 30 40 50 60 | 69.2 36.0 21.0 13.6 9.4 6.8 | | |

Gas Evolved at Atmospheric Pressure, cc:

Fragmentation Test:

20 mm HE, Mark 1, Projectile, Total No. of Fragments for:

| Nitroglycerin | 22 |
|-------------------|----|
| Tetranitromethane | 17 |
| Tetranifromethane | 17 |

Minimum Propagating Diameter: (d)

| <u>[%] Dimethylphthalate</u> <u>in NG</u> | <u>Min. Propagating</u> Diameter, inches | Maximum Diameter for 2 Failures in 2 Trials, inches |
|---|---|---|
| 0 5 10 15 | (3/16 cairns) 1/8 1/4 | 1/16 B/A6 3/8 |
| 20 22.5 25 | 3/4 1 1.55 | 17192 2 |

Sensitivity to Electrostatic Discharge, Joules (test condition, unconfined;no value given for confinement):> 12.5

| Solubility, | grams | \mathbf{of} | nitroglycerin/100 | gn | (%) | of: |
|-------------|-------|---------------|-------------------|----|-----|-----|

| $\underline{\mathbf{W}}_{i}$ | ater | Alc | <u>ohol</u> | Trichlor | ethylene | Carbon Tetr | achloride |
|------------------------------|----------------------|----------------|--------------|-----------|----------|-------------|-----------|
| °C | <u>%</u> | o _C | 76 | <u>oc</u> | <u>%</u> | <u>°</u> C | % |
| 15 20 50 | 0.16 0.18 0.25 | 0 20 | 37•5 54.0 | Rm | 22 | Rm | 2 |

| Carbon Disulfide | | | | | gm/100 gn (%), at 25 ⁰ C in | | | |
|--|-----------------|----------------|----------|-------|--|---|----------|--------|
| <u>°c</u> | | <u>%</u> | | - | Ether [∞] 2: 1 Ether:Alcohol > 100 | | | |
| Ambi | ent | 1 | | | Acetone | | W PIC | 10 |
| Sol | uble in a | 11 Pro | portion | s in: | | | | |
| MethanolPherAcetonePyriEtherXyleEthyl acetateNitroAmyl acetatep-NMethyl nitrateLiquEthyl nitrateChloNitroglycolEthyTetranitrodiglycerineEthyAcetic acidTetrBenzeneDick | | | | | | nzene otoluene DNT corm chloride oromide nloroethy coethylen | | itrate |
| Sol | ubilitv i | n NG, | of: | | | | | |
| | <u>ohol</u> | D | NT | T | NT | Wa | ter | |
| °c | % | o _C | <u>%</u> | °C | <u>%</u> | °C | <u>%</u> | |
| 0 20 50 | 3.4 5.4 ∞ | 20 | 35 | 20 | 30 | 25 | 0.06 | |
| Prepar | ation: | | | | | | | |

 $\begin{array}{c} CH_2 \longrightarrow OH \\ I \\ CH \longrightarrow OH \\ CH_2 \longrightarrow OH \end{array} + 3HNO_3 \longrightarrow \begin{array}{c} CH_2 \longrightarrow ONO_2 \\ I \\ CH \longrightarrow ONO_2 \\ I \\ CH_2 \longrightarrow ONO_2 \end{array} + 3H_2O$

Glycerine is usually nitrated at 25° C, or below, by adding it very slowly to a well agitated mixture of nitric and sulfuric acids, e.g., 40/59.5/0.5, nitric acid/sulfuric acid/water, using an acid/glycerine ratio of approximately 6. Agitation of the reaction mixture is accomplished by use of compressed air. A rapid temperature rise, or appearance of red fumes, automatically requires dumping of the charge, immediately, into a drowning vessel filled with water. After all the glycerine has been added to the nitrator, agitation and cooling are continued until the temperature drops to about 15° C, and the charge is then run into a separator where the NG rises to the top, and is run off' to the neutralizer. The nitroglycerin is washed first with water, then with sodium carbonate, and finally with water. The resultant NG when washed with water, produces washings which do not color phenolphthalein, and itself is neutral to litmus paper.

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Origin:

Nitroglycerin was first prepared in 1846 or 1847 by Ascanio Sobrero, an Italian chemist (Mem Acad Torino (2) 10, 195 (1847)). For several years after this discovery, nitroglycerin attracted little interest as an explosive until Alfred Nobel in 1864 patented improvements in its manufacture and method of initiation (British Patent <u>1813</u>). Nobel gave the name dynamite to mixtures of nitroglycerin and non-explosive absorbents, such as charcoal, siliceous earth or Kieselguhr (British Patent <u>1345</u> (1867)). Later developments led to gelatine dynamites, ammonia dynamites, and so called straight dynamites. The first propellants using nitroglycerin were called Ballistite (Nobel, British Patent <u>1471</u> (1888))- and Cordite (Abel and Dewar, British Patents <u>5614</u> and <u>11,664</u> (1889)).

Destruction by Chemical Decomposition:

Nitroglycerin is decomposed by adding it slowly to 10 times its weight of 18% sodium sulfide (Na₂S.9H₂O). Heat is liberated by this reaction; but this is not hazardous if stirring is maintained during the addition of nitroglycerin and continued until solution is complete.

References: 48

(a) A. H. Blatt, <u>Compilation of Data on Organic Explosives</u>, OSRD Report No. 2014, 29 February 1944.

- (b) Ph. Naoum, Z ges Schiess-Sprengstoffw, pp. 181, 229, 267 (27 June 1932).
- (c) Landolt Bornstein, Physikalisch-Chemische Tabellen, 5th Ed. (1923).

International Critical Tables.

B. T. Fedoroff et al, <u>A Manual for Explosive Laboratories</u>, Vol I-IV, Lefax Society, Inc., Philadelphia, 1943, 1946.

(d) H. A. Strecker, Initiation, Propagation and Luminosity Studies of Liquid Explosives, OSRD Report No. 5609, 3 December 1945.

(e) Also see the following Picatinny Arsenal Technical Reports on Nitroglycerin:

| <u>o</u> | <u>1</u> | 2 | <u>3</u> | <u>4</u> | 5 | <u>6</u> | <u>7</u> | <u>8</u> | <u>9</u> |
|---|---|---|--|--|------------------------------|--|--|---|---|
| 620 660 800 1020 1150 1210 1410 1620 1680 | 511 551 701 891 911 1031 1041 1151 1611 1651 1651 1781 1851 1851 1931 | 652 672 922 1142 1282 1362 1542 1662 1742 1752 1992 | 233 343 673 903 1023 144 3 164 3 1663 1863 1993 | 454 494 1024 1074 1084 1454 1524 1624 1674 1754 | 1155 1235 1955 2015 | 1206 1456 1496 1556 1616 1786 1816 1896 2056 | 817 837 1197 1297 1637 1817 1847 | 768 1348 1398 1738 1918 2098 | 69 249 579 709 1349 1359 2119 |

⁴⁸See footnote 1, page 10.

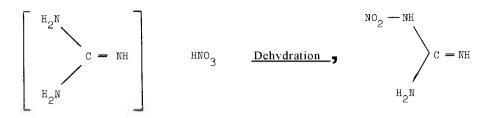
2021 2181 2201

| Composition: % | | Molecular Weight: $(CH_4N_4O_2)$ | 104 |
|---|---------------|---|-------------------|
| C 11.5 NH ₂ | | Oxygen Balance: CO ₂ % CO % | -31 -15.4 |
| H 3.9 HN = C | | Density: gm/cc Crystal | 1.72 |
| N 53.8 NH NO ₂ | | | 232 |
| 0 30.8 2 | | Melting Point: °C | 232 |
| C/H Ratio 0.038 | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 47 26 7 | Boiling Point: "C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| Friction Pendulum Test: | (e) | | |
| Steel Shoe | Unaffected | Vacuum Stability Test: cc/40 Hrs. at | |
| Fiber Shoe | Unaffected | 90°C | |
| Rifle Bullet Impact Test: 5 Trials | (e) | – 100°C 120°C | 0.37 0.44 |
| % | ζ, | 135°C | 0.44 |
| Explosions 0 | | 150°C | |
| Portials 0 Burned 0 | | 200 Gram Bomb Sand Test: | |
| Unaffected 100 | | Sand, gm | 36.0 |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) 1 | | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate | |
| 5 Decomposes 275 | | Lead Azide | 0.20 |
| 10 | | Tetryl | 0.10 |
| 15 | | Ballistic Mortar, % TNT: (a) | 104 |
| 20 | | Trauzi Test, % TNT: (b) | 101 |
| 75°C International Heat Test: % Loss in 48 Hrs | 0.04 | Plate Dent Test: (c) Method | А |
| 100°C Heat Test: | | Condition | Pressed |
| % LOSS, 1st 48 Hrs | 0.18 | Confined | No |
| % Loss, 2nd 48 Hrs | 0.09 | Density, gm/cc Brisance, % TNT | 1.50 95 |
| Explosion in 100 Hrs | None | | |
| Flammability Index: | | Detonation Rate: (e) Confinement Condition | |
| Hygroscopicity: % 30 ⁰ C, 90% RH | None | Charge Diameter, in. | , |
| Volatility: | None | Density, gm/cc | 1.55 |

| Fragmentation lest: | Shaped Charge Effectiveness, $TNT = 100$: | | | | | |
|---|---|---------------------------------------|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | | | | | |
| Total No. of Fragments: For TNT | Color: Color | rless | | | | |
| For Subject HE | Principal Uses: | | | | | |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Propellant composition ingred bursting charge ingredient | lient, | | | | |
| Total No. of Fragments: For TNT | Method of Loading: | | | | | |
| For Subject HE | Loading Density: gm/cc | | | | | |
| Fragment Velocity: ft/sec | A t 3000 psi | 0.95 | | | | |
| At 9 ft At 25½ ft | Storage: | | | | | |
| Density, gm/cc | Method | Dry | | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 | | | | |
| Air: Peak Pressure Impulse | Compatibility Group Exudation | Group I | | | | |
| Energy | Solubility, gm/100 gm (%), in: | | | | | |
| Air, Confined: impulse | Water 2 | 5 0.44 | | | | |
| Under Water: Peak Pressure Impulse | 10 1.0 N Potassium Hydroxide 2 40% Sulfuric Acid 2 | 5 1.2 0 3.4* | | | | |
| Energy | * gm/100 cc solution | | | | | |
| Underground: Peak Pressure Impulse Energy | Booster Sensitivity Test: Condition Tetryl, gn Wax, in. for 50% Detonation Density, gm/cc | (d) Pressed 100 0.67 1.41 | | | | |
| | Heat of: Combustion, cal/gm Explosion, cal/gm Gas Volume, cc/gm Formation, cal/gm | 1995 721 1077 227 | | | | |

Preparation:

(Chemistry of Powder and Explosives, Davis)



Four hundred gms of dry guanidine nitrate is added in small portions to 500 cc concentrated sulfuric acid at 10° C, or below. As soon as all crystals have disappeared the milky solution is poured into 3 liters of ice-water, and allowed to stand until crystallization is complete. The product is filtered, rinsed with water, and recrystallized from about 4 liters of boiling water, yield about 90%.

Origin:

Nitroguanidine was first prepared in 1877 by Jousselin, but it was 1900 before it found use in propellant compositions. During World War I, nitroguanidine was used by the Germans as an ingredient of bursting charge explosives.

Destruction by Chemical Decomposition:

Nitroguanidine is decomposed by dissolving in 15 times its weight of 45% sulfuric acid at room temperature and warming the solution until gas is evolved. Heating is continued for one-half hour.

References: 49

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III</u> - <u>Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, OSRD Report No. 5746, 27 December 1945.

(b) Canadian Report, CE-12, 1 May-15 August 1941.

(c) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(d) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute for</u> <u>Tetryl in Boosters</u>, NL Memo 10,303, 15 June 1949.

(e) Departments of the Army and the Air Force TM 9-1910/TO 11A-1-34, Military Explosives, April 1955.

⁴⁹See footnote 1, page 10.

Nitroguanidine

(f) Also see the following Picatinny Arsenal Technical Reports on Nitroguanidine:

| <u>o</u> | <u>1</u> | 2 | 3 | <u>6</u> | <u>_7</u> | 8 | 2 |
|----------|----------------------|----------------------|----------------------|----------|-------------|-----|--------------|
| 1490 | 1391 2181 2201 | 1282 1392 2142 | 1183 1423 2193 | 1336 | 907 2177 | 758 | 1439 1749 |

| Composition: % | Molecular Weight: $(C_{4}H_{6}N_{4}O_{11})$ | 286 |
|--|---|------------------------|
| c 16.8 $O_2 NO - CH_2$ | Oxygen Balance: CO₂ % CO % | 0.0 22 |
| 0_NO-CH C - NO | Density: gm/cc 20 [©] C | 1.64 |
| 0 61.5 0 ₂ NO - CH ₂ | Melting Point: "C | |
| C/H Ratio 0.126 | Freezing Point: °C | - 39 |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 25 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | Boiling Point: °C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | 1.4896 1.4874 |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C | |
| Rifle Bullet Impact Test: Trials % Explosions Partials | 100°C 120°C 135°C 150°C | |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm 0.2 gm sample absorbed by 0.2 gm of kleselguhr | 28 |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) 1 5 Ignites 185 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminote Lead Azide Tetryl | |
| 15 20 | Ballistic Mortar, % TNT: | |
| | Trauzi Test, % TNT: | |
| 75°C International Heat Test: % Los s in 48 Hrs | Plate Dent Test: Method | |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | | s (1mm wall) |
| Hygroscopicity: % | Condition Charge Diameter, in. Density, gm/cc | Liquid 0.39 1.64 |
| Volatility: 25°C, mg/cm ² /24 hrs 0.127 x 10 ⁻³ | Rate, meters/second | 7860 |

Nitroisobutylglycerol Trinitrate (NIBTN) Liquid

| Fragmentation Test: | Shaped Charge Effectiveness, TNT $=$ 100: |
|---|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: Yellow oil |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib Total Ne, of Frameworks | Principal Uses: Gelatinizing agent for nitrocellulose |
| Total No. of Fragments: For T N T For Subject HE | Method of Loading: |
| Fragment Velocity: ft/sec | Loading Density: gm/cc |
| At 9 ft At 25½ ft Density, gm/cc | Storage: Method Liquid |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation |
| Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy Underground: | Solubility: Soluble in methyl and ethyl alcohols, ace- tone, ether, ethylenedichloride, chloroform and benzene. Insoluble in water, carbon disulphide, and petroleum ether. <u>Toxicity:</u> Slight, decidedly less than nitroglycerin. |
| Peak Pressure Impulse Energy | Gelatinizing Action: Slight on nitrocellulose. 82.2°C KT Test: Minutes 2 |

Preparation:

A total of 675 gn 37% formalin is added to 150 gn nitromethane containing 2 gn potassium carbonate hemi-hydrate. The first 200 gn formalin is added slowly, keeping the temperature below 30° C, and then the heat of reaction is allowed to raise the temperature to 80° C, and the mixture then heated two hours at 90° C. The reaction mixture is then concentrated at reduced pressure and diluted, and this process repeated several times to remove formaldehyde. After the final concentration the cooled mixture is filtered and the crystalline product recrystallized from alcohol and then several times from ether and dried.

The nitrated product is then obtained by nitrating 50 gm nitroisobutylglycerol with 300 gm mixed acid (60/38/2, sulfuric acid/nitric acid/water) below 15°C for 1.5 hours.

Origin:

This explosive (also called Trimethylolnitromethane Trinitrate, Nitroisobutanetriol Trinitrate, Nitroisobutylglycerin Trinitrate and incorrectly but widely used Nitroisobutylglycerol Trinitrate) was first described in 1912 by Hofwimmer (Z ges Schiess - Sprengstoffw 7, 43 (1912). Hofwimmer prepared the compound by the condensation of 3 moles of formaldehyde with 1 mole of nitromethane in the presence of potassium bicarbonate, the subsequent nitration of the product. The explosive can now be produced from coke, air, and natural gas.

References: 50

(a) H. A. Aaronson, <u>Study of Explosives Derived from Nitroparaffins</u>, PATR No. 1125, 24 October 1941.

- (b) M. Aubry, Me'' poudr, 25, 197-204 (1932-33); CA 27, 4083 (1933).
- (c) A. Stettbacher, Nitrocellulose 5, 159-62, 181-4, 203-6 (1934); CA 29, 1250 (1935).
- (d) W. de C. Crater, U.S. Patent 2,112,749 (March 1938); CA 32, 3964 (1938).

(e) H. J. Hibshman, E. H. Pierson, and H. B. Haas, Ind Eng Chem <u>32</u>, 427-9 (1940); CA <u>34</u>, 3235 (1940).

(f) A. Stettbacher, Z ges Schiess Sprengstoffw 37, 62-4 (1942); CA 38, 255 (1944).

⁵⁰See footnote 1, page 10.

Nitrostarch Demolition Explosive (NSX)

| Composition: % | | Molecular Weight: | 325 |
|--|----------------------------|---|----------|
| Nitrostarch (12.50% N) Barium Nitrate Mononitronaphthalene | 49 40 7 | Oxygen Balance: CO, % CO % | -19 a |
| Paranitroaniline | 3 | Density: gm/cc | |
| 0 i 1 | 1 | Melting Point: "C | |
| C/H Ratio | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | 21 | Boiling Point: °C | |
| Sample Wt 20 mg | а | Refractive Index, n ^D ₂₀ | |
| Picatinny Arsenal Apparatus, in. Sample Wt, mg | a | n ₂₅ | |
| | | n ^D 30 | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| | kles, snaps | cc/40 Hrs, at | |
| Fiber Shoe Unafi | fected | 90°C | |
| Rifle Bullet Impact Test: 10 Trials | 8 Trials* | 100°C | 11+ |
| % | % | 120°C | |
| Explosions 90 | õ | 135°C | |
| Partials 0 | 13 | 150°C | |
| Burned 0 | 0 200 Gram Bomb Sand Test: | | |
| *Rindated cited paper 10 | 87 | Sand, gm | 39.5 |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) | | Sensitivity to Initiation: Minimum Detonating Charge, gm | |
| 1 | | Mercury Fulminate | 0.26 |
| 5 Decomposes 195 | | Lead Azide | |
| 10 | | Tetryl | |
| 15 | | | |
| 20 | | Ballistic Mortar, % TNT: (a) | 96 |
| 75°C International Heat Test: | | Trauzl Test, % TNT: | |
| % Loss in 48 Hrs | 0.2 | Plate Dent Test: | |
| | _ | Method | |
| 100°C Heat Test: | | Condition | |
| % Loss, 1st 48 Hrs | 0.3 | Confined | |
| % Loss, 2nd 48 Hrs | 0.3 | Density, gm/cc Brisance, % TNT | |
| Explosion in 100 Hrs | None | | |
| Flammability Index: | | Detonation Rate: Confinement | |
| Hygroscopicity: % 30°C, 90% RH | 2.1 | Condition Charge Diameter, in. | |
| Volatility: | | Density, gm/cc Rate, meters/second | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: |
|---|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib Total No. of Fragments: For TNT | Principal Uses: Demolition, bursting charges, and priming compositions Method of Loading: Hand tamped |
| For TNT For Subject HE | |
| Fragment Velocity: ft/sec At 9 ft | Loading Density: gm/cc Apparent 0.92 |
| At 25½ ft Density, gm/cc | Storage: |
| | Method Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 |
| Air: Peak Pressure Impulse | Compatibility Group Group I Exudation None |
| Energy Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | 120°C Heat Test: Minutes Salmon Pink 70 Red Fumes 255 Explodes 256 |

Nitrostarch Demolition Explosive (NSX)

Preparation: (b)

The nitration of starch proceeds with the formation of hexanitro starch according to the following equation:

 $2C_{6}H_{10}O_5 + 6HNO_3 \rightarrow C_{12}H_{14}O_4(ONO_2)_6 + 6H_2O_5$

Tapioca starch is considered the best for nitration purposes, although other starches give fairly stable products. The starch, pretreated to remove oils, fats and water soluble impurities, is dried and screened. Feeding of the dried starch into stainless steel nitrators containing mixed acid (62%-63% HNO₃ and 37%-38% H₂SO₄) is done slowly with constant agitation of the mixture. The heat evolved must be controlled by cooling coils. The nitrated starch is separated from the spent acid, washed with a large amount of water and centrifuged. Final drying is on trays heated to 35° - 40° C with air. This product is so sensitive even a static discharge might cause explosion.

Nitrostarch demolition explosives contain a high percentage of nitrostarch, an oxidizing agent, mineral oil, a stabilizer and/or other ingredients.

Orinin:

Nitrostarch was first prepared in 1833 by Branconnot, who called it xyloidine (Ann chim phys [2] 52, 290 (1833)). T. J. Pelouze studied xyloidine further and reported its explosive properties (Compt rend 7, 713 (1838). It found military use in the United States during World Wars I and II as blasting explosives and as an ingredient of bursting charges and priming compositions.

References: 51

(a) W. R. Tomlinson, Jr., <u>Physical and Explosive Properties of Military Explosives</u>, PATR No. 1372, 29 November 1943.

(b) G. D. Clift and B. T. Fedoroff, <u>A Manual for Explosives Laboratories</u>, Vol I, Lefax Society, Inc., Philadelphia (1942).

(c) Also see the following Picatinny Arsenal Technical Reports on Nitrostarch Explosives:

| 1 | 2 | 4 | Z | <u>a</u> | <u>0</u> |
|------|-------------|------|------|-------------------|----------|
| 1611 | 782 2032 | 1034 | 1117 | 838 848 | 1269 |

⁵¹See footnote 1, page 10.

Octol, 70/30

| Composition: % | | Molecular Weight: | 265 |
|---|--------------------------|--|-------------|
| 70 HMX TNT | 70 30 | Oxygen Balance: CO, % CO % | -38 -7•5 |
| | | Density: gm/cc Ca | ast 1.80 |
| | | Melting Point: °C | |
| C/H Ratio | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | | Boiling Point: °C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. | 18 26 | Refractive Index, n ^D ₂₀ n ^D ₂₃ | |
| Sample Wt, mg | 20 | n ₃₀ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| Steel Shoe | Unaffected Unaffected | cc/40 Hrs, at 90°C | |
| Fiber Shoe | Ollaffected | 100°C | |
| Rifle Bullet Impact Test: Trials | | 120°C | 0.37 |
| Systems % | | 135°C | 21 |
| Explosions Partials | | 150°C | |
| Burned | | 200 Gram Bomb Sand Test; | |
| Unaffected | | Sand, gm Exploratory | 58.4 |
| Explosion Temperature: Seconds, 0.1 (no cap used) | ° _C | Sensitivity to Initiation: Minimum Detonating Charge, gm | |
| 1 5 Elemente en esta el la | v 335 | Mercury Fulminate | |
| 5 Flames erratical 10 15 | IY 333 | Lead Azide Tetryl | 0.30 |
| 20 | | Ballistic Mortar, % TNT: | 115 |
| | | Trauzl Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | | Plate Dent Test: Method | |
| 100°C Heat Test: | | Condition | |
| % Loss, 1st 48 Hrs | | Confined | |
| % Loss, 2nd 48 Hrs | | Density, gm/cc | |
| Explosion in 100 Hrs | | Brisance, % TNT | |
| Flammability Index: | | Detonation Rate: Confinement | None |
| Hygroscopicity: % | | Condition | Cast |
| | | Charge Diameter, in. Density, gm/cc | 1.0 1.80 |
| | | | 1.00 |

.

| Booster Sensitivity Test: Condition Tetryl, gm Wax, in. for 50% Detonation Wax, gm Density, gm/cc | | Decomposition Equation: Oxygen, atoms/sec (Z/sec) Heat, kilacalarie/male (AH, kcal/mal) Temperature Range, °C Phase |
|--|-----------------------------------|---|
| Heat of: Combustion, cal/gm Explosion, cal/gm Gas Volume, cc/gm Formation, cal/gm Fusion, cal/gm | 2722 107 ¹ 4 847 | Armor Plate Impact Test: 60 mm Mortar Projectile: 50% Inert, Velocity, ft/sec Aluminum Fineness 500-lb General Purpose Bombs: |
| Specific Heat: col/gm/°C | | Plate Thickness, inches 1 1¼ 1½ 1½ 1¾ |
| Burning Rate: cm/sec Thermal Conductivity: col/sec/cm/°C | | Bomb Drop Test: T7, 2000-Ib Semi-Armor-Piercing Bomb vs Concrete: |
| Coefficient of Expansion: Linear, %/°C | | Mox Safe Drop, ft 500-lb General Purpose Bomb vs Concrete: |
| Volume, %/°C Hardness, Mohs' Scale: | | Height, ft Trials |
| Young's Modulus: E, dynes/cm² | | Unaffected Low Order High Order |
| E, lb/inch² Density, gm/cc | | 1000-IbGeneral Purpose Bomb vs Concrete: |
| Compressive Strength: Ib/inch ² | 1510 See below | Height, ft Trials Unaffected |
| Vapor Pressure: "C mm Mercury <u>Compressive Strength:</u> 1b/inch ² | * | Low Order High Order |
| Average (10 tests) High Low | 1510 17 ⁴ 0 1330 | Ultimate Deformation:%Average (10 tests)2.26High2.58Low1.97 |

*Test specimen 1/2" x 1/2" cylinder (approximately 3 gm) pressed at 3 tons (6,000 lb) total load or 30,000 psi with a 2 minute time of dwell.

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | |
|---|--|---------------------------|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | |
| Total No. of Fragments: For TNT | Color: | Buff |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: HE projectile and bomb | filler |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: | Cast |
| | Loading Density: gm/cc | 1.80 |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | |
| Density, gm/cc | Method | Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | Group I |
| Air, Confined: Impulse Under Water: Peak Pressure | Work to Produce Rupture: ft-lb/inch ³ Average (10 tests) High Low | * 1.55 1.87 1.10 |
| Impulse Energy | Efflux Viscosity, Saybolt Seconds: | 5.9 |
| Underground: Peak Pressure Impulse Energy | | |
| | *Test specimen 1/2" x 1/2" cylinder (a mately 3 gm) pressed at 3 tons (6,000 total load or 30,000 psi with a 2 min time of dwell. | 1b) |

| Explosive | Simulated Altitude, Feet | One-Inc Confined m/s | h Column Unconfined , m/s | | h Column Unconfined m/s |
|--|-----------------------------|----------------------------|---------------------------------|---------|-------------------------------|
| 70/30, RDX/INT; density, gm/cc 1.62 | Ground | 7900 | 8100 | 7660 | 8030 |
| | 30,000 | 8020 | 8120 | 7900(4) | 7800 |
| Average | | 8005 | 8085 | 7895 | 7873 |
| 70/30, HMX/INT; | Ground | 7960 | 7900(4) | 7870 | 7640(4) |
| density, gm/cc 1.61 | 30,000 | 8050 | 8060 | 7930 | 7710 |
| | 60,000 | 8020 | 7930 | 7890 | 7650 |
| | 90,000 | 7950 | 8000 | 7940 | 7650 |
| Average | | 7995 | 7973 | 7908 | 7663 |

Effect of Altitude, Charge Diameter and Degree of Confinement on Detonation Velocity* (Reference b)

*70/30 Octol confined charge in 1/4" steel tube, AISI 1015 seamless, 1" diameter 18" long, and 2" diameter 7" long. All means were determined from sets of five values unless otherwise indicated by (). A 26 gn tetry booster was used to initiate each charge.

| | | Į į | Himilated Al | .t.itude, Fe | et |
|----------------|--|---------------|---------------|----------------------|---------------|
| Explosive | <u>Charge Diameter.</u> <u>Inches</u> | Ground m/s | 30,000 m/s | <u>60,000</u> m/s | 90,000 m/s |
| 70/30, RDX/INT | 1 | 3415 | 3672 | 3666 | 3685 |
| | 2 | 4647 | 5192 | 5236 | 6011 |
| | | | | | |
| | 2 | 4703 | 5464 | 6089 | 6111 |

Average Fragment Velocities at Various Altitudes* (g)

*Outside diameter 2.54"; inside diameter 2.04"; length 7".

Tensile Strength:*

| | lb/inch ² |
|-------------------|----------------------|
| Average (8 tests) | 169 |
| High | 204 |
| Low | 128 |

*Test specimen as per Picatinny Arsenal sketch XL-076B, at 21°C.

| Modulus of Elasticity:* | |
|-------------------------|----------------------|
| 1 | lb/inch ² |
| Average (10 tests) | 73,200 |
| High | 79,300 |
| · Low | 63,000 |

*Test specimen 1/2" x 1/2" cylinder (approximately 3 gm) pressed at 3 tons (6,000 lb) total load or 30,000 psi with a 2 minute time of dwell.

Setback Sensitivity Test: (a)

| Critical Pressure | 92,000 psi* |
|-------------------|-------------|
| Density, gm/cc | 1.72 |

| 1/2 - 2 | 1297 |
|----------------|------|
| 2 - 5 | 665 |
| 5 - 10 | 497 |
| 10 - 25 | 661 |
| 25 - 50 | 471 |
| 50 - 75 | 247 |
| 75 - 150 | 322 |
| 150 - 750 | 295 |
| 750 - 2500 | 12 |
| Total Number | 4467 |

Octol, 75/25

| Composition: | Molecular Weight: | 276 |
|---|--|---------------|
| 75 HMX 75 TNT 25 | Oxygen Balance: O, % CO % | - 35 - 6.3 |
| | Density: gm/cc Cast | 1.81 |
| | Melting Point: °C | |
| C/H Ratio | Freezing Point: "C | |
| Impoct Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg | Boiling Point: "C Refractive Index, n ^D ₂₀ | |
| Picatinny Arsenal Apparatus, in. 17 Sample Wt, mg 25 | n ₂₅ | |
| | n ₃₀ | |
| Friction Pendulum Test: | Vacuum Stability lest: | |
| Steel Shoe Unaffected Fiber Shoe Unaffected | cc/40 Hrs, at 90°C | |
| 92. | 100°C | |
| Rifle Bullet Impoct Test: 10Triols <i>%</i> <u>3/16" Stee1 1/8" A1</u> | 120°C | 0,39 |
| Explosions 70 70 | 135°C | |
| Partials | 150°C | |
| Burned | 200 Gram Bomb Sand Test: | |
| Unaffected 30 30 | Sand, gm Exploratory | 62.1 |
| Explosion Temperature: ^O C Seconds, 0.1 (no cap used) | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate | |
| 5 Flames erratically 350 | Lead Azide | 0.30 |
| 10 | Tetryl | |
| 15 | Ballistic Mortar, % TNT: | 116 |
| 20 | Trouri Test, % TNT: | 110 |
| 75°C International Heat Test: | , | |
| % Loss in 48 Hrs | Plate Dent Test: Method | |
| 100°C Heat Test | Condition | |
| % Loss, 1st 48 Hrs | Confined | |
| % Loss, 2nd 48 Hrs | Density, gm/cc | |
| Explosion in 100 Hrs | Brisance, % TNT | |
| Elemmehility ledev: | Detonation Rote: | |
| Flammability Index: | Confinement | None |
| Hygroscopicity: % | Condition Charge Diameter, in. | Cast 1.0 |
| ··· · | Density, gm/cc | 1.0 |
| Yolatility: | Rate, meters/second | 8643 |

| Booster Sensitivity Test: | | Decomposition Equation: |
|---|-------------------|--|
| Condition | | Oxygen, atoms/sec (Z/sec) |
| Tetryl, gm | | Heat, kilocalorie/ mole |
| Wox, in. for 50% Detonation | | (AH, kcal/mol) |
| Wax, gm | | Temperature Range, °C |
| Density, gm/cc | | Phase |
| | | |
| Heat of: | | Armor Plate Impact Test: |
| Combustion, cal/gm | 2676 | |
| Explosion, cal/gm | 1131 | 60 mm Mortar Projectile: |
| Gas Volume , cc/gm | 830 | 50% Inert, Velocity, ft/sec |
| Formation, cal/gm | | Aluminum Fineness |
| Fusion, cal/gm | 29.4* | |
| *Calculated for 76.9% HMX, 23.1% Th | NT. | 500-Ib General Purpose Bombs: |
| Specific Heat: cal/gm/°C | ** | |
| Specific Heat: cal/gm/°C -79°C -80° to +80°C 22° to 74°C | 0.200 | Plate Thickness, inches |
| -80° to +80°C 33° to 74°C | $0.240 \\ 0.245$ | |
| 90° to 150°C | 0.243 | 1 |
| **Determined for 76.9% HMX, 23.1% | | 11/4 |
| | | 11/2 |
| | | 134 |
| Burning Rate: | | |
| cm/sec | | Bomb Drop Test: |
| | | |
| Thermal Conductivity: | | T7, 2000-Ib Semi-Armor-Piercing Bomb ₩ Concrete: |
| cal/sec/cm/"C | | |
| | | Max Safe Drop, ft |
| Coefficient of Expansion: Linear, %/°C | | |
| | | 500-Ib General Purpose Bomb vs Concrete: |
| Volume, %/°C | | Height, ft |
| | | Trials |
| Hardness, Mohs' Scale: | | Unaffected |
| | | Low Order |
| Young's Modulus: | | High Order |
| E , dynes/cm² | | |
| E, Ib/inch ² | | 1000-ib General Purpose Bomb vs Concrete: |
| Density, gm/cc | | |
| | n oluc | Height, ft |
| Compressive Strength: Ib/inch ² | 1340 See below | Trials |
| | See Delow | Unaffected |
| Vapor Pressure: | | Low Order |
| "C mm Mercury | | High Order |
| Compressive Strength: 1b/inch ² | *** | |
| Average (10 tests) | 1340 | Ultimate Deformation: % |
| High | 1560 | Average (10 tests) 2.43 |
| Low | 1040 | High 2.89 Low 2.04 |
| *************************************** | | |

***Test specimen 1/2" x 1/2" cylinder (approximately 3 gm) pressed at 3 tons (6,000 1b) total load or 30,000 psi with a 2 minute time of dwell.

Octol, 75/25

| Fragmentation lest: | Shaped Charge Effectiveness, $TNT = 100$: | |
|--|---|---------------------|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | |
| Total No. of Fragments: For TNT | Color: | Buff |
| For Subject HE | Principal Uses: HE projectile and bomb | filler |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: | Cast |
| | Loading Density: gm/cc | 1.81 |
| Fragment Velocity: ft/sec At 9 ft A t 25½ ft | Storage: | |
| Density, gm/cc | Method | Dry |
| Blast (Relative to TNT): | Hazard Closs (Quantity-Distance) | Class 9 |
| Air: Peak Pressure Impulse | Compatibility Group Exudation | Group I |
| Energy Air, Confined: Impulse | Work to Produce Rupture: ft-lb/inch ³ Average (10 tests) | * 1.31 |
| Under Water: Peak Pressure Impulse Energy | High Low Efflux Viscosity, Saybolt Seconds: | 1.57 1.07 9.0 |
| Underground: Peak Pressure Impulse | | |
| Energy | *Test specimen 1/2" x 1/2" cylinder (a mately 3 gm) pressed at 3 tons (6,000 total load or 30,000 psi with a 2 mi time of dwell. |) lb) |
| | mately 3 gm) pressed at 3 tons (6,000 total load or 30,000 psi with a 2 mi |) lb) |

Fragment Velocity Test: M26 Hand Grenade:

| Compositio 75/25 Cyc 75/25 Octo | lotol | 4948 4908 5124 | |
|---------------------------------------|-------|----------------------|--|

(a)

| Modulus of Elasticity:* | c |
|-------------------------|----------------------|
| | lb/inch ^c |
| Average (10 tests) | 62,100 |
| High | 75,900 45,200 |
| LOW | 45,200 |

*Test specimen 1/2" x 1/2" cylinder (approximately 3 gm) pressed at 3 tons (6,000 lb) total load or 30,000 psi with a 2 minute time of dwell.

| | 1 |
|----------------------|------------------|
| Weight Group, grains | No. of Fragments |
| 1/2 - 2 | 1611 |
| 2 - 5 | 777 |
| 5 - 10 | 535 |
| 10 - 25 | 719 |
| 25 - 50 | 480 |
| 50 - 75 | 246 i |
| 75 - 150 | 339 |
| | 1 |

Octol, 70/30; Octol, 75/25

Preparation: 🔭

Water-wet HMX is added slowly to molten TNT in a steam-jacketed kettle at a temperature of 100° C. The mixture is heated and stirred until all moisture is evaporated. The composition is cooled to a satisfactory pouring temperature and cast directly into ammunition components or prepared in the form of chips to be stored for later use.

References: 52

(a) 1st Indorsement from Chief, Explosives Development Section, to Chief, Explosives Research Section, Picatinny Arsenal, dated 12 May 1958. Subject: "Properties of Octols and HTA-3."

(b) A. W. O'Brien, Jr., C. W. Plummer, R. P. Woodburn and V. Philipchuk, Detonation Velocity Determinations and Fragment Velocity Determinations of Varied Explosive Systems and Conditions, National Northern Corporation Final Summary Report NNC-F-13, February 1958 (Contract DAI-19-020-501-ORD-(P)-58).

* 58 word Standard Operating Procedure.

⁵²See footnote 1, psge 10.

| Composition: | | Molecular Weight: | 245 | | | |
|---|-----------------------------|---|------------|--|--|--|
| % RDX | 90 | Oxygen Balance: CO, % CO % | -62 -18 | | | |
| Polystyrene (unmodified) | 8.5 | | 0.81 | | | |
| Dioc ^t ylphthalate | 1.5 | Density: gm/cc Unpressed Pellet pressed at 30,000 psi Melting Point: "C | 1.6? | | | |
| C/H Ratio | | Freezing Point: "C | | | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | Unpressed 28 15 20 | Boiling Point: "C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ Vacuum Stability Test: | | | | |
| Friction Pendulum lest: Steel Shoe Fiber Shoe | Unaffected Unaffected | Vacuum Stability Test: cc/40 Hrs, at 90°C | *- | | | |
| Rifle Bullet Impact lest: 10 Trials | . | - 100°C 120°C | 0.41 | | | |
| %Explosions10Partic Is90 | | 135°C 150°C | | | | |
| Burned O Unaffected O | | 200 Gram Bomb Sand Test: Sand, gm | | | | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Smokes 275 10 15 | | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide TetryI Ballistic Mortar, % TNT: | | | | |
| 20 | | | | | | |
| 75"C International Heat lest: % Loss in 48 Hrs | | Trauzl Test, % TNT: Plate Dent lest: Method | | | | |
| 100°C Heat lest: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | 0.00 0.00 None | Condition Confined Density, gm/cc Brisance, % TNT | | | | |
| Flammability Index: | | Detonation Rate: Confinement | | | | |
| Hygroscopicity: % | | Condition Charge Diameter, in. | | | | |
| * Test procedure described in May 1956. | n PATR No. 2247, | Density, gm/cc Rate, meters/second | | | | |

| Booster Sensitivity Test: | | Decomposition Equation: |
|--|--------------------|---|
| | | Oxygen, otoms/sec (Z/sec) |
| Tetryl, gm | | Heat, kilocolorie/mole |
| Wax, in. for 50% Detonation | | (AH, kcal/mol) |
| Wax, gm | | Temperature Range, °C |
| Density, gm/cc | | Phase |
| Heat of: | | Armor Plate Impact Test: |
| Combustion, cal/gm | 3027 | |
| Explosion, cal/gm | 983 | 60 mm Mortar Projectile: |
| Gas Volume, cc/gm | | 50% Inert, Velocity, ft/sec |
| Formation, col/gm | | Aluminum Fineness |
| Fusion, col/gm | | 500 th Osmani Durness Benches |
| Specific Heat: col/gm/°C | | 500-lb General Purpose Bombs: |
| | | Plate Thickness, inches |
| | | 1 |
| | | 11/4 |
| | | 11/2 |
| | | 134 |
| Burning Rate: | | |
| cm/sec | | Bomb Drop Test: |
| Thermal Conductivity: col/sec/cm/"C | | T7, 2000-lb Semi-Armor-Piercing Bomb vs Concrete: |
| | | |
| Coefficient of Expansion: | | Max Safe Drop, ft |
| Linear, %/°C | | 500-Ib General Purpose Bomb vs Concrete: |
| Volume, %/°C | | Height, ft |
| | | Trials |
| Hardness, Mohs' Scale: | | Unaffected |
| | | Low Order |
| • | See below | High Order |
| E, dynes/cm ² | | |
| E, lb/inch ² | | 1000-lb General Purpose Bomb vs Concrete: |
| Density, gm/cc | | |
| | | Height, ft |
| Compressive Strength: Ib/inch ² 240 Percent 8. |)3 2149 9 13,1 | Trials |
| Percent 8. | 7 13,1 | Unaffected |
| Vapor Pressure: | | Low Order |
| "C mm Mercury | | High Order |
| | <u>Femperature</u> | |
| E, lb/inch ² (avg of 5) Ambier 39,955 | | |

*Pellets (Lot OAC-596-55) 0.750 inch diameter by 0.750 inch long, pressed at 30,000 psi with 30-second dwell.

| Fragmentation Test: | Shaped Charge Effectiveness, TNT | = 100: |
|--|--|---------------------------|
| 90 mm HE, M71 Projectile, Lot WC-91: | Glass Cones St | teel Cones |
| Density, gm/cc | Hole Volume | |
| Charge Wt, Ib | Hole Depth | |
| Total No. of Fragments: | Color: | White |
| For TNT | | |
| For Subject HE | Principal Uses: High mechanic | al strength |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | explosive | |
| Density, gm/cc | | |
| Charge Wt, Ib | | |
| Total No. of Fragments: | Method of Loading: | Pressec |
| ForTNT | | |
| For Subject HE | | J, v 10J |
| | Loading Density: gm/cc Presse 0 10 20 30 | d, psi x 10 ⁵ |
| Fragment Velocity: ft/sec | 1.10 1.49 1.59 1.6 | |
| At 9 ft At 25½ ft | Storage: | |
| Density, gm/cc | Method | Dry |
| | Hazard Class (Quantity-Distance | e) Class |
| Blast (Relative to TNT): | | |
| Air: | Compatibility Group | Group |
| Peak Pressure | | None |
| Impulse | Exudation | INDITE |
| Energy | | <u>.</u> |
| Air Confined. | Rockwell Hardness, "R" Sc | |
| Air, Confined: Impulse | 1/2 inch diameter Penetra | tor, 60 Kg Load: |
| | Pellet Specific | |
| Under Water: | No.* Gravity | Hardness |
| Peak Pressure Impulse | 1.624 | 84 |
| Energy | 2 1.623 | 90 |
| Livigy | 3 1.611 4 1.600 | 84 80 |
| Underground: | 5 1,590 | 75 |
| Peak Pressure | 6 1.571 7 1.548 | 73 62 |
| Impuls e | 8 1.524 | 49 |
| Energy | | |
| | *Pellets (Lot HOL-E-93) we in diameter and 3/4 inch b | ere 1-1/2 inches high. |
| | | |

| o Initia | lion by . | Type 11 | Special I | Blasting | Caps | (a) |
|----------------|---|---|---|--|--|---|
| Gap , 0.250 | (Distan <u>ce</u> 0.300 | E From B 0.350 | asc of C 0.400 | ap to Pe 0.450 | 11et), In 0.500 | nches 0.750 |
| | | | | | | |
| 1 | 8 | 5 | 6 | 2 | 1 | 1 |
| 0.082 | 0.090 | 0.087 | 0.080 | 0.080 | | |
| 0 | 1 | 3 | 4 | 1 | 1 | 1 |
| | | | | | | |
| 3 | 8 | 9 | 4 | 3 | 5 | 2 |
| 0.090 | 0.089 | 0.087 | 0.084 | 0.087 | 0.075 | |
| 0 | 0 | 2 | 3 | 2 | 3 | 2 |
| | | | | | | |
| 5 | 3 | 5 | 5 | 5 | 5 | 5 |
| 0.109 | 0.096 | 0.095 | 0.09 2 | 0.097 | 0.087 | |
| | | | | | | |
| | Gap . 0.250 . 1 0.082 0 . 3 0.090 0 . 5 | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | Gap (Distance From Base of C 0.250 0.300 0.350 0.400 1 8 5 6 0.082 0.090 0.087 0.080 0 1 3 4 3 8 9 4 0.090 0.089 0.087 0.084 0 0 2 3 5 3 5 5 | Gap (Distance From Base of Cap to Pe 0.250 0.300 0.350 0.400 0.450 1 8 5 6 2 0.082 0.090 0.087 0.080 0.080 0 1 3 4 1 3 8 9 4 3 0.090 0.089 0.087 0.084 0.087 0 2 3 2 3 2 5 3 5 5 5 | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ |

| Sensitivity of I | B-RDX and | 98/2 1 | RDX/Stearic | Acid |
|----------------------|------------|--------|--------------|-----------|
| Pellets* to Initiati | on by Type | e II S | pecial Blast | ting Caps |

** Mild steel plate 5" x 5" x 1".

Performance of PB-RDX as Booster: (b, d)

Ten 2.75 inch HEAT ML Rocket Heads were unaffected in performance by storage at 71° C for 28 days. Thus, PB-RDX was not desensitized by contact with TNT-bearing explosives. Tetryl, similarly used, becomes desensitized when stored in bursting charges at elevated temperatures.

In addition, 108 modified M307Al 57 mm projectiles were fired for performance against armor. Each round contained a PB-RDX booster pellet. There was no evidence in these firings that the projectiles were inadequately boostered.

Preparation:

The purchase description sheet for polystyrene-bonded RDX (X-PA-PD-1088, 25 October 1956) requires that the PB-RDX shall be a mixture of RDX, coated and surrounded by a homogeneous mixture of polystyrene and dioctylphthalate. The specified percentage of RDX shall consist of a mixture of 757% Type B, Class A RDX and 25% Type B, Class E RDX. The granulation of the unpressed composition shall be as follows:

| Through U. S. Standard Sieve No. | · · · · | Minimum % | Maximum 🖇 | r 2 |
|-------------------------------------|---------|-----------|-----------|--------|
| 6 | | 100 | | |
| 12 | | 60 | | |
| 20 | | | 2 | 1 |
| ২ন | | | 0 | |

Two methods have been reported for the preparation of PB-RDX (Reference: L o Alamos Scientific Laboratory, Contract W-7405-Eng 36 with U.S. Atomic Energy Commission, Report No. IA-1448). The earlier method employed a Baker-Perkins type mixer to blend the components. This procedure gave a product with good pressing characteristics. However, the molding composition was nonuniform in granulation and tended to be dusty. The slurry method of PB-RDX preparation gave a product which was uniform, free-flowing and dustless. In addition, PB-RDX granulated by the slurry method exhibited satisfactory drying, handling and pressing characteristics.

The final procedure incorporating the better features found from the study of such variables as solvents, solvent/plastic ratios, lacquer addition and temperature, agitation, RDX particle size distribution, dispersants and rosin additive, was as follows (Reference c):

Forty-two and five-tenths grams (42.5 gm) of polystyrene and 8 cc dioctylphthalate were dissolved in 200 cc toluene in a lacquer dissolver. Steam was introduced into the jacket until the temperature reached 65° C. The lacquer was agitated constantly until it was ready to be added to the granulator. This lacquer contained a 1:4 ratio of plastic-plasticizer to toluene.

Four hundred and fifty grams (450 gm) of RDX and 4500 grams of H_2O (ratio 1:10) were added to the granulator. The agitator was set for 400 rpm and the temperature was raised to 75°C by introducing steam into the jacket. The temperature differential between the lacquer solution and the RDX/water slurry was 5° to 10°C.

The lacquer solution was poured through the charging funnel into the granulator. As soon as the lacquer was added, a solution of gelatin in water was added, and the mixture was agitated until the lacquer was well dispersed in the RDX slurry (approximately 5 minutes). Granulation took place at this point. Steam was introduced again into the jacket to distill the solvent until the temperature reached 98° C. Cooling water was then run into the jacket to cool the batch to 40° C. The coated material from the granulator was collected on a Buchner funnel and dried in a tray at 70° C for 24 hours. Temperatures below 70° C did not furnish enough heat, but a temperature of 80° C produced stickiness and caking of PB-RDX.

Origin:

An explosive consisting of RDX coated with polystyrene plasticized with dioctyphthalate was initially developed in 1952 for the Atomic Energy Commission by Los Alamos Scientific Laboratory of the University of California (Contract W-7405-Eng 36 with U. S. Atomic Energy

Commission, Report No. LA-1448). The specific formulation of 90/8.5/1.5 RDX/polystyrene/ dioctylphthalate was subsequently standardized by Los Alamos. This explosive, originally designated PBX, has been redesignated PB-RDX. The detailed requirements for the present polystyrene-bonded RDX(PB-RDX) are given in purchase description X-PA-PD-1088, 25 October 1956.

References: 53

(a) B. J. Zlotucha, T. W. Stevens and C. E. Jacobson, <u>Characteristics of Polystyrene-Bonded RDX(PB-RDX)</u>, PAIR No. 2497, April 1958.

(b) A. J. Pascazio, The Suitability of a Bare PBX Booster Pellet in the 2.75 Inch M1 HEAT Rocket Head, PAIR No. 2271, November 1955.

(c) J. L. Vermillion and R. C. Dubberly, Plastic-Bonded RDX, Its Preparation by the Slurry Method, Holston Defense Corporation, Control No. 20-T-16 Series A (PAC 1081), 5 March 1953.

(d) C. J. Eichinger, <u>Report on Cartridge HEAT 57 mm M307A1</u> (Mod) with Modified Copper Liner, Aberdeen Proving Ground, Development and Proof Services, First Report on OC Project TA3-5204, October 1957.

⁵³See footnote 1, page 10.

| Composition: | Molecular Weight: $(C5^{H}9^{N}3^{O}10)$ | 271 |
|---|---|------------------|
| % с 22.1 н 3.3 | Oxygen Balance: CO₂ % CO % | -27 3 |
| $\begin{bmatrix} 1 & 3 & 5 \\ & & \text{HOCH}_2 & & C \\ N & 15.5 \end{bmatrix} = \begin{bmatrix} 1 & -CH_2 & 0NO_2 \\ & & & \text{CH}_2 & 0NO_2 \end{bmatrix}$ | Density: gm/cc | 1.54 |
| CH ₂ ONO ₂ | Melting Point: "C | 26 to 28 |
| C/H Ratio 0.141 | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 5 to 10 Sample Wt, mg 38 | Boiling Point: "C 4 mm <i>Hg</i> Decompos Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^S ₃₀ | es 130 |
| Friction Pendulum Test: Steel Shoe Fiber Shoe Rifle Bullet Impact Test: Trials | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C 120°C | 2.54 to 5.ගි |
| % Explosions Partials | 135°C 150°C | |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm | |
| Explosion Temperature: [°] C Seconds, 0.1 (no cap used) 1 5 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl | |
| 15 20 | Ballistic Mortar, % TNT: | |
| | Trauri Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method | |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement | |
| Hygroscopicity: % | Condition Charge Diameter, in. | |
| Volatility: | Density, gm/cc Rate, meters/second | |

| Fragmentation Test: | Shaped Charge Effectiveness, TNT = 100: |
|---|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: White |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Explosive, propellant or igniter ingredient |
| Total No. of Fragments : For TNT For Subject HE | Method of Loading: |
| | Loading Density: gm/cc |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc | Storage: Method Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation None |
| Air, Confined: Impulse | PETRIN esters are listed in reference (b) and most of these esters have been shown to have explosive properties. |
| Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy <u>Absolute Viscosity, poises:</u> Temp, 17° C 14.8 23° C 4.8 28° C 3.0 38° C 1.2 | An infrared spectrophotometric procedure was developed for the determination of the acetone content of PETRIN (ref c). A 2.5 gm sample of PETRIN is dissolved in chloroform and the volume increased to 25 milliliters in a volumetric flask. The acetone content of the PETRIN solution is determined by its infra red absorption at 5.82μ in a 0.5 mm cell. A double beam method is used with a reference cell containing chloroform and acetone-free PETRIN. The quantity of the latter must be carefully adjusted to give a good balance be- tween the test sample and reference cells for the strong PETRIN peak at 6.02μ maximum. Heat of: |
| | Explosion, cal/gm 1204 |

Preparation:

| с(сн ₂ он) ₄ + | 3HNO 3 | H ₂ SO ₄ | ohch ₂ c(ch ₂ no ₃) ₃ | + | 3н ₂ 0 |
|--------------------------------------|---------------|--------------------------------|--|---|-------------------|
| pentaerythritol | nitric | sulfuric | pentaerythritol | | water |
| MW 136 | acid MW 63 | acid _{MW} 98 | trinitrate MW 271 | | MW 18 |

The earliest procedure used for the manufacture of PETRIN was that developed at Alleghany Ballistics Laboratory. In this process, called the "A process," 80% HNO₃ and the solid pentaerythritol were charged to the reactor and 80% H₂SO₄ was added slowly at a rate to permit control of temperature at 0° to 5°C. This mixture was held for a 2-1/2-hour reaction period, then drowned in water and filtered to give a cake containing both the tri- and tetra-nitrates of pentaerythritol. The cake was dissolved in acetone and neutralized in solution with ammonium carbonate, after which the PETN was precipitated by the addition of water. After filtration, the PETRIN was recovered from the filtrate by stripping off the solvent under vacuum. Yields by this process averaged about 40%.

An improved process, called the "B process," used the same primary reaction procedure but a different work-up procedure. After the reaction holding period, water was added to dilute the mixed acid and the batch was extracted in situ with methylene chloride. The organic layer was separated, neutralized with aqueous sodium bicarbonate, and stripped of methylene chloride under vacuum to yield the product directly. Yields by this process were about 50% and quality of the product was much improved over that of the "A process."

The "C process," currently in use, involves essentially the simultaneous synthesis and extraction of PETRIN from the reaction mixture. Methylene chloride approximately equal to the total weight of the other components is added to the reaction mixture before the sulfuric acid. After a suitable time following the addition of sulfuric acid, the solvent is removed and replaced by fresh solvent one or more times. The combined extracts are neutralized and concentrated. Because of their initially relatively large volume, PEIN must be removed by filtration from the concentrated PETRIN solution before the final solvent is stripped. Yields by this process have been 60% to 65%.

Origin:

The nitration products of pentaerythritol or its derivatives containing not more than three NO_2 groups were patented for use as explosives, propellants or ignition materials in 1936 (German Patents 638,432 and 638,433; CA 31, 1212 (1937)).

A process in which pentaerythritol monoacetate was converted to pentaerythritol trinitrate monoacetate, which was then saponified under carefully controlled conditions to PETRIN, was reported in 1954 (N. S. Marans, D. E. Elrick and R. F. Preckel, J Am Chem Soc <u>76</u>, 1304). PETRIN was also prepared by the nitration of pentaerythritol with a mixture of <u>80%</u> HNO₃ and <u>80%</u> H₂SO₄ in 1955 (A. T. Camp, N. S. Marans, D. E. Elrick and R. F. Preckel, J Am Chem Soc <u>72</u>, 751).

References:54

(a) Rohm and Haas Company, Redstone Arsenal Division, Process for the Manufacture of Pentaerythritol Trinitrate Monoacrylate and Petrin Acrylate Propellants, 12 March 1956.

(b) E. Berlow, R. H. Barth and J. E. Snow, <u>The Pentaerythritols</u>, ACS Monograph No. 136, p. 65, Reinhold Publishing Corporation, New York, 1958.

(c) R. H. Pierson, An Infrared Spectrophotometric Method for Determination of Acetone <u>Content of Pentaerythritoltrinitrate</u>, U.S. Naval Ordnance Test Station Report NOTS 1877, NAVORD Report No. 5649, 3 February 1958.

⁵⁴See footnote 1, page 10.

| Composition % | Molecular Weight: (C8H11N3O11) 325 (Monomer) 325 | | | | | |
|--|--|--|--|--|--|--|
| с 29.5 н 3.4 сн ₂ оло ₂ | Oxygen Balance: -54 CO, % -12 | | | | | |
| $CH_2 = CH - CO_2 CH_2 C - CH_2 ONO_2$ N 12.9 | Density: gm/cc | | | | | |
| о 54.2 ^{СН₂ОNO₂} | Melting Point: "C 78 to 79 | | | | | |
| C/H Ratio 0.239 | Freezing Point: "C | | | | | |
| Impact Sensitivity, 2 Kg Wt: | Boiling Point: "C | | | | | |
| Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | Refractive Index, n_{20}^D n_{25}^D n_{30}^D | | | | | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C | | | | | |
| Rifle Bullet Impact Test: Trials % Explosions Partials Burned Unaffected | 120°C 135°C 150°C 200 Gram Bomb Sand Test: Sand, gm | | | | | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 10 15 20 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl Ballistic Mortar, % TNT: | | | | | |
| 75°C International Heat Test: | Trauzi Test, % TNT: | | | | | |
| % Loss in 48 Hrs 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Plate Dent Test: Method Condition Confined Density, gm/cc Brisance, % TNT | | | | | |
| Flammability Index: | Detonation Rate: Confinement | | | | | |
| Hygroscopicity: % Ni 1 | Condition Charge Diameter, in. | | | | | |
| Volatility: | Density, gm/cc Rate, meters/second | | | | | |

Pentaerythritol Trinitroacrylate (PETRIN Acrylate)

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT=$ 100: | | | |
|---|---|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | | | |
| Total №. of Frogments: For TNT | Color: White | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, lb Total No. of Fragments: | Principal Uses: Ingredient of composite rocket propellants | | | |
| For TNT For Subject HE | Method of Loading: | | | |
| Fragment Velocity: ft/sec | Loading Density: gm/cc | | | |
| At 9 ft At 25½ ft Density, gm/cc | Storage: Method Dry at temperatures below melting point | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation None | | | |
| Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | Heat of: Combustion, cal/gm 2923 Explosion, cal/gm 791 | | | |

| | Pre | parat | ion: |
|--|-----|-------|------|
|--|-----|-------|------|

| HOCH2C(CH2NO3)3 | + (| CH ₂ = CHC | :0Cl + | C6H | 5N(CH ₃) ₂ |
|--|-------------------|--------------------------------|------------------------------------|--------|-----------------------------------|
| pentaerythritol trinitrate (PETRIN) MW 271 0 | | acrylyl chloride MW 90.5 | ; | an | ethyl iline 121 |
| (02NOCH2)3CCH2OCCH | = CH ₂ | + | с _б н ₅ м(сн | 3)2HCl | |

(a)

pentaerythritol trinitrate monoacrylate (PETRIN acrylate)

dimethylanine

MW 325

hydrochloride

The original synthesis for PETRIN acrylate employed trifluoroacetic anhydride and glacial acrylic acid as the acrylation agent for PETRIN. These two materials were charged to a reaction vessel and the initial reaction was controlled by the slow addition of PETRIN at a temperature of 10° to 15°C. Following a period of one hour, the batch was drowned in water, precipitating the PETRIN acrylate. This solid was separated by filtration, dissolved in chlo-roform, and neutralized in solution with sodium bicarbonate. The product was then crystallized during a period of 16 hours at 0° C and dried under vacuum to remove traces of solvent. The yield for this process was about 60%.

A significant improvement in yield (to about 74%) and purity (approximately 98%) was realized by the substitution of methanol for chloroform and crystallization of the product from the solution without neutralization, residual acid being removed by washing the filter cake with water.

Because of the high cost and hygroscopic nature of trifluoroacetic anhydride, a new process, based on dimethylaniline and acrylyl chloride, was considered. This process is currently under development in the Rohm and Haas Chemical Processing facilities and is not considered optimum. Yields averaged 46% and product purities averaged 93.5%.

PETRIN Acrylate Propellants:

PETRIN acrylate could be used as a monopropellant because it has a specific impulse of 214 lb-sec/lb and a burning rate of 0.2 in/sec. The addition of an oxidizer increases both the impulse and burning rate.

A composition which presently appears most promising is as follows:

| | Composition M |
|-----------------------------------|----------------------------------|
| PETRIN acrylate (> 97% purity), % | 34.3 (binder) |
| Triethylene glycol trinitrate, 🐐 | 11.8 (plasticizer) |
| Glycol diacrylate, 🖇 | 2.9 (crosslinker) |
| Ammonium perchlorate, % | 51.0 (oxidizer) |
| Hydroquinone, % | 0.014 (polymerization inhibitor) |

Measured specific impulse 238 lb-sec/lb, at density of 1.3.

Reference:55

(a) Rohm and Haas Company, Redstone Arsenal Division, Process for the Manufacture of Pentaerythritol Tetranitrate Monoacrylate and Petrin Acrylate Propellants, 12 March 1956.

55See footnote 1, page 10.

| Composition: | | Molecular Weight: | 50/50 265 | 10/90 234 |
|--|-----------------------------|--|----------------|----------------|
| PEIN 50 | 10 90 | Oxygen Balance: CO, % CO % | -42 - 5 | -68 -21 |
| TNT 50 | <i>,</i> , | Density: gm/cc | 1.65 | 1.60 |
| | | Melting Point: "C | | 76 |
| C/H Ratio | | Freezing Point: "C | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | <u>50/50 10/90</u> 34 65 | Boiling Point: °C | | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 12 14 15 18 | Refractive Index, n_{20}^{D} n_{25}^{D} n_{30}^{D} | | |
| Friction Pendulum Test: | | Vacuum Stability Test: | 50/50 | 10/90 |
| Steel Shoe Fiber Shoe | Unaffected Unaffected | cc/40 Hrs, at 90°C | <u>yo</u> , yo | 20, 90 |
| Rifle Bullet Impact Test: 25 Trials, | 50/50 | 100°C | 3.0 | 3.0 |
| % | | 120°C | 11+ | 11+ |
| Explosions 72 | | 135°C | | |
| Partials 20 | | 150°C | | |
| Burned 0 | | 200 Gram Bomb Sand Test | | |
| Unaffected 8 | | Sand, gm | 55.6 | 49.5 |
| Explosion Temperature: °C, Seconds, 0.1 (no cap used) 290 | 50/50 | Sensitivity to Initiation: Minimum Detonating C | harge, gm | 50/50 |
| 1 266 5 Decomposes 220 | | Mercury Fulminate Lead Azide | | 0.19* 0.13* |
| 10 204 | | | | - |
| 15 197 | | Tetryl *Alternative initiati | ng charges. | |
| 20 >190 | | Ballistic Mortar, % TNT: | (a) | 126 |
| 75°C International Heat Test: | | Trauzl Test, % TNT: | (b) | 122 |
| % Loss in 48 Hrs | | Plate Dent Test: Method | (c) | В |
| 100°C Heat Test: | 50/50 | Condition | | Cast |
| % Loss, 1st 48 Hrs | 0.0 | Confined | | No |
| % Loss, 2nd 48 Hrs | 0.2 | Density, gm/cc | | 1.66 |
| Explosion in 100 Hrs | None | Brisance, % TNT Detonation Rate: | | 121 |
| Flammability Index: Will not con | tinue to burn | Confinement | | None |
| | | Condition | | Cast |
| Hygroscopicity: % 30°C, 90% RH | | Charge Diameter, in, | | 1.0 |
| Voletility: | | Density, gm/cc | | 1.66 |
| - | | Rate, meters/second | | 7465 |

Pentolite, 50/50; 10/90

| Booster Sensitivity Test: (d) Condition Pressed Tetryl, gm 100 Wax, in. for 50% Detonation 2.36 Wax, gm Density, gm/cc 1.60 | 50/50 Cast 100 2.08 1.65 | Decomposition Equation: Oxygen, otoms/sec (Z/sec) Heat, kilocolorie/mole (AH, kcol/mol) Temperature Range, °C Phase | |
|---|--------------------------------------|---|---------------------|
| Heat of: Combustion, col/gm Explosion, col/gm Gas Volume, cc/gm Formation, col/gm Fusion, col/gm Specific Heat: col/gm/°C | 1220 | Armor Plate Impact Test: 60 mm Mortar Projectile: 50% Inert, Velocity, ft/sec Aluminum Fineness 500-Ib General Purpose Bombs: Plate Thickness, inches 1 31/4 | <u>50/50</u> 170 |
| Burning Rate: cm/sec | | 1 %4 1 <u>1 %4</u> | |
| Thermal Conductivity: col/sec/cm/"C | | Bomb Drop Test: T7, 2000-1b Semi-Armor-Piercing Bom | nb vs Concrete: |
| Coefficient of Expansion: Linear, %/°C | | Max Safe Drop, ft 500-Ib General Purpose Bomb vs Con | crete: |
| Volume, %/°C | | Height, ft Trials | |
| Hardness, Mohs' Scale: | | Unaffected Low Order | |
| Young's Modulus: E', dynes/cm² | | High Order | |
| E, Ib/inch ² Density, gm/cc | | 1000-Ib General Purpose Bomb vs Con | crete: |
| Compressive Strength: Ib/inch ² 200 Density, gm/cc Vapor Pressure: °C mm Mercury | 1.68 | Height, ft Trials Unaffected Low Order High Order | |
| | | | |

| Fragmentation Test: | 50/50 | Shaped Charge Effectiveness, TNT = 100: 50/50 10/90 50/50 25/75 |
|--|--------------|--|
| 90 mm HE, M71 Projectile, Lot WC-91: | | Glass Cones(f) Steel Cones (g) |
| Density, gm/cc | 1.65 | Hole Volume 157 105 149 119 |
| Charge Wt, Ib | 2.147 | Hole Depth 116 116 131 119 |
| Total No. of Fragments: | | Color: Yellow-white |
| For TNT | 703 | |
| For Subject HE | 968 | Principal Uses: Shaped charges, bursting |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | | charges, demolition blocks |
| Density, gm/cc | 1.65 | |
| Charge Wt, Ib | 0.872 | |
| Total No. of Fragments: | | Method of Loading: Cast |
| ForTNT | 514 | |
| For Subject HE | 650 | Loading Density: gm/cc 5 0/50 1 0/90 |
| FragmentVelocity: ft/sec | | 1.65 1.60 |
| At 9 ft At 25 ½ ft | 2810 2580 | Storage: |
| Density, gm/cc | 1.66 | Method |
| Blast (Relative to TNT): | (e) | Hazard Class (Quantity-Distance) $Class 9$ |
| Air: | | Compatibility Group Group I |
| Peak Pressure | 105 | |
| Impulse | 107 | Exudation |
| Energy | | |
| Air, Confined: Impulse | | <u>Compatibility with Metals:</u> <u>Dry:</u> Copper, brass, aluminum, magnesium, magnesium-aluminum alloy, mild steel coated |
| Under Water: Peak Pressure | | with acid-proof black paint, and mild steel plated with copper, cadmium or nickel are not affected. Zinc plated steel is only slightly |
| Impulse | | affected. |
| Energy | | Wet Stainless steel, aluminum and mild steel coated with acid-proof black paint are |
| Underground: Peak Pressure | | not affected. Copper, brass, magnesium, mag- nesium-aluminum alloy, mild steel and mild |
| Impulse | | steel plated with copper, cadmium, zinc or nickel are slightly affected. |
| Energy | | Effect of Temperature on (h) |
| Eutectic Temperature. ^o C: | 7 6 | Rate of Detonation: 50/50 |
| gn PEIN/100 gn INT 76°C 95°C | 13.0 28.3 | 16 hrs at, °C -54 ^{2-1,2-2} 21 Density, gm/cc 1.67 1.66 Rate, m/sec 7470 7440 |

Preparation:

Pentolite is manufactured by either the slurry method or coprecipitation of PEIN and TNT. In the slurry method PEIN, in water, is stirred and heated above 80° C. TNT is added and when molten, it coats the particles of PEIN. The slurry is cooled with rapid stirring and the separated granules are collected on a filter and dried below 75° C.

In coprecipitation, PEIN and TNT are dissolved separately in acetone. The solutions are mixed and the explosives are precipitated simultaneously by pouring the mixed solution into cold water under vigorous agitation. The precipitated solid is collected on a filter and dried in air.

Origin:

Standardized during World War 11, with the 50-50 PETN/INT mixture being the more important for bursting charges and booster-surround charges.

References :56

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III - Miscellaneous</u> <u>Sensitivity Tests</u>; Performance Tests, <u>OSRD Report No. 5746</u>, 27 December 1945.

(b) Philip C. Keenan and Dorothy Pipes, <u>Table of Military High Explosives</u>, Second Revision, NAVORD Report No. 87-46, 26 July 1946.

(c) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(d) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute, for</u> <u>Tetryl in Boosters</u>, NOL Memo 10, 303, 15 June 1949.

(e) W. R. Tomlinson, Jr., <u>Blast Effects of Bomb Explosives</u>, PA Tech Div Lecture, 9 April 1948.

(f) Eastern Laboratory, du Pont, Investigation of Cavity Effect, Sec 111, Variation of Cavity Effect with Explosive Composition. NDRC Contract W672-ORD-5723.

(g) Eastern Laboratory, du Pont, Investigation of Cavity Effect, Final Report, Contract W-672-ORD-5723, E. Lab, du Pont, 18 September 1943.

(h) W. F. McGarry and T. W. Stevens, Detonation Rates of the More Important Military Explosives at Several Different Temperatures, PAIR No. 2303, November 1956.

(i) Also see the following Picatinny Arsenal Technical Report on Pentolite:

| <u>o</u> | <u>1</u> | 2 | <u>3</u> | <u>4</u> | <u>5</u> | 6 | <u>7</u> | 8 |
|----------------------|----------------------|----------------------|------------------------------|--------------|----------|----------------------|----------------------|------------------------------|
| 1360 1420 1570 | 1291 1451 1651 | 1212 1262 1372 | 1133 1193 1213 1363 | 1284 2004 | 1325 | 1436 1466 1796 | 1477 1677 1737 | 1388 1598 1668 1838 |

⁵⁶See footnote 1, page 10.

| Composition: % | | Molecular Weight: $(C_5 H_8 N_4)$ | D ₁₂) 316 |
|---|---------------|---|-----------------------|
| C 19.0 0NO ₂ | | Oxygen Balance: | |
| н 5.2 сн5 | | 00, % | -10 15 |
| | | C0 % | 1) |
| N 17.7 $o_2^{NO-CH} = C - CH$ | 2 0102 | Density: gm/cc Cryst | ta 1 1,77 |
| 0 60.8 ^{CH} 2 | | Melting Point: °C | 141 |
| C/H Ratio 0,134 0N02 | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 17 6 16 | Boiling Point: °C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| Steel Shoe | Crackles | cc/40 Hrs, at | |
| Fiber Shoe | Jnaffected | 90°C | |
| Rifle Bullet Impact Test: 5 Trials * | | 100°C | 0.5 |
| When Bullet impact rest. 5 mais * | | 120°C | 11+ |
| Explosions 100 | | 135°C | |
| Partials 0 | | 150°C | |
| Burned 0 | | 200 Gram Bomb Sand Test: | |
| Unoffected 0 <u>*4.86% moisture in samples</u> | | Sand, gm | 62.7 |
| Explosion Temperature: "C | | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) 272 | | Minimum Detonating Charg | e, gm |
| 1 244 | | Mercury Fulminate | 0,17* |
| 5 Decomposes 225 | | Lead Azide | 0.03* |
| 10 211 | | Tetryl *Alternative initiating | ahargas |
| 15 | | • • • • | |
| 20 | | | a) 145 |
| 75°C International Heat lest: | | | b) 173 |
| % Loss in 48 Hrs | 0.02 | Plate Dent Test: (Method | c) A |
| 100°C Heat Test: | | Condition | Pressed |
| % Loss, 1st 48 Hrs | 0.1 | Confined | Yes |
| % Loss, 2nd 48 Hrs | 0.0 | Density, gm/cc | 1.50 |
| Explosion in 100 Hrs | None | Brisance, % TNT | 129 |
| Flammability Index: Will not contin | ue to burn | Detonation Rate: Confinement | None |
| Hygroscopicity: % 30 ⁰ C, 90% RH | 0.0 | Condition Charge Diameter, i n . | Pressed 1.00 |
| Volatility: | 0.0 | Density, gm/cc | 1.70 |
| ····••• · | | Rate, meters/second | 8300 |

PETN (Pentaerythritol Tetranitrate)

| Booster Sensitivity Test: | (c) | Decomposition Equation: (e) (e) (f) Oxygen, otoms/sec 10 ^{19.8} 10 ^{20.6} 10 ^{23.1} |
|--|---------|---|
| Condition | Pressed | Oxygen, otoms/sec 10 ¹⁹⁺⁸ 10 ²⁰⁺⁶ 10 ²³⁺¹ (Z/sec) |
| Tetryl, gm | 5 | Heat, kilocolorie/mole 47.0 50.9 52.3 |
| Wax, in. for 50% Detonation | | (AH kcol/mol) |
| Wax, gm | 3 | Temperature Range, °C 161-233 108-120 137-157 |
| Density, gm/cc | 1.6 | Phase Liquid Solid At mel ing poin |
| Heat of: Combustion, cal/gm | 1960 | Armor Plate Impact Test: |
| Explosion, col/gm | 1385 | |
| Gas Volume, cc/gm | 790 | 60 mm Mortar Projectile: 50% Inert, Velocity, ft/sec |
| Formation, col/gm | 383 | Aluminum Fineness |
| Fusion, col/gm | 0-5 | |
| Fusion, cut/gm | | 500-lb General Purpose Bombs: |
| Specific Heat: col/gm/°C | (d) | Plate Thickness, inches |
| Room Temperature | 0.26 | Plate Thickness, inches |
| | | 1 |
| | | 11/4 |
| | | 11/2 |
| | | 184 |
| Burning Rate: | | |
| cm/sec | | Bomb Drop Test: |
| Thermal Conductivity: cal/sec/cm/°C | | T7, 2000-lb Semi-Armor-Piercing Bomb vs Concrete: |
| Coefficient of Expansion: | | Max Safe Drop, ft |
| Linear, %/°C | | 500-lb General Purpose Bomb vs Concrete: |
| Volume, %/°C | | Height, ft |
| | | Trials |
| Hardness, Mohs' Scale: | 1.9 | Unaffected |
| Voursie Medulue | | Low Order |
| Young's Modulus: | | High Order |
| E, dynes/cm² E = b (inch² | | |
| E, b/inch ² | | 1000-lb General Purpose Bomb vs Concrete: |
| Density, gm/cc | | Height ft |
| Compressive Strength: lb/inch ² | | — Height, ft Trials |
| compressive energy in a more | | Unaffected |
| | | Low Order |
| Vapor Pressure: "C mm Mercury | | |
| | | High Order |
| | | |
| | | |

PETN (Pentaerythritol Tetranitrate)

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$ | : | | | | |
|--|---|----------------------|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm∕cc Charge Wt, Ib | Glass Cones Steel Co Hole Volume Hole Depth | nes | | | | |
| Total No. of Fragments: For TNT | Color: | White | | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: | Principal Uses: Class A - Detonating fuse and boosters | | | | | |
| Density, gm/cc Charge Wt, Ib | Class B - Priming compositions | | | | | |
| Total No. of Fragments: For TNT | Method of Loading: | | | | | |
| For Subject HE | Loading Density: gm/cc psi x 1 3 5 10 20 30 | 40 | | | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | 1.37 1.58 1.64 1.71 1.73 Storage: | 1.74 | | | | |
| Density, gm/cc | Method | Wet | | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 | | | | |
| Air: Peak Pressure Impulse | Compatibility Group Exudation | Group M (wet None | | | | |
| Energy | | | | | | |
| Air, Confined: Impulse | Bulk Modulus at Room Temperature (25°-30°C) : | (i) | | | | |
| Under Water: Peak Pressure | Dynes/cm ² x 10 ⁻¹⁰ Density, gm/cc | 4.60 1.77 | | | | |
| Impulse Energy | | | | | | |
| | | | | | | |
| Underground: Peak Pressure | | | | | | |
| Impulse Energy | | | | | | |
| | | | | | | |
| | | | | | | |
| | 1 | | | | | |

100

112

15.920

30.900

Compatibility with Metals:

Dry: Copper, brass, aluminum, magnesium, magnesium-aluminum alloy, stainless steel, mild steel, mild steel coated with acid-proof black paint and mild steel plated with copper, cad-mium, nickel or zinc are not affected.

Wet: Stainless steel is unaffected and aluminum only vary slightly so after prolonged storage. Copper, brass, magnesium, magnesium-aluminum alloy, mild steel, mild steel coated with acid-proof black paint and mild steel plated with cadmium, copper, nickel or zinc are affected.

Sensitivity of PEIN to electrostatic discharge, joules; Through 100 Mesh: (g)

| Unconfined | 0.06 |
|------------|------|
| Confined | 0.21 |

Solubility, grams of PETN per 100 grams (%) of: (h)

| | rethylene Icohol | Ac | etone | Be | enzene | <u>To</u> | luene |
|----------------------------|----------------------------------|---------------------|----------------------------------|---------------------|----------------------------------|----------------------------------|---|
| <u>°c</u> | <u>%</u> | <u>°</u> _ | <u>%</u> | <u>°</u> | % | o _C | of |
| 0 20 40 60 | 0.070 0.195 0.415 1.205 | 0 20 40 60 | 14.37 24.95 30.56 42.68 | 0 20 40 80 | 0.150 0.450 1.160 7.900 | 0 20 40 60 80 | 0.150 0.430 0.620 2.490 5.850 |

| Methyl acetate | | Eth | er | <u><i>B</i>-Ethoxy-ethyl-</u> <u>acetate</u> | | Chloro | Chlorobenzene | |
|----------------------|----------------------|-----------------|-------------------------|---|-----------------------------------|----------------------------|-----------------------------------|--|
| °c | Z | <u>oc</u> | K | °c | <u>%</u> | <u>oc</u> | % | |
| 20 30 40 50 | 13 17 22 31 | 0 20 34.7 | 0.200 0.340 0.450 | 20 30 40 50 60 | 1.5 4.1 7.6 11.2 14.2 | 20 30 40 50 60 | 0.35 2.8 6.1 9.2 12.2 | |

| Ethylenedichloride Methanol | | anol | Tetrachloroethane | | <u>Carbon</u> tetrachloride | | |
|-----------------------------|---------------------------|----------------|---------------------|-----------------------------|--------------------------------|----------------------|----------------------------------|
| <u>о</u> с | <u>%</u> | <u>°</u> | 4 | o _C | <u>%</u> | <u>o</u> c | % |
| 10 30 50 | 0.9 1.5 2 .6 | 20 40 60 | 0.46 1.15 2.6 | 20 30 40 50 | 0.18 0.27 0.40 0.58 | 20 30 40 50 | 0.096 0.108 0.118 0.121 |

PEIN (Pentaerythritol Tetranitrate)

| Iso | propanol | <u>Isobu</u> | tanol | Chlor | roform | , - | INT |
|----------------------------|---|--|--|--------------------|----------|--|--|
| o _c | <u>%</u> | <u>°с</u> | <u>%</u> | <u>°c</u> | <u>%</u> | °C | <u>%</u> |
| 15 20 30 40 50 | 0.02 0.0 ^{1,} 0.15 0.36 0.46 Eutetic of the s and 87% TNT at 7 | 20 30 40 50 system PET 76 ⁰ C. | 0.27 0.31 0.39 0.52 N-TNT is abo | 20 Dut 13% PETN | 0.09 | 80 85 90 95 100 105 110 115 120 125 | 19.3 25.0 32.1 39.5 48.6 58.2 70.0 87.8 115 161 |

Preparation:

(Nitroglycerin and Nitroglycerin Explosives, Naoum)

 $8\text{HCHO} + \text{CH}_3\text{CHO} + \text{Ca}(\text{OH})_2 \rightarrow 2\text{C}(\text{CH}_2\text{OH})_4 + \text{Ca}(\text{HCOO})_2 \text{ C}(\text{CH}_2\text{OH})_4 + 4\text{HNO}_3 \rightarrow \text{C}(\text{CH}_2\text{ONO}_2)_4 + 4\text{H}_2\text{O}$

1. In this preparation 1940 gm of formaldehyde and 600 gm of aceteldehyde are dissolved in 90 liters of water containing 1600 gm suspended slaked lime. The reaction is complete in about 3 weeks if agitated several times a day. The solution is filtered, the calcium formate precipitated with oxalic acid, filtered off, and the water removed under reduced pressure. On cooling the mother liquor about 1200 gm crude pentaery-thritol, melting point $235^{\circ}-240^{\circ}c$ are obtained. Purification is readily effected by stirring with a little alcohol, filtering and recrystallization from water.

2. To 400 cc of strong white nitric acid, are added 100 gm of pentaerythritol (through 50 mesh), at 5° C or below, under good agitation. After addition is complete stirring, at 5° C, is continued for 15 minutes. The mixture is drowned in 3 liters of ice-water, filtered, the product washed free of acid with water and then digested 1 hour in 1 liter of hot 0.5% sodium carbonate solution. The product is filtered, and recrystallized from acetone.

Origin:

PETN was known as an explosive in 1894 when it was proposed as an addition to smokeless powders to raise their flammability and ease of combustion (German Patent <u>81,664</u> (1894). Modern methods of preparation are described by Vignon and Gerin (Compt rend <u>133</u>, 590 (1901) and German Patent 265,025 (1912) and A. Stettbacher (Z ges Schiess - Sprengstoffw <u>11</u>, 112, 182 (1916) and <u>24</u>, 259 (1929)). PETN was not used on a practical basis until after World War I.

Destruction by Chemical Decomposition:

PETN is decomposed by dissolving in 8 times its weight of technical grade acetone and burning the solution in a shallow container. If preferred, warm the acetone solution to 40° C, stir and add 7 parts by weight, to each part of PETN, of a solution of 1 part sodium sulfide (Na₂S·9H₂O) in 2 parts water heated to 80°C. The aqueous solution should be added at such a rate that the acetone solution does not boil. After mixing is complete continue stirring for one-half hour. References :57

(a) L. C. Smith and E. G. Eyster, Physical Testing of Explosives, Part III - Miscellaneous Sensitivity Tests: Performance Tests, OSRD Report No. 5746, 27 December 1945.

- (b) Ph. Naoum, Z ges Schiess Sprengstoffw, pp. 181, 229, 267 (27 June 1932).
- (c) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.
- (d) International Critical Tables.

(e) M. A. Cook and M. T. Abegg, "Isothermal Decomposition of Explosives," University of Utah, <u>Ind & Eng Chem</u>, (June 1956), pp. 1090-1095.

(f) A. J. B. Robertson, "The Thermal Decomposition of Pentaerythritol Tetranitrate, Nitroglycerin, Ethylenediamine Dinitrate and Ammonium Nitrate," J Chem Ind <u>67</u>, 221 (1948).

(g) F. W. Brown, D. H. Kusler and F. C. Gibson, <u>Sensitivity of Explosives to Initiation</u> by Electrostatic Discharges, U.S. Dept of Int, Bureau of Mines, R1 3052, 1946.

(h) Various sources in the open literature.

(i) W. 5. Cramer, <u>Bulk Compressibility Data on Several High Explosives</u>, NAVORD Report No. 4380, 15 September 1956.

(i) Also see the following Picatinny Arsenal Technical Reports on PETN:

| <u>o</u> | 1 | <u>2</u> | <u>3</u> | <u>4</u> | <u>5</u> | 6 | <u>1</u> | <u>8</u> | 2 |
|---|--|--|--|-----------------------------|--|--|---|--|--------------------------------------|
| 760 1170 1260 1290 1300 1320 1360 1380 1390 1430 1450 1570 | 1041 1311 1381 1451 1561 1611 1651 | 772 922 1182 1192 1212 1262 1342 1352 1352 1372 1452 | 843 863 1063 1133 1253 1343 1493 1533 | 904 1274 1284 1414 | 1305 1325 1445 1705 1885 2125 | 1246 1276 1316 1376 1446 1456 1466 1556 1796 | 407 527 857 1247 1517 1617 1737 1797 | 318 838 1238 1318 1388 1568 1598 1838 2178 | 1379 1429 1489 1559 2179 |

57See footnote 1, page 10.

| Composition: | Molecular Weight: $(C_{6}H_{4}N_{4}O_{6})$ | 228 | | | |
|---|---|---------------------|--|--|--|
| $\begin{array}{c} \% \\ c & 31.5 \\ H & 1.8 \\ \end{array} \qquad \begin{array}{c} NH_2 \\ 0_2 N \\ \end{array} \qquad \begin{array}{c} NH_2 \\ NO_2 \end{array}$ | Oxygen Balance: CO, % CO % | -56 -14 | | | |
| N 24.5 | Density: gm/cc Crystal | 1.76 | | | |
| 0 42.2 NO ₂ | Melting Point: °C | 189 to 190 | | | |
| C/H Ratio 0.500 | Freezing Point: "C | | | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | Boiling Point: °C Decomposes befo | re boiling point | | | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 23 Sample Wt, mg 20 | Refractive Index, n ² ₂₀ n ² 5 n ³ 30 | | | | |
| Friction Pendulum lest: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C | 0.9 | | | |
| Rifle Bullet Impact lest: Trials % Explosions Partials | 100°C 120°C 135°C 150°C | 0.9 | | | |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm | 48.1 | | | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate | | | | |
| 10 | Lead Azide Tetryl | 0.30 | | | |
| 15 20 | Ballistic Mortar, % TNT: | 100 | | | |
| 75°C International Heat Test: | Trauzl Test, % TNT: | 107 | | | |
| % Loss in 48 Hrs | Plate Dent Test: Method | | | | |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | | | | |
| Flammability Index: | Detonation Rate: Confinement | None | | | |
| Hygroscopicity: % | Condition Charge Diameter, in. | Pressed 0.5 | | | |
| Volatility: | Density, gm/cc Rate, meters/second | 1.72 7300 | | | |

| Frogmentotion Test: | Shaped Charge Effectiveness, $TNT = 100$: | | |
|---|---|-----------------|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm∕cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | | |
| Total No. of Fragments: For TNT | Color: Ye | llow | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: High temperature heat resistant explosive | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: | Pressed | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Loading Density: gm/cc A t 50,000 p s i Storage: | 1.72 | |
| Density, gm/cc | Method | Dry | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | Group I None | |
| Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | <u>Solubility:</u> Insoluble in water, slightly so alcohol and ether. Soluble in hot acetic acid, hot ethyl acetate and and acetone. <u>Heat of:</u> Combustion, cal/gm (a) Explosion, cal/gm Formation, cal/gm (a) | glacial | |
| | | | |

Preparation:

Five grams of picryl chloride were dissolved in 180 milliliters of absolute methanol. The solution was then saturated with anhydrous, gaseous ammonia. The time required was approximately 30 minutes. The amino derivative precipitated in 78% yield (3.6 gm) melting at 190° C (literature MP 189° C).

Origin:

Picramide (2,4,6-trinitroaniline) was first prepared in 1854 by Pisani who treated picryl chloride with ammonium carbonate (CR 39, 853). The use of picramide, as a brisant explosive, was patended by Chemische Fabrik Griesheim 26 May 1894 (German Patent 84,628). Meisenheimer and Patzig reacted trinitrobenzene with hydroxylamine in cold alcohol solution to obtain picramide (Ber 39, 2534 (1906)). Witt and Witte obtained the compound by nitrating a solution of aniline in glacial acetic acid or concentrated H_2SO_4 at about 5°C with concentrated HNO₃ (Ber 41, 3091 (1908)). Holleman gives details of the prep ation from p-nitroaniline and from acetanilide (Rec trav chim 49, 112 (1930)).

Reference: 58

(a) William H. Rinkenbach, "The Heats of Combustion and Formation of Aromatic Nitro Compounds," J Am Chem Soc 52, 116 (1930).

⁵⁸See footnote 1, page 10.

| Composition: % | | Molecular Weight: | 236 |
|--|--------------|--|------------|
| Explosive D 52 | | Oxygen Balance: ◯◯凵 % ◯◯ % | -63 -19 |
| 111 | | Density: gm/cc Cast | 1.62 |
| | | Melting Point: °C | |
| C/H Ratio | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | 100+ | Boiling Point: "C Refractive Index, n ^D ₂₀ | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 17 19 | n ₂₅ | |
| | | | |
| Friction Pendulum Test: Steel Shoe | Unaffected | Vacuum Stability Test: | |
| Fiber Shoe | Unaffected | cc/40 Hrs, :: 90°C | |
| | onuncetea | - 100°C | 0.37 |
| Rifle Bullet Impact Test: Trials | | 120°C | 0.68 |
| Explosions 0 | | 135°C | |
| Partials 0 | | 150°C | 0.7 |
| Burned 40 | | 200 Gram Bomb Sand Test: | |
| Unaffected 60 | | Sand, gm | 45.9 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 456 | | Sensitivity to Initiation: Minimum Detonating Charge, gm | |
| 1 354 5 Decomposes 285 | | Mercury Fulminate Lead Azide | 0.20 |
| 10 265 | | Tetryl | 0.05 |
| 15 260 | | | |
| 20 255 | | Ballistic Mortar, % TNT: (a) | 100 |
| 75°C International Heat Test: % Loss in 48 Hrs | 0.0 | Plate Dent Test: (b) | |
| | | Method Condition | B Cast |
| 100°C Heat Test: | | Confined | No |
| % Loss, 1st 48 Hrs | 0.0 | Density, gm/cc | 1.63 |
| % Loss, 2nd 48 Hrs Explosion in 100 Hrs | 0.05 None | Brisance, % TNT | 100 |
| Flammability Index: | | Detonation Rate: (b) Confinement | None |
| - | | - Condition | Cast |
| Hygroscopicity: % 30 ⁰ C,90%RH | 0.02 | Charge Diameter, in. | 1.0 |
| Volatility: | | Density, gm/cc | 1.63 |
| | | Rate, meters/second | 6970 |

Picratol, 52/48

| Emgmentation Test: | | Shaped Charge Effectiveness, TNT = 100 | : |
|---|--------------------------------|---|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | 1.61 2.075 | Glass Cones Steel Cor Hole Volume Hole Depth | es |
| Total No. of Fragments: For TNT For Subject HE | 70 3 76 9 | | n-yellow |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | 1.61 0.850 | Principal Uses: AP, SAP projectiles | and bombs |
| Total No. of Fragments: For TNT For Subject HE | 514 487 | Method of Loading: | Cast |
| Fragment Velocity: ft/sec | | Loading Density: gm/cc | 1.62 |
| At 9 ft At 25½ ft Density, gm/cc | 2590 2 <i>320</i> 1.62 | Storage: | |
| | | Method | Dry |
| Blost (Relative to TNT): | | Hazard Class (Quantity-Distance) | Class 9 |
| Air: Peak Pressure Impulse Energy | 100 100 | Compatibility Group | Group I None at 65 ⁰ C |
| Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy | | Preparation: Picratol is made by heating TNT 90°C in a steam-jacketed melt ket sive D is added slowly, without pr and the mixture stirred until unif position. This slurry is cooled to and poured into the appropriate and component. | tle. Explo- ceheating, form in com- to about 85°C |
| Underground: Peak Pressure Impulse Energy Bamb Drop Test: T7, 2000-1b Semi-Armor-Piercing Bomb vs Concrete: Max Safe Drop, ft 10,000-1 | | Origin: Developed during World War II as tive, melt-loaded AP bomb and pro Booster Sensitivity Test: Condition Tetryl, gm Wax, in. for 50% Detonation Density, gm/cc | |

References: 59

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III</u> - <u>Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, OSRD Report No. 5746, 27 December 1945.

(b) D. P. MacDougall, <u>Methods of Physical Testing</u>, OSRD Report No. 803, 11 August 1942.

(c) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute for</u> <u>Tetryl in Boosters</u>, NOL Mamo 10,303, 15 June 1949.

(d) R. W. Drake, <u>Fragment Velocity and Panel Penetration of Several Explosives in Simu-</u><u>lated Shells</u>, OSRD Report No. 5622, 2 January 1946.

(e) Also see the following Picatinny Arsenal Technical Reports on Picratol:

| <u>o</u> | ک | 6 | <u>_7</u> | <u>8</u> | <u>9</u> |
|----------|------|----------------------|--------------|----------|----------|
| 1470 | 1885 | 1466 1796 1956 | 1737 1797 | 1838 | 1729 |

⁵⁹See footnote 1, page 10.

| Composition: | | Molecular Weight: (C6 | ^H 3 ^N 3 ^O 7 ⁾ | 229 |
|--|-------------------------|--|---|--------------|
| C 31.5 | Oxygen Balance: O, % | | -45 | |
| н 1.3 о2и | T NO2 | CO % | | -3.5 |
| N 18.3 |] - | Density: gm/cc | Crystal | 1.76 |
| o 48.9 Y | | Melting Point: "C | | 122 |
| C/H Ratio 0.656 NO ₂ | | Freezing Point: "C | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | 85 | Boiling Point: °C | | |
| Sample Wt 20 mg | | Refractive Index, no | | |
| Picatinny Arsenal Apparatus, in. Sample Wt, mg | 13 17 | n ^D 23 | | |
| Campie we, mg | τI | n ₃₀ | | |
| Friction Pendulum Test: | | | | - |
| Steel Shoe | | Vacuum Stability Test: cc/40 Hrs, at | | |
| Fiber Shoe | | 90°C | | |
| Dide Dullet Immed Tests Trial | | 100°C | | 0.2 |
| Rifle Bullet Impact Test: Trials | | 120°C | | 0.5 |
| % Explosions 0 | | 135°C | | |
| Partials 60 | | 150°C | | |
| Burned 40 | | 200 Gram Bomb Sand Test | t: | |
| Unaffected 0 | | Sand, gm | | 48.5 |
| Explosion Temperature: "C | | Sensitivity to Initiation: | | |
| Seconds, 0.1 (no cap used) | | Minimum Detonating C | harge, gm | |
| 1 5 December 220 | | Mercury Fulminate | 0.26* | |
| 5 Decomposes 320 | | Lead Azide | | 0.24* |
| 10 15 | | Tetryl *Alternative initiatin | ng charges. | |
| 15 20 | | Ballistic Mortar, % TNT: | (a) | 112 |
| 20 | | Traurl Test, % TNT: | (b) | 101 |
| 75°C International Heat Test: | | | | |
| % Loss in 48 Hrs | 0.05 | Plate Dent Test: Method | (c) | A |
| 100°C Heat Test: | | Condition | | Pressed |
| % Loss, 1st 48 Hrs | 0.03 | Confined | | No |
| % Loss, 1st 46 Hrs % Loss, 2nd 48 Hrs | 0.03 0.09 | Density, gm/cc | | 1.50 |
| | | Brisance, % TNT | | 107 |
| Explosion in 100 Hrs | None | Detonation Rate: | 1.55 | - |
| Flammability Index: | | Confinement | (d) Ur | confined |
| Hygroscopicity: % 30°C, 90% RH | 0.04 | Condition Charge Diameter, in. | Pressed 1.0 | Cast 1.25 |
| | | Density, gm/cc | 1.64 | 1.25 |
| Volatility: | | | | |

•

| Booster Sensitivity lest: | (c) | Decomposition Equation: |
|--|-----------------------|---|
| Condition | Pressed Cast | Oxygen, otoms/sec |
| Tetryl, gm | 10 5 | (Z/sec) |
| Wax, in. for 50% Detonation | | Heat, kilacolarie/male |
| , | 2 0 | (ΔH, kcol/mal) Tomporatura Bango °C |
| Wax, gm | | Temperature Range, °C |
| Density, gm/cc | 1.6 1.7 | Phase |
| Heat of: Combustion, cal/gm | 2672 | Armor Plate Impact lest: |
| | | |
| Explosion, cal/gm | 1000 | 60 mm Mortar Projectile: |
| Gas Volume, cc/gm | 675 | 50% Inert, Velocity, ft/sec |
| Formation, col/gm | 248 | Aluminum Fineness |
| Fusion, col/gm (e) | 20.4 | |
| Temperature, ^O C | 122 | 500-16 General Purpose Bombs: |
| Specific Heat: col/gm/°C (e) | I | Plate Thickness, inches |
| $\frac{O_{C}}{O}$ | 0.235 | |
| 30 | 0.258 | 1 |
| 60 | 0.282 | 11/4 |
| 90 | 0.310 0.337 | 11/2 |
| 120 | 0+001 | |
| | | 134 |
| Burning Rate: | | |
| cm/sec | | Bomb Drop lest: |
| Thermal Conductivity: (f) |). | |
| col/sec/cm/°C | 6.24×10^{-4} | 17, 2000-Ib Semi-Armor-Piercing Bomb vs Concrete: |
| Densitv.gm/cc | 1.406 | |
| Coefficient of Expansion: | | Max Safe Drop, ft |
| Linear, %/°C | | 500-lb General Purpose Bomb vs Concrete: |
| | | |
| Volume, %/°C | | Height, ft |
| | | Trials |
| Hardness, Mohs' Scale: | 2.1 | Unaffected |
| | | |
| Young's Modulus: | | |
| E', dynes/cm² | | High Order 🚬 |
| E lb/inch ² | | 1000-lh General Rumose Rombye Concrete |
| Density, gm/cc | | 1000-Ib General Purpose Bomb vs Concrete: |
| Donary, griv co | | Height, ft |
| Compressive Strength: Ib/inch ² | | Trials |
| | | Unaffected |
| | | Low Order |
| Vapor Pressure: "C mm Merci | 107 | |
| | ury | High Order |
| 195 2 | | |
| 255 50 | | |
| | | |
| | | |
| | | |

| Fragmentation Test: | Sheped Charge Effectiveness, $TNT = 10$ |)0: | | | | |
|--|--|--------------------------------------|--|--|--|--|
| 90 mm HE, M71 Projectile, lot WC-91: Density, gm/cc Charge Wt, lb | Gloss Cones Steel Cones Hole Volume Hole Depth | | | | | |
| Total No. of frequents: For TNT | Cobr: Yellow | | | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, ib | Principel Uses: Formerly projectile filler, now explosive admixture; and for the manufacture of Explosive D | | | | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Looding: Pr | ressed | | | | |
| Frogment Velocity: ft/sec At 9 ft At 25½ ft | | 10 ³ 15 20 .61 1.64 | | | | |
| Density, gm/cc | Method | Dry | | | | |
| Blast (Relative to TNT); | Hazard Class (Quantity-Distance) | Class 9 | | | | |
| Air: Peak Pressure Impulse Energy | Compot i bili ty Group Exudation | Group I None | | | | |
| Air, Confinedr Impulse | | | | | | |
| Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | | | | | | |

| Wat | Water Alcohol Benzene Toluene Ether | | | | | | | | |
|----------------------------------|---|----------------------|----------------------|---------------------|--|------------------------------------|------------------|-----------------------------|--------------------------|
| <u></u> | ž | <u>°c</u> | ž | <u>م</u> | <u></u> | <u>م</u> | Z | <u>e</u> | 2 |
| 0 20 40 60 80 100 | 0.85 1.17 1.88 2.98 4.53 7.1 | 0 20 40 | 4.5 6.9 12.0 | 0 20 40 60 | ~2 9.6 27.5 59 | 20 60 | ~13 ~30 | 20 34.7 | ~3 3.96 |
| Chlore | oform | Ethyl | acetate | <u>Ca</u> tetra | <u>bon</u> chloride | Pyr | ridine | Acet | one |
| ° _C | 76 | <u>°</u> | 26 | <u>°c</u> | Z | °c | ž | <u>o</u> c | 2 |
| 20 60 | -2 ~6 | 20 30 40 50 | 42 50 58 69 | 20 60 | ~0.07 ~0.4 | 10 30 50 | 24 37.5 58 | 20 30 40 50 | 125 137 164 208 |
| Me | <u>ethanol</u> , | Isog | propyl alc | <u>ohol</u> | Propano | <u>01-1</u> | Carbon d | isulfide | |
| oC | 2 | o _C | | 2 | <u>°c</u> | 2 | <u>°c</u> | 2 | |
| 0 20 40 50 | 14 19 31 41 | 10 30 50 | | 6.4 9.8 15.5 | 0 20 40 5 0 | 2.4 3•3 5.4 7•4 | 20 30 | 0.12 0.16 | |
| Preparati | on: (Sum | mary Re | port of ND | RC, MV 8 | 3, Vol I) | | | | |
| C6H6 | + Hg(NO3) | 2 | | > | C6H5HgNO3 | + HNO3 | | (| 1) |
| с ₆ н ₅ 1 | HgN03 + N2 | 04 | | | с ₆ н ₅ No + 1 | 1g(N03)2 | | (| 2) |
| • | NO + 2NO | | | | | | | (| 3a) |
| C6H51 | N2 ^{NO} 3 + H2 | 0 | | > | с6н20н + 1 | ¹ 2 + HNO3 | | (| 3b) |
| с ₆ н ₅ с | OH + HNO3 | | NO2 | > | о ₂ мс ₆ н ₄ он | + н ₂ о | | (| 3c) |
| с _{6^н5} | NO oxidat | H Ion and | INO rearrangei | ment > | о ₂ мс _б н ₄ он | | | (| 4) |
| 02NC | _б он + нюо _З | | NO2 | > | (02N)2C6H | ₃ он + н ₂ о | | (| (5) |
| (0 ₂ N |)2 ^{C6H3OH} + | HN03 | NO2 | > | (02N)3C6H2 | ₂ 0H + H ₂ 0 | | (| 6) |

Solubility: grams per 100 grams (%) of: (g)

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The two variables of greatest importance in this process are nitric acid concentration and the effective concentration of benzene (i.e., benzene dissolved in the oxynitration solution). The optimal concentration of nitric acid is in the range 10.4 to 11.6 molar (or the equivalent of 50% to 55% by weight for pure acid). The acid concentration greatly influences the over all rate of reaction, below 10.4 molar the rate falls off rapidly, while above 10.4 molar the rates of both the oxynitration reaction and various side reactions, such as direct nitration, increase rapidly. The range mentioned above seems, in general, to give the lowest proportion of neutral nitro-compounds to nitro-phenols with, at the same time, an adequate rate of oxynitration. The oxynitration solution must be fortified frequently, or, preferably, continuously with nitric acid. Strengths of nitric acid between 95% and 98% are best, due to the smaller increase in reaction volume than if weaker acid were used. The use of absolute nitric acid requires that its direct contact with liquid benzene be avoided.

The effective concentration of benzene is probably the most critical variable affecting the proportion of neutral nitro-compounds to nitrophenols and amounts of colored by-products. Saturation of the oxynitration solution with benzene is undesirable and thus in batch processes slow benzene addition is preferable to the addition of it in one portion; in continuous processes where an excess of benzene is used the rate of agitation is important.

The concentration of mercuric nitrate catalyst does not appear to be a critical factor over a fairly wide range. Concentrations of 0.37 to 0.5 mole of mercuric nitrate per liter of oxynitration solution have been found to give satisfactory results in most cases.

A continuous process, known as the continuous solution process, works on the following cycle. The oxynitration solution is saturated with benzene by vigorous agitation with excess benzene at room temperature, the saturated solution is separated from excess benzene and circulated through a heated coil; it is then cooled to room temperature and agitated again, with benzene, which extracts the organic product and resaturates the oxynitration solution. In evaluating this process, the rate of formation of dinitrophenol per liter of reacting solution in the coil is determined; 70 gm of dinitrophenol per liter per hour is representative performance. The dinitrophenol is, of course, nitrated to picric acid.

Origin:

Picric Acid was first prepared in 1771 by Woulff who found the reaction of nitric acid and indigo yielded a dye. Hausmann isolated Picric Acid in 1778 and studied it further (Journal de physique 32, 165 (1788)). The preparation was studied by many chemists but in 1841 Laurent established its identity (Ann chim phys 111, 3, 221 (1841)). It was used as a yellow dye until Turpin, in 1885, proposed Picric Acid as a bursting charge for high explosive shell (French Patent 167,512). The British adopted Picric Acid as a military explosive in 1888 under the name of lyddite and other nations soon began to use it as the first meltloaded high explosive. Mixtures of other explosives and Picric Acid were developed until it was gradually replaced by TNT about 1900. Today Picric Acid is used for the manufacture of Explosive D.

Destruction by Chemical Decomposition:

Picric Acid is decomposed by dissolving in 25 times its weight of a solution made from 1 part sodium hydroxide and 21 parts sodium sulfide ($Na_2S'9H_2O$) in 200 parts of water. Some hydrogen sulfide and ammonia are evolved.

References: 60

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III</u> - <u>Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, OSRD Report No. 5746, 27 December 1945.

(b) Ph. Naoum, Z ges Schiess-Sprengstoffw, pp. 181, 229, 267 (27 June 1932).

(c) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(d) G. H. Messerly, <u>The Rate of Detonation of Various Explosive Compounds</u>, OSRD Report No. 1219, 22 February 1943.

M D. Hurwitz, The Rate of Detonation of Various Compounds and Mixtures, OSRD Report No. 5611, 15 January 1946.

(e) International Critical Tables.

(f) E. Hutchinson, The Thermal Sensitiveness of Explosives. The Thermal Conductivity Explosive Materials, AC Report No. 2861, First Report, August 1942.

(g) Values taken from various sources in the open literature.

(h) Also see' the following Picatinny Arsenal Technical Reports on Picric Acid:

| 1 | 2 | <u>3</u> | 4 | <u>5</u> | 6 | 7 | 8 | 9 |
|------|------------------------------------|----------|-------------------|-------------------|---|---------------------|------|------|
| 1651 | 132 582 1172 1352 1372 | 1383 | 694 764 874 | 65 425 1585 | 266 556 926 976 986 1446 1556 | 1347 1557 | 1118 | 1549 |

⁶⁰See footnote 1, page 10.

| Composition: % | | Molecular Weight: | 310 |
|--|-----------------|---|-------------|
| PETN Gulf Crown E Oil | 81 19 | Oxygen Balance: CO, % CO % | -74 -31 |
| | | Density: gm/cc Hand tam | 1.35 |
| | | Melting Point: "C | |
| C/H Ratio | | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | | Boiling Point: "C | |
| Sample Wt 20 mg | 44 | Refractive Index, n ^D ₂₀ | |
| Picatinny Arsenal Apparatus, in. Sample Wt, mg | 11 27 | N25 | |
| | | n ^D ₃₀ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| | fected | cc/40 Hrs, at 90°C | |
| Fiber Shoe Unaf | fected | 100°C | 0.48 |
| Rifle Bullet Impact Test: Trials | | 120°C 16 hours | 11+ |
| % | | 135°C | **' |
| Explosions 0 | | 150°C | |
| Partials 0 | | | |
| Burned 0 | | 200 Grem Bomb Sand Test: | 44.0 |
| Unaffected 100 | | Sand, gm | 41.6 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) | | Sensitivity to Initiation: Minimum Detonating Chorge | e, gm |
| 1 5 Decomposes* | | Mercury Fulminate | 0.20* |
| 10 | | Lead Azide | 0.20* |
| 15 | | *Alternative initiating c | harges. |
| 20 | | Ballistic Mortar, % TNT: | |
| *No value obtained. | | Trauzl Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | | Plate Dent Test: (| a) |
| % Loss in 46 His | | Method | -, |
| 100°C Heat Test: | | Condition | Hand tamped |
| % Loss, 1st 48 Hrs | 0.17 | Confined | No |
| % Loss, 2nd 48 Hrs | 0.00 | Density, gm/cc | 1.33 |
| Explosion in 100 Hrs | None | Brisance, % TNT | 76 |
| Flammability Index: | | Detonation Rate: | |
| termine may marked | | Confinement | None |
| Hygroscopicity: % 30 ⁰ C, 90% RH | 0.02 | Condition | Hand tamped |
| rightscopicity. 70 30 63 90% rul | 0.02 | Charge Diameter, in. | 1.0 |
| Volatility: | | Density, gm/cc Rate, meters/second | 1.37 |
| | | Rale, meters/second | 7075 |

PIPE

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: |
|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc l+33 Charge Wt, Ib l+723 | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments:For TNT703For Subject HE519 | Color: |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc 1.39 Charge Wt, Ib 0.735 Total No. of Fragments: For TNT For Subject HE 428 | Principal Uses: Plastic demolition explosive Method of Loading: Hand tamped Loading Density: 1.35 |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc | Storage: Method Dry |
| Blast (Relative to TNT): Air: Peak Pressure Impulse | Hazard Class (Quantity-Distance) Class 9 Compatibility Group Group I Exudation |
| Energy Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy <u>Preparation:</u> PIPE is manufactured by simple mechanica mixing of PETN in oil. | Origin:PIPE, a mechanical mixture of PEIN and Gulf Crown E 0il, was developed in the United States during World War 11.References: 61(a) L. C. Smith and E. G. Eyster, Physical Testing of Explosives, Part III-Miscellaneous Sensitivity Tests; Performance Tests, OSRD Report No. 5746, 27 December 1945.(b) S. Livingston, Properties of Explosives RIPE, PIPE and PEP-3, Picatinny Arsenal Techni- cal Report 1517, 24 April 1945. |

⁶¹See footnote 1, page 10.

| Composition: | | Molecular Weight: | 291 |
|--|----------|--|----------------------|
| % Lead Nitrate | 70 | Oxygen Balance: CO, % CO % | -5.4 +9•3 |
| IMI | 30 | Density: gm/cc | |
| | | Melting Point: "C | |
| C/H Ratio | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg | | Boiling Point: "C | |
| Picatinny Arsenal Apparatus, in. Sample Wt, mg | 13 22 | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | | Vacuum Stability Test: cc/40 Hrs, at 90°C | |
| Rifle Bullet Impact Test: Trials % Explosions Partiols | | 100°C 120°C 135°C 150°C | |
| Burned Unaffected | | 200 Gram Bomb Sand Test: Sand, gm | 32.4 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Decomposes 238 10 15 | | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminote Lead Azide Tetryl | 0.20 0.10 |
| 20 | | Ballistic Mortar, % TNT: | |
| 75°C International Heat lest: % Loss in 48 Hrs | | Plate Dent Test: Method | |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | | Detonation Rate: (b) Confinement | |
| Hygroscopicity: % | | Condition Charge Diameter, in. | |
| Volatility: | | Density, gm/cc Rate, meters/second | 2. 89 4850 |

| Fragmentation lest: | Shaped Charge Effectiveness, $TNT = 100$: | | | |
|---|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel C o nes (a) Hole Volume 114 Hole Depth 103 | | | |
| Total No. of Fragments: For TNT | Color: Light yellow | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: | | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Cast | | | |
| | Loading Density: gm/cc | | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | | | |
| Density, gm/cc | Method Dry | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 | | | |
| Air: Peak Pressure Impulse | Compotibility Group Group I | | | |
| Energy Air, Confined: Impulse | Origin: An explosive containing 70% lead nitrate and 30% TNT has been used in Belgium under the name of "Marcarite." | | | |
| Under Water: Peak Pressure Impulse Energy | (a) Eastern Laboratory, du Pont, <u>Investi-</u> gation of Cavity Effect, Sec III, Variation of | | | |
| Underground: Peak Pressure Impulse | Cavity Effect with Explosive Composition, NDRC Contract W-672-ORD-5723. (b) Thorpe's Dictionary of Applied Chem- istry, Fourth Edition, Vol IV, Longmans, Green | | | |
| Energy Preparation: | and Company, London - New York - Toronto, p. 464. | | | |
| Plumbatol is manufactured by simple mechanical mixing of lead nitrate in molten TNT. | | | | |

62_{See} footnote 1, page 10.

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PLX (Liquid)

| Composition: | | | Molecular Weight: | $\frac{100}{61}$ | $\frac{95/5}{61}$ |
|--|-----------------|-------------------------------------|--|-----------------------|-------------------|
| Nitromethane Ethylenediamine | 100 | 5 | Oxygen Balance: CO, % CO % | -39 -13 | -48 -21 |
| *The mixture 95/5 Nitromethane/Ethylenediamine is designated PLX (for Picatinny Liquid Explo- | | | Density: gm/cc | 1.14 | 1.12 |
| sive). See note und | er <u>Stora</u> | <u>ge</u> . | Melting Point: °C | -29 | |
| C/H Ratio | | | Freezing Point: "C | | |
| Impact Sensitivity, 2 Kg W Bureau of Mines Appara | | <u>100</u> <u>95/5</u> 100+ 100+ | Boiling Point: °C | 101 | |
| Sample Wt 20 rng Picatinny Arsenal Appar | ratus, in. | | Refractive Index, n ^D ₂₀ | | |
| Sample Wt, mg | | 20 20 | n ₂₅ n ₃₅ | | |
| friction Pendulum Test: | | | Vacuum Stability Test: | | |
| Steel Shoe | | Unaffected | cc/40 Hrs, at | | |
| Fiber Shoe | | Unaffected | 90°C | | |
| Rifle Bullet Impact Test: | 10 Trials | 5 Trials | 100°C 120°C | | |
| Explosions | % 0 | % O | 135°C | | |
| Partials | 0 | 0 | 150°C | | |
| Burned | 0 | 0 | 200 Gram Bomb Sand Tes | | <u>95/5</u> |
| Unaffected | 100 | 100 | Sand, gm | st: <u>100</u> 8.1 | <u>50.6</u> |
| Explosion Temperature: Seconds, 0.1 | "C 100 | °c 95/5 | Sensitivity to Initiation: Minimum Detonating (| Chorao am | |
| Seconds, U.1 | 100 | <u>7777</u> | Mercury Fulminate | Sharge, gin | |
| 5 | 430 | 430 | Lead Azide | | |
| 10 | | - | | | |
| 15 | | | Tetryl | | |
| 20 | | | Ballistic Mortar, % TNT: | 134 | |
| 75°C laterational linet T | | | Trauzl Test, % PA | 127 | |
| 75°C International Heat Te % Loss in 48 Hrs | est. | | Plate Dent Test: Method | | |
| 100°C Heat Test: | | | Condition | | |
| % Loss, 1st 48 Hrs | | | Confined | | |
| % Loss, 2nd 48 Hrs | | | Density, gm/cc | | |
| Explosion in 100 Hrs | | | Brisance, % TNT | | |
| Flammability Index: | | | Detonation Rate: Confinement | 1/32"* Glass | 1/32"* Glass |
| | | | | Liquid | Liquid |
| Hygroscopicity: % | | | Charge Diameter, in. | - | 0.94 |
| | | | Density, gm/cc | 1.14 | 1.12 |
| Volatility: | | | · · · · | | |

PLX (Liquid)

AMCP 706-177

| Booster Sensitivity lest: Nitromethane | Decomposition Equation: (d) <u>Nitromethane</u> |
|--|---|
| Condition | Oxygen, atoms/sec |
| Tetryl, gm | (Z/sec) Heat kilocalarie/male 56.6 |
| Wax, in. for 50% Detonation | Heat, kilocalarie/male 56.6 (AH, kcal/mal) |
| Wax, gm | Temperature Range, °C 380-430 |
| Density, gm/cc | Phase Gaseous |
| Heat of: (a) | Armor Plate Impact Test: |
| Combustion, cal/gm 2830 | Amor Flate Impact rest. |
| Explosion, cal/gm | 60 mm Mortar Projectile: |
| Gas Volume, cc/gm | 50% Inert, Velocity, ft/sec |
| Formation, cal/gm =348 | Aluminum Fineness |
| Fusion, cal/gm Vaporization, cal/gm 149 | 500-lb General Purpose Bombs: |
| Specific Heat: col/gm/°C (b) | |
| $C = 0.4209 \cdot 0.00076t + 0.0000061t^2$ P for 15°C to 70°C | Plate Thickness, inches |
| | 1 |
| | 11/4 |
| | 11/2 |
| | 134 |
| Burning Rate: | |
| cm/sec | Bomb Drop Test: |
| Thermal Conductivity: col/sec/cm/°C | T7, 2000-1b Semi-Armor-Piercing Bomb vs Concrete: |
| | Max Safe Drop, ft |
| Coefficient of Expansion: Linear, %/°C | 500-Ib General Purpose Bomb vs Concrete: |
| Volume, %/°C | Height, ft |
| | Trials |
| Hardness, Mohs' Scale: | Unaffected |
| | Low Order |
| Young's Modulus: | High Order |
| E, dynes/cm² E, lb/inch² | |
| E, ID/Inch ² Density, gm/cc | 1000-Ib General Purpose Bomb vs Concrete: |
| | Height, ft |
| Compressive Strength: Ib/inch ² | Triols |
| - | Unaffectea |
| Vapor Pressure: (c) | Low Order |
| °C mm Mercury | High Order |
| 70 258 | |
| 85 444 | |
| | |
| | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | | | |
|---|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, ib | Glass Cones Steel Cones Hole Volume Hole Depth | | | |
| Total No. of Fragments: For TNT | Color: Light yellow | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Minefield clearing | | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pumping | | | |
| Fragment Velocity: ft/sec | Loading Density: gm/cc <u>100</u> 95/5 1.14 1.12 | | | |
| At 9 ft At 25½ ft Density, gm/cc | Storage: Method Components stored separately; mixed only when ready to use | | | |
| Blast (Relative to TNT): Air: Peak Pressure Impulse Energy | Hazard Class (Quantity-Distance) Compatibility Group Exudation | | | |
| Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure impulse Energy | nimum Propagating100 $95/5$ Thickness. in: 0.5 0.063 Viscosity centipoises:(e)Temp, $10^{\circ}C$ 0.748 $25^{\circ}C$ 0.625 $40^{\circ}C$ 0.533 Compatibility with Metals:Stainless steel, mild steel and durironnot affected; corrodes brass. | | | |
| | | | | |

Origin:

Nitromethane has been known since 1872 (Kolbe, J prakt Chem (2) $\underline{5}$, 427 (1872), but was available only as a laboratory product until it appeared as an industrial chemical in 1940. A number of patents have been issued for nitromethane produced as a by-product of the nitration of propane (U. S. Patent 1,967,667 (1934); British Patent 443,707 (1937); and Canadian Patent 371,007 (1938).

The development of nitromethane liquid explosives was based on information that nitromethane is sensitized to initiation and propagation of detonation by the addition of various amines. This study made at Picatinny Arsenal in 1945 indicated that mixtures of nitromethane with 5% of ethylenediamine, n-butyl-amine, or morpholine showed considerable promise for application in mine-field clearance (L. H. Eriksen and J. W. Rowen, PATR No. 1565, 17 September 1945).

References:63

(a) D. E. Holcomb and C. F. Dorsey, "Thermodynamic Properties of Nitroparaffins," Ind Engr Chem $\underline{\mu_1}$, 2788 (1949).

(b) J. W. Williams, "A Study of the Physical Properties of Nitromethane," J Am Chem Soc <u>47</u>, 2644 (1925).

(c) L. Medard, "Explosive Properties of Nitromethane," Mem poudr 33, 125 (1951).

(d) T. L. Cottrell, T. E. Graham and T. J. Reid, "The Thermal Decomposition of Nitromethanes," Transactions of the Faraday Society $\frac{47}{5}$, 584 (1951).

(e) F. Bellinger, H. B. Friedman, W. H. Bauer, J. W. Eastes and W. C. Bull, "Chemical Propellants: Stability of Mononitromethane," Ind Engr Chem <u>40</u>, 1320 (1948).

(f) Also see the following Picatinny Arsenal Technical Reports on Nitromethane:

| <u>o</u> | <u>1</u> | 3 | 5 | <u>م</u> | Z | B | 9 |
|----------|--------------|------|--------|----------|------|------|------|
| 1660 | 1681 1831 | 2113 | 1565 . | 2016 | 1747 | 1708 | 1619 |

⁶³See footnote 1, page 10.

| Composition: | Molecular Weight: $(KC_6H_4N_4O_6)$ | 225 |
|---|--|--|
| % с 27.3 н 0.4 N 21.2 | Oxygen Balance: CO ₂ % CO % | -60 -18 |
| $\begin{array}{c} n \\ 0 \\ 36.3 \\ 0_2 n \\ \end{array}$ | Density: gm/cc | 2.21 |
| к 14.8 | Melting Point: °C Explodes | 210 |
| C/H Ratio 0.416 | Freezing Point: °C | |
| Impoct Sensitivity, 2 Kg Wt: Bureou of Mines Apparatus, cm *- | Boiling Point: °C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 3 (11b wt) 6 Sample Wt, mg 7 | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₂₀ | |
| Friction Pendulum Test: | Vocuum Stability Test: | |
| Steel Shoe Explodes | cc/40 Hrs, at | |
| Fiber Shoe Explodes | 90°C | |
| Rifle Bullet Impact Test: Trials | 120°C | |
| % | 135°C | |
| Explosions Partio Is | 150°C | |
| Burned | 200 Grom Bomb Sand Teat: | |
| Unaffected | Sond, gm 44.8 Black povder, fuse 9.5 | 43.6 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) | Sensitivity to Initiatien: Minimum Detonating Charge, gm | |
| 1 | Mercury Fulminate 0.30 | 0.20 |
| 5 250 10 | Lead Azide Tetryl | 0.10 |
| | | ······································ |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent lest: Method | <u> </u> |
| 100°C Heat Test: | Condition | |
| % Loss, 1st 48 Hrs 0.03 | Confined | |
| % Loss, 2nd 48 Hrs 0.05 | Density, gm/cc Brisance, % TNT | |
| Explosion in 100 Hrs None | | |
| Flammability Index: | Detonation Rate: Confinement | |
| Hygroscopicity: % 30°C, 75% RH 0.11 30°C, 90% RH 0.27 | Condition Charge Diameter, in. | |
| | Density, gm/cc | |

| Baester Sensitivity Test: | | Decomposition Equation: |
|--|-------|---|
| Condition | | Oxygen, atoms/sec |
| Tetryl, gm | | (Z/sec) |
| Wax, in. for 50% Detonation | | Heat, kilocalorie/mole (AH kcol/mol) |
| Wax, gm | | Temperature Ronge, °C |
| • • | | Phase |
| Density, gm/cc | | |
| Heat of: | 2209 | Armor Plate Impact Test: |
| Combustion, col/gm | | |
| Explosion, cal/gm | 725 | 60 mm Mortar Projectile: |
| Gas Volume, cc/gm | 604 | 50% tncrt, Velocity, ft/sec |
| Formation, col/gm | | Aluminum Fineness |
| Fusion, col/gm | | 500-lb General Purpose Bambs; |
| Specific Heat; col/gm/°C (b) | | |
| | | Plate Thickness, inches |
| ~~ 50 | 0.217 | 1 |
| 0 | 0.217 | |
| 25 | 0.217 | 11/4 |
| 50 | 0.217 | 11/2 |
| Burning Rate: | | 1% |
| cm/sec | | |
| | | Somb Drop Test: |
| Thermal Conductivity: | | 77, 2000-1b Semi-Armer-Piercing Bomb vs Concrete: |
| col/sec/cm/°C | | TT, AVV-ID Jenni-Armor-Freezeng Bond Ts Concepte. |
| Coefficient of Expansion; | | Mex Safe Drop, ft |
| Linear, %/°C | | 500-16 General Purpose Bomb vs Concrete: |
| Volume, %/°C | | Height, ft |
| | | Trials |
| Hardness, Mohs' Scale: | | Unaffected |
| ¥ | | Low Order |
| Young's Modulus: | | High Order |
| Ę′, dynes∕cm² | | |
| E, lb/inch ² | | 1000-ib General Purpose Bomb vs Concrete: |
| Density, gm/cc | | |
| | | Height, ft |
| Compressive Strangth: Ib/inch ² | | Triols |
| | | Unaffected |
| Vapor Pressure: | | Low Order |
| °C mm Mercury | | High Order |
| | | - |
| | | |
| | | |
| | | |

| Fragmentation Test: | Shaped Charge Effectiveness, TNT = 100: | | | |
|--|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: | Glass Cones Steel Cones | | | |
| Density, gm/cc | Hole Volume | | | |
| Charge Wt, Ib | Hole Depth | | | |
| Total No. of Fragments: | Color: Orange to brown | | | |
| For TNT | | | | |
| For Subject HE | Principal Uses: Primary explosive | | | |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | | | | |
| Density, gm/cc | | | | |
| Charge Wt, Ib | | | | |
| Total No. of Fragments: | Method of Loading: Pressed | | | |
| For TNT | Method of Loading. Flessed | | | |
| For Subject HE | | | | |
| | Loading Density: gm/cc psix 10 ⁻³ | | | |
| Fragment Velocity: ft/sec | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | |
| At 9 ft At 25½ ft | Storage: | | | |
| Density, gm/cc | | | | |
| | Method Wat | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) Class 9 | | | |
| Air: | Compatibility Group Group M (wet) | | | |
| Peak Pressure | Fredetien | | | |
| | Exudation | | | |
| Energy | | | | |
| Air, Confined: | Solubility in Water, gm/100 gm solvent, at: | | | |
| Impulse | 30°C 0.245 | | | |
| Under Water: | Stab Sensitivity: | | | |
| Peak Pressure Impulse | Density Firing Point (inch-ounces) | | | |
| Energy | <u>gm/cc 0% 50% 100%</u> | | | |
| Licity | 1.63 73 79 84 1.77 66 75 ⁸ 3 | | | |
| Underground: | 1.81 42 48 64 | | | |
| Peak Pressure | 1.86 12 15 18 1.93 11 17 21 | | | |
| Impulse | 1.93 11 11 211.98 7 11 14 | | | |
| Energy | Activation Energy: | | | |
| | | | | |
| | kcal/mol 82.6 Induction Period, sec 0.5-10 | | | |
| | | | | |
| | | | | |

Preparation of Potassium Salt of 4,6-dinitrobenzfuroxan: (a)

Benzfuroxan, made by the reaction of ortho-nitroaniline and alkaline sodium hypochlorite, was dissolved in 6 parts of 96% sulf'uric acid and nitrated at 5° -20°C with a 4 to 1 sulfuricnitric acid mixture. The salt was prepared by neutralization of the 4,6-dinitrobenzfuroxan with potassium bicarbonate followed by recrystallization from hot water. The product forms in small golden orange plates which explode at 210°C.

Origin:

The potassium salt of 4,6-dinitrobenzfuroxan was first prepared in 1899 by von P. Drost (Ann 307, 56 (1899)).

References: 64

(a) R. J. Gaughran, J. P. Picard and J. V. R. Kaufman, "Contribution to the Chemistry of Benzfuroxan Derivatives," J Am Chem Soc <u>76</u>, 2233 (1954).

(b) C. Lenchitz, <u>Ice Calorimeter Determination of Enthalpy and Specific Heat of Eleven</u> <u>Organometallic Compounds</u>, PATR No. 2224, November 1955.

(c) Also see the following Picatinny Arsenal Technical Reports on Potassium Dinitrobenzfuroxan:

| 2 | 3 | <u>6</u> | <u>9</u> |
|------|------|----------|----------|
| 2122 | 2093 | 2146 | 2179 |

⁶⁴See footnote 1, page 10.

| Composition: % | | Molecular Weight: | 252 |
|--|------|--|-------------|
| RDX | 30 | Oxygen Balance: | -45 - 9 |
| Tetryl | 50 | | |
| TNT | 20 | Density: gm/cc | 1.68 |
| | | Melting Point: "C Eutectic | 67 |
| C/H Ratio | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | 44 | Boiling Point: °C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | | Refractive Index, n ^O ₂₀ n ^O 25 n ^O 30 | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| Steel Shoe | | cc/40 Hrs, at | |
| Fiber Shoe | | 90°C | 2.0 |
| Rifle Bullet Impact Test: Trials | | 120°C | 3.0 |
| Surlaciona 20 | | 135°C | |
| Explosions 20 Partials 20 | | 150°C | |
| Burned 0 | | 200 Gram Bomb Sand Test: | |
| Unaffected 60 | | Sand, gm | 54.8 |
| Explosion Temperature: "C | | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) | | Minimum Detonating Charge, gm | |
| 1 5 | | Mercury Fulminate | 0.23* |
| 10 | | Lead Azide | 0.22* |
| 15 | | Tetry! *Alternative initiating charges. | |
| 20 | | Ballistic Mortar, % TNT: (a) | 132 |
| | | Trauzi lest, % TNT: | |
| 75°C International Heot lest: % Loss in 48 Hrs | | Plate Dent Test: (b) | |
| | | Method | В |
| 100°C Heat Test: | | Condition | Cast |
| % Loss, 1st 48 Hrs | | Confined | No |
| % Loss, 2nd 48 Hrs | | Density, gm/cc | 1.68 |
| Explosion in 100 Hrs | | Brisance, % TNT | 127 |
| Flammability Index: | | Detonation Rate: | None |
| | | Confinement Condition | Cast |
| Hygrosco _o icity: % | | Charge Diameter, in. | Last 1.0 |
| 30 0 C, 90%RH, 15 days | 0.00 | Density, gm/cc | 1.64 |
| Volatility: | | Rate, meters/second | 7655 |

PTX-1

| Fragmentation Test: | | Shaped Charge Effectiveness, TNT = | 100: |
|---|---|--|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, lb | 1.64 2.180 | Glass Cones Stee Hole Volume Hole Depth | l Cones |
| Total No. of Fragments: For TNT | 703 | Color: | |
| For Subject HE | 999 | Principal Uses: Land mines and o | demolition |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | | charges | |
| Density, gm/cc | 1.63 | | |
| Charge Wt, Ib | 0.864 | | |
| Total No. of Fragments: | | Method of Loading: | Cast |
| For TNT | 514 | | |
| For Subject HE | 68 5 | Loading Density: gm/cc | 1.68 |
| Fragment Velocity: ft/sec | 0/00 | | |
| At 9 ft At 25½ ft | 2690 2460 | Storage: | |
| Density, gm/cc | 1.64 | Method | Dry |
| Blast (Relative to TNT): | | Hazard Class (Quantity-Distance) | Class 9 |
| Air: | (d) | Compatibility Group | Group I |
| Peak Pressure | 111 | | Exudes at 65 ⁰ C |
| Impulse | 109 | Exudation | Exudes at 05 C |
| Energy | | | |
| Air, Confined: | | Preparation: | |
| Impulse Under Water: Peak Pressure Impulse Energy | | The ternary explosive syste RDX, tetryl and TNT is prepare appropriate weight of water-w tol (40/60) previously melted jacketed melt kettle. Heating are continued until all the w and the mixture is uniform in PTX-1 is also prepared by add Coinposition B. | ed by adding the et RDX to a tetry in a steam- g and stirring vater is evaporated composition. |
| Underground: Peok Pressure | | Composition B. Compatibility with Metals: | |
| Impulse | | Dry: Aluminum, mild steel | not affected. |
| Energy | | Wet: Aluminum, mild steel | not affected. |
| Tetryl, gm 1 Wax, in. for 50% Detonation 1 | ssed Cast 00 100 .94 1.82 .61 1.68 | | |

Origin:

The possibility of employing ternary mixtures to obtain explosives having greater power and higher brisance than binary mixtures was suggested by the analysis of Russian 76 mm, armor piercing high explosive rounds (PATR No. 1311, 17 July 1943). The Russian'type ternary explosives, based on the composition and laboratory studies of such mixtures, were indicated to be effective pressed fillers. In conducting *a* preliminary study of <u>castable</u> ternary explosive mixtures suggested by the Russian fillers, a mixture consisting of RDX/tetryl/TNT, designated PTX-1 was developed which had explosive and physical properties offering considerable advantage for military applications (PATR No. 1360, 27 October 1943; and 1379, **11** January 1944).

A PTX-3 composition, prepared by the addition of Haleite to 40/60 tetrytol, also offered promise but limited to applications where the charge would not be required to withstand storage at 65° C without exudation.

References: 65

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III</u> - <u>Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, OSRD Report No. 5746, 27 December 1945.

(b) D. P. MacDougall, <u>Methods of Physical Testing</u>, OSRD Report No. 803, 11 August 1942.

(c) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute for Tetryl in Boosters</u>, NOL Mamo 10,303, 15 June 1949.

(d) W. R. Tomlinson, Jr., <u>Blast Effects of Bomb Explosives</u>, PA Tech Div Lecture, 9 April 1948.

(e) Also see the following Picatinny Arsenal Technical Reports on PTX-1:

| <u>o</u> | 2 | <u>3</u> | 6 | <u>7</u> | 2 |
|----------|------|----------|--------------|----------|----------------------|
| 153C | 1402 | 1623 | 1466 1506 | 1437 | 1379 1429 1469 |

⁶⁵See footnote 1, page 10.

PTX-2

AMCP 706-177

| Composition: | Molecular Weight: 244 | 243 |
|--|---|---------------------------|
| % RDX 44 - 41 PETN 28 - 26 | Oxygen Balance: <i>CO</i> , % - 33 CO % - 3 | -36 - 4 |
| TNT 28 - 33 | Density: gm/cc | 1.70 |
| | Melting Point: "C Eutectic | 75 |
| C/H Ratio | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 35 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | Boiling Point: °C Refractive Index, n ⁰ ₂₀ n ⁰ ₂₃ n ⁰ ₃₀ | |
| Friction Pendulum Test: Steel Shoe Crackle Fiber Shoe | vacuum Stability Test: cc/40 Hrs, at 90°C 100°C | 2.6 |
| Rifle Bullet Impact Test: Trials % Explosions 60 Partials 0 | 120°C 135°C 150°C | 11+ |
| Burned O Unaffected 40 | 200 Gram Bomb Sand Test: Sand, gm | 56.9 |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) 1 5 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl | 0.21 0.00 0.00 |
| 15 20 | Ballistic Mortar, % TNT: (a) | 138 |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: (b) Method | В |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | Cast No 1.71 141 |
| Flammability Index: | Detonation Rate: Confinement | None |
| Hygroscopicity: % 30°C, 90% RH, 15 days 0.00 | Condition Charge Diameter, in. Density, gm/cc | Cast 1.0 1.70 |
| Volatility: | Rate, meters/second | 8065 |

<u>PTX-2</u>

| Fragmentation Test: | | Shoped Charge Effectiveness, $TNT = 10$ | 0: | |
|--|--|---|--------------------------------------|--|
| 90 mm 旺, M71 Projectile, Lot WC Density, gm/cc Charge Wt, Ib | 2-91: 1.68 2.226 | Glass Cones Steel Co Hole Volume \sim 130 Hole Depth | ones | |
| Total No. of Fragments: For TNT | 703 | Color: | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot K Density, gm/cc Charge Wt, Ib | 1128 C-5: 1.70 0.897 | Principal Uses: Shaped charges Fragmentation cha | rges | |
| Total No. of Fragments: For TNT For Subject HE | 514 750 | Method of Loading: | Cast | |
| Fragment Velocity: ft/sec At 9_ft | 3020 | Loading Density; gm/cc | 1.70 | |
| A t 25½ ft Density, gm/cc | 2850 1.70 | Storage: Method | Dry | |
| Blast (Relative to TNT): | | Hazard Class (Quantity-Distance) | Class 9 | |
| Air: Peak Pressure Impulse Energy | (d) 113 113 | Compatibility Group | Group I None at 65 ⁰ C | |
| Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy Rooster Sensitivity Test: Condition Tetry1, gn Wax, in. for 50% Detonation | () Pressed Cast 100 100 1.87 2.32 | Preparation:The ternary explosive system consisting of RDX, PETN and TNT is prepared by adding the appropriate weight of water-wet RDX to a pen- tolite (30/70) previously melted in a steam- jacketed melt kettle. Heating and stirring are continued until all the water is evaporated and the mixture is uniform in composition. PTX-2 is also prepared by adding water-wet PETN to RDX Composition B. Compatibility with Metals:Dry:Aluminum, mild steel not affected. Wet: Aluminum not affected. | | |

Origin:

The possibility of employing ternary mixtures to obtain explosives having greater power and higher brisance than binary mixtures was suggested by the analysis of Russian 76 mm, armorpiercing high explosive rounds (PATR No. 1311, 17 July 1943). The Russian type ternary explosives, based on the composition and laboratory studies of such mixtures, were indicated to be effective <u>pressed</u> fillers. In conducting a preliminary study of <u>castable</u> ternary explosive mixtures suggested by the Russian fillers, a mixture consisting of <u>RDX/PETN/TNT</u>, designated PTX-2 was developed which had explosive and physical properties offering considerable advantage for military applications (PATR No. 1360, 27 October 1943; and 1379, **11** January 1944).

A PTX-4 composition, prepared by the addition of Haleite to 30/70 Pentolite, also offered promise but because of border-line stability in accelerated stability tests, PTX-4 must be proven by long term storage to be acceptable for use in standard ammunition.

References: 66

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III - Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance</u> Tests, <u>OSRD Report No. 5746</u>, 27 December 1945.

(b) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(c) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute for</u> <u>Tetryl in Boosters</u>, NOL Mamo 10,303, 15 June 1949.

(d) W. R. Tomlinson, Jr., <u>Blast Effects of Bomb Explosives</u>, PA Tech Div Lecture, 9 April 1948.

(e) Also see the following Picatinny Arsenal Technical Reports on PTX-2:

| Ω | 2 | 3 | 4 | 5 | <u>6</u> | 8 | <u>9</u> |
|------|------|----------------------|------|------|----------|------|-----------------------------|
| 1530 | 1482 | 1483 162 3 | 1414 | 1445 | 1466 | 1838 | <i>1379</i> 1429 1469 |

⁶⁶See footnote 1, page 10.

PVA-4

| Composition: % | | Molecular Weight: | 217 |
|---|------------|--|---------------|
| RDX | 90 | Oxygen Balance: | |
| | | CO <u>∘</u> % CO % | -37 -10 |
| Polyvinyl Acetate | 8 | | |
| Dibutylphthalate | 2 | Density: gm/cc Pressed | 1.60 |
| | | Melting Point: °C Softening Point: °C | 92 |
| C/H Ratio | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | 39 | Boiling Point: "C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. | 9 | Refractive Index, $\mathbf{n}_{20}^{\mathrm{D}}$ | |
| Sample Wt, mg | 13 | ∩ ^D ₂₅ | |
| | | n ^D ₃₀ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| Steel Shoe | Crackles | cc/40 Hrs, at | |
| Fiber Shoe | Unaffected | 90°C | • · - |
| Rifle Bullet Impact Test: 5 Triols * | | 100°C | 0.45 |
| 20 | | 120°C | 0.88 |
| Explosions | | 135°C | |
| Portials 0 | | 150°C | 11+ |
| Burned 60 | | 200 Gram Bomb Sand Test: | |
| Unoffected *100 trials at -46°C - Unaffe | cted | Sand, gm | 58.5 |
| Explosion Temperature: "C | | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) | | Minimum Detonating Charge, gm | |
| 1 330 | | Mercury Fulminate | |
| 5 Decomposes 375 | | Lead Azide | 0.22 |
| 10 265 | | Tetryl | |
| 15 | | Ballistic Mortar, % TNT: | |
| 20 | | Trauri Test, % TNT: | |
| 75°C International Heat Test: | | · · · · · · · · · · · · · · · · · · · | |
| % Loss in 48 Hrs | | Plate Dent Test: | |
| | | Method | |
| 100°C Heat Test: | | Condition | |
| % Loss, 1st 48 Hrs | 0.10 | Confined | |
| % Loss, 2nd 48 Hrs | 0.06 | Density, gm/cc Brisance, % TNT | |
| Explosion in 100 Hrs | None | | |
| Flammability Index: | | Detonation Rate: | News |
| | | Confinement | None |
| Hygroscopicity: % 30 ⁰ C, 90% RH | 0.20 | Condition | Cast |
| | | Charge Diameter, in. Density, gm/cc | $1.0 \\ 1.60$ |
| Volatility: 55°C, vacuo, 6 hrs | 0.03 | Rate, meters/second | |
| | | Kate, meters/second | 7910 |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | |
|---|---|---|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Co Hole Volume Hole Depth | ones |
| Total No. of Fragments: For TNT | Color: | White |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Demolit | ion charges |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pressed or | extruded |
| | Loading Density: gm/cc | 1.60 |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | |
| Density, gm/cc | Method | Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation Not | Group I ne at 71 [°] C |
| Air, Confined: Impulse | Plasticity: -40 ⁰ C | Cracked |
| Under Water: Peak Pressure Impulse Energy | 25 [°] C | 0.3 |
| Underground: Peak Pressure Impulse Energy | | |

PVA-4

Preparation:

Explosive FVA-4, a semi-plastic composition of Canadian origin, consists of 90% RDX, 8% polyvinyl acetate and 2% dibutylphthalate (DBP). This formulation was developed by Dr. Sutherland of Shawinigan Chemicals, Ltd. In evaluating various types of polyvinyl acetate commercially available in the United States, a type obtained from Union Carbide and Carbon, under the industrial named or designation "AYAT" was the most promising coating for RDX in the proportions RDX/PVA (AYAT)/DBP 92/6/2.

A practical method of preparing this composition was by the addition of a solution of the coating agent to an aqueous RDX slurry. Based dn the quality of the product and the pellet densities obtained, a procedure of adding an acetone solution of PVA + DBP to a hot water slurry of RDX, under agitation, was adopted as standard.

References: 67

(a) See the following Picatinny Arsenal Technical Reports on PVA-4: 1532 and 1634.

⁶⁷See footnote 1, page 10.

| Composition; | | Molecular Weight: $(C_2H_3NO_3)_n$ | (89) _n |
|---|-------------|--|-------------------|
| % C 27 3.4 | | Qxygen Balance: CO, % CO % | -45 - 9 |
| (H ₂ C-CH-ONO ₂) _n 15.6 | | Density: gm/cc | |
| <i>o</i> 54 | | Melting Point: °C (Soft Pb) | 50 |
| C/H Ratio 0.203 | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatys, cm | 14.86%N | Boiling Point: "C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. | 4 | Refractive Index, n ^D ₂₀ | |
| Sample Wt, mg | 7 | n ₂₅ | |
| | | n ₃₀ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| | ackles | cc/40 Hrs, at | |
| Fiber Shoe Un | affected | 90°C | 11 . |
| Rifle Buttet Impact Test: Trials | | | - |
| % | | 120°C 16 hou 135°C | 15 11+ |
| Explosions | | | |
| Partials | | 150°C | |
| Burned | | 200 Gram Bomb Sand Test: | |
| Unaffected | | Sand, gm | 49.9 |
| Explosion Temperature: °C | | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) | | Minimum Detonating Charge, gm | |
| 1 5 265 | | Mercury Fulminate | |
| 10 | | Lead Azide | |
| 15 | | Tetryl | |
| 20 | | Bellistic Mortar, % TNT: | |
| | | Trauzi Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | | Plate Dent Test: | |
| | | Method | |
| 100°C Heat Test: | | Condition | |
| % Loss, 1st 48 Hrs | 1.9 | Confined | |
| % Loss, 2nd 48 Hrs | 2.1 | Density, gm/cc | |
| Explosion in 100 Hrs | None | Brisance, % TNT | |
| Flammability Index : | | Detonation Rate: Confinement | |
| Hygroscopicity: % 30 [°] C, 90% RH | 0.62 | Condition Charge Diameter, in. | |
| Volatility : | | Density, gm/cc | |
| | | Rate, meters/second | |

| Fragmentation Test: | Shaped Charge Effectiveness, TN | T = 100: | |
|--|--|----------------------|--|
| 90 mm HE, M71 Projectile, Lot WC-91: | Class Capes | Stool Cones | |
| Density, gm/cc | Glass Cones Steel Cones Hole Volume | | |
| Charge Wt, Ib | Hole Depth | | |
| Total No. of Fragments: | | | |
| For TNT | Color: | | |
| For Subject HE | | | |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | Principal Uses: | | |
| · · · · | | | |
| Density, gm/cc | | | |
| Charge Wt, Ib | | | |
| Total No. of Fragments: | | | |
| For TNT | Method of Loading: | | |
| For Subject HE | | | |
| | Loading Density: gm/cc | | |
| ragment Velocity: ft/sec | | | |
| At 9 ft At 25½ ft | Sternwei | | |
| Density, gm/cc | Storage: | | |
| | Method | | |
| last (Relative to TNT); | Hazard Class (Quantity-Distanc | e) | |
| Air: | | | |
| Peak Pressure | Compatibility Group | | |
| Impulse | Exudation | | |
| Energy | | | |
| Air, Confined: | 55.5°C KI Test: | | |
| Impulse | | | |
| | Minutes | 60+ | |
| Under Water: Peak Pressure | <u>_34.5°C Heat Test:</u> | Minutor | |
| Impulse | Salmon Pink | <u>Minutes</u> 20 | |
| Energy | Red Fumes | 25 | |
| | Explodes | 300+ | |
| Underground: | 40-Hour Hydrolysis Test: | | |
| Peak Pressure | % hno ₃ | 5.07 | |
| Impulse | <u>'eat of:</u> | - 1 | |
| Energy | | | |
| | Combustion, cal/gm | 2960 | |
| | Explosion, cal/gm Gas Volume, cc/gm | 900 8 2 8 | |
| | | 838 | |
| | | | |

Preparation:

Polyvinyl alcohol is mixed with acetic anhydride. The mixture is cooled to $-5^{\circ}C$ and the nitric acid is added slowly while the mass is being stirred. The temperature is controlled by the rate of acid addition so that when all the acid has been added the temperature does not rise above $20^{\circ}C$.

When the nitration is complete, the mixture is drowned by allowing a fine stream of the syrupy liquid to flow from the nitrator and mix intimately with a large stream of water. This causes the product to precipitate in a fine state.

The finely divided precipitate is purified by boiling in frequent changes of water.

Origin:

The first preparation of polyvinyl nitrate was reported in 1929 by solution of polyvinyl alcohol in concentrated sulfuric acid and treatment with nitrating acid at a temperature not over 50° C. (German Patent 537,303). Later patents issued relative to polyvinyl nitrate included U. S. Patent 2,118,487 (1938) and German Patent 737,199 (1943).

| Composition: | · · · · · · · · · · · · · · · · · · · | Molecular Weight: | 230 |
|---|---------------------------------------|--|--------------------|
| RDX Gulf Crown E Oil | 85 15 | Oxygen Balance: O, % CO % | -70 -35 |
| | | Density: gm/cc Hand tamped | 1.37 |
| | | Melting Point: "C | |
| C/H Ratio | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | 53 | Boiling Point: °C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 13 25 | Refractive Index, n ^D ₂₀ n ^D ₂₃ n ^D ₃₀ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| Steel Shoe | Unaffected | cc/40 Hrs, at 90°C | |
| Fiber Shoe | Unaffected | 100°C | 0.34 |
| Rifle Bullet Impact lest: Trials | | 120°C | 0.56 |
| % | | 135°C | |
| Explosions 0 Portiats 0 | | 150°C | |
| Portials 0 Burned 0 | | 200 Gram Bomb Sand Test: | |
| Unaffected 100 | | Sand, gm | 40.1 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) | | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate | |
| 1 5 Decomposes; no val | ue obtained | | 0.20 |
| 10 | | Tetryl | 0.20 |
| 15 | | ,. | |
| 20 | | Ballistic Mortar, % TNT: (a) | 118 |
| 75% | | - Traurl Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | | Plate Dent lest: (b) Method | В |
| 100°C Heat Test: | | - | Hand tamped |
| % Lass, 1st 48 Hrs | 0.03 | Confined | No |
| % Loss, 2nd 48 Hrs | 0.04 | Density, g m/cc | 1.37 |
| Explosion in 100 Hrs | None | Brisance, % TNT | 85 |
| Flammability Index: | | Detonation Rate: Confinement | None |
| Hygroscopicity: % 30 ⁰ C, 90% RH | 0.04 | Condition I Charge Diameter, in. | Hand tamped 1.0 |
| Volatility: | | Density, gm/cc Rate, meters/second | 1.37 7390 |

RIPE

| | Fragmentation Test: | | Shaped Charge Effectiveness, TNT $=$ 100: | | |
|---|-----------------------|--|---|--|--|
| 90 mm HE, M71 Projectile, Lot WC | C-91: | Glass Canes Steel C | lones | | |
| Density, gm/cc | 1.36 | Hole Volume | | | |
| Chorge Wt, Ib | 1.766 | Hole Depth | | | |
| Tatol Na. of Fragments: | | Calar: | White | | |
| For TNT | 703 | | WIII CE | | |
| For Subject HE | 592 | Principol Uses: Plastic demolitic | on explosive | | |
| 3 inch HE, M42A1 Projectile, Lot K | C-5: | | | | |
| Density, gm/cc | 1.42 | | | | |
| Chorge Wt, ib | 0.756 | | | | |
| Total Na. of Frogments: | | Method of Looding: Hand | tamped | | |
| For TNT | 514 | • | L | | |
| For Subject HE | 501 | Looding Density: gm/cc | 1.37 | | |
| ragment Velocity: ft/sec | | | | | |
| At 9 ft At 25½ ft | 2650 2 3 70 | Storage: | | | |
| Density, gm/cc | 1.395 | Method | Dry | | |
| lost (Relative to TNT); | | | Class 9 | | |
| Air: | | Compatibility Group | Group I | | |
| Peak Pressure | | None at 85°C in 3 Exudation None at 95°C in 1 | 30 hrs | | |
| Impuise Energy | | Exudatian None at 95°C in I Exudes at 105°C i | in 48 hrs | | |
| | | Origin: | <u> </u> | | |
| Air, Confined: Impulse | | | | | |
| | | RIPE, a mechanical mixture of Crown E Oil, was developed in th | | | |
| Under Woter: Peak Pressure | | during World War II. | | | |
| Impulse | | References:68 | | | |
| Energy | | (a) L. C. Smith and E. G. Eys <u>Testing of Explosives</u> , Part III | ster, <u>Physical</u> - Miscellaneo | | |
| Underground: Peok Pressure | | Sensitivity Tests; Performance 1 port No. 5746, 27 December 1945. | | | |
| Impulse | | (b) D. P. MacDougall, <u>Methods</u> <u>Testing</u> , OSRD Report No. 803, 11 | August 1002 | | |
| Energy | | | | | |
| Preparation: | | (c) Also see the following Pi Technical Reports on RIPE: 1713, | catinny Arsen | | |
| RIPE is manufactured by si mixing of RDX in oil. | mple mechanical | recumical heports on RIFE: 1/13, | , 1097 and 171 | | |

 68 See footnote 1, page 10.

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| Composition: | Molecular Weight: (AgN ₃) 150 | | |
|--|--|--|--|
| % N 28.0 Ag 72.0 | Oxygen Balance:COL %CO % | | |
| Ag-N=N≝N | Density: gm/cc Crystal 5.1 | | |
| C/H Ratio | Melting Point: °C (a) 251 Decomposes rapidly above melting point to Freezing Point: "C silver and nitrogen. | | |
| Impact Sensitivity, 2 Kg Wt: | Boiling Point: °C | | |
| Bureau of Mines Apparatus, cm 6 Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 3 Sample Wt, mg 18 | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | | |
| Friction Pendulum Test:PA Small ApparatusSteel ShoeDetonatesFiber ShoeDetonates | Vacuum Stability Test: cc/40 Hrs, at 90°C | | |
| Rifle Bullet Impact Test: Trials % Explosions Portials | - 100°C 120°C 135°C 150°C | | |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sond (b) Hage Powder fuse 18.9 | | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 310 1 5 Explodes 290 10 15 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl Ballistic Mortar, % TNT: | | |
| 20 | , Trauzi Test, % Hg(ONC) ₂ (c) aa | | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method | | |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | | |
| Flammability Index: | Detonation Rate: Confinement Condition Charge Diameter, in. | | |
| Hygroscopicity: % (b) 25°C, 100% RH 0.04 | | | |
| Volatility: 75 ⁰ C, 24 hrs 0.00 | Density, gm/cc Rate, meters/second | | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 10$ | 00: |
|--|---|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel C Hole Volume Hole Depth | Cones |
| Total No. of Frogments: For TNT | Color: White | e <i>to</i> gray |
| For Subject HE | Principal Uses: Ini | itiators |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | | |
| Total No. of Fragments: For TNT | Method of Loading: Pres | ssed |
| For Subject HE | Loading Density: gm/cc Var | iable |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storage: | |
| Density, gm/cc | Method | W e t |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 |
| Air: | Compatibility Group | Group M |
| Peak Pressure Impulse | Exudation | None |
| Energy | | |
| Air, Confined: Impulse | Initiating Efficiency: Grams Required to Give Complete Initiation of TNT | (c) 0.02-0.05 |
| Under Water: Peak Pressure | Solubility in 100 gm Solvent at Room Temperature: | |
| Impulse Energy | <u>Solvent</u> Water (b) | <u>Grams</u> 0.006 |
| Underground: Peak Pressure Impulse Energy | Ammonium hydroxide Nitric acid Ether (b) Ethyl alcohol, 95% Acetone | Soluble Decomposes 0.017 0.006 0.015 |
| Explosive Power: (f) | Unaffected by water and CO ₂ . | (d) |
| Kilogram meters 192,000 % Mercury Fulminate 1.097 | Heat of: Explosion, cal/gm (c, d) Formation, cal/gm (e) | 452 67 . 8 |

Preparation:

 $NaN_3 + AgNO_3 \rightarrow AgN_3 + NaNO_3$

Prepare the following aqueous solutions:

- a. 5% NaN₃, sodium azide, 50 cc
- b. 25% AgNO₃, silver nitrate, 25 cc

The silver nitrate solution is placed in a 200 cc cdnductive rubber beaker equipped with a hard wood stirrer operated by an air motor. The sodium azide solution is placed in a separatory funnel fastened in a ring stand above the beaker containing the silver nitrate. A long cord (10 ft) is fastened to the stopcock of the separatory funnel so that the funnel can be emptied by remote control. The silver nitrate solution is now stirred very rapidly and the sodium azide is slowly run into the nitrate solution. Stirring is continued for 5 minutes. The contents of the beaker are filtered through folded filter paper and washed free of sodium azide and silver nitrate with distilled water.

Silver azide should be stored under water in a conductive rubber container. This preparation will yield approximately 7 grams.

The preparation should be conducted under a hood and behind a barricade. The product obtained by the above procedure has a very fine particle size, almost colloidal. Very fine silver azide is safer to handle and is just as efficient and stable as the large, coarse crystalline material (Ref b). When a thin film of fine silver azide is precipitated on mercury fulminate, tetryl, etc., these substances are as efficient weight for weight as pure silver azide (Ref g). White silver azide is less affected by light than mercury or lead azide (Ref h). Long colorless crystals which explode on breaking are obtained from ammonium hydroxide.

Origin:

Silver azide was first prepared in 1890-1 by T. Curtius (Ber 23, 3032; Ber 24, 3344-5) by passing hydrazoic acid (HN_2) into neutral silver nitrate solution. Taylor and Rinkenbach prepared pure "collocial" aggregates and showed its sensitivity depends upon its particle size (Army Ordnance 5, 824 (1925). Silver azide was found in a detonator of foreign ammunition for the first time in 1945 (Ref i).

References:⁶⁹

(a) A. R. Hitch, "Thermal Decomposition of Certain Inorganic Trinitrides," J Am Chem Soc <u>40</u>, 1195 (1918).

(b) C. A. Taylor and Wm. H. Rinkenbach, "Silver Azide: An Initiator of Detonation," Amy Ordnance, Vol 5, p. 824 (1925).

- (c) E. De W. S. Colver, High Explosives, London and New York, p. 527.
- (d) A. Stettbacher, Spreng u. Schlesstoffe, Rascher, Zurich, p. 97 (1948).
- (e) A. Marshall, Explosives, 2nd Ed, Vol II, p. 767, London.
- (f) A. Stettbacher, Z ges Schiess-Sprengstoffw 10, pp. 193-214 (1915).

⁶⁹See footnote 1, page 10.

Silver Azide

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(g) F. Blechta, Chim et Ind Special No. 921-5 (June 1933); C. A. 28, 646.

(h) L. Wohler and W. Krupko, Berichte <u>46</u>, 2047-2050 (1913).

(i) F. G. Haverlak, Examination of 120/45 MM HE Shell. Italian (FMAM-464), PATR No. 1515, 10 April 1945.

| Composition: | Molecular Weight: (C ₂ H ₈ N ₁₀ 0) 188 | | |
|--|---|--|--|
| % C 12.8 H 4.3 II // | Oxygen Balance: CO ₂ % CO % | | |
| C-NH-NH-N = N-C | Density: gm/cc At 3000 psi 1.05 | | |
| o 8.5 ^{NH} 2 NH-NH-NO | Melting Point: "C Explodes 140-1 60 | | |
| C/H Ratio 0.068 | Freezing Point: "C | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 7 | Boiling Point: "C | | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in.2; (8 oz wt) 8 Sample Wt, mg | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C | | |
| Rifle Bullet Impact Test: Trials % Explosions Partials | 100°C 120°C 135°C 150°C | | |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand gm Black powder_fuse 4.0 | | |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 160 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate 0.40 Lead Azide Tetryl | | |
| 15 20 | Ballistic Mortar, % TNT: | | |
| | Trauzi Test, % TNT: (a) 61 | | |
| 75°C International Heat Test:% Loss in 48 Hrs0.5 | Plate Dent Test: Method | | |
| 100°C Heat lest: | Condition | | |
| % Loss, 1st 48 Hrs 23.2 | Confined | | |
| % Loss, 2nd 48 Hrs 3.4 | Density, gm/cc | | |
| Explosion in 100 Hrs None | Brisance, % TNT | | |
| Flammability Index: | Detonation Rate: Confinement Condition Charge Diameter, in. | | |
| Hygroscopicity: % 30 ^o C, 90% RH 0.77 | | | |
| Volatility: | Density, gm/cc Rate, meters/second | | |

| ragmentation Test: | Shaped Charge Effectiveness, TNT = 10 |)0: |
|---|---|-------------------------------|
| 90 mm HE, M71 Projectile, Lot WC-91: | Glass Cones Steel C | ones |
| Density, gm/cc | Hole Volume | |
| Charge Wt, ¹ b | Hole Depth | |
| Total No. of Fragments: | Color: Pale | yellow |
| For TNT | | |
| For Subject HE | Principal Uses: Priming compositi detonators | ons and |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | detonators | |
| Density, gm/cc | | |
| Charge Wt, Ib | | |
| Total No. of Fragments: For TNT | Method of Loading: | Pressed |
| For Subject HE | Loading Density: gm/cc A t 3000 psi 1.0 | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft | Storoge: | |
| Density, gm/cc | Method | Wat |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 |
| | Compatibility Group | Group M |
| Air: Peak Pressure | | • • |
| Impulse | Exudation | |
| Energy | | |
| Air, Confined: | Solubility: | |
| Impulse Under Water: | Practically insoluble in wat acetone, ether, benzene, carbon or ethylenedichloride. | er, alcohol, tetrachlorido |
| Peak Pressure Impulse | Sensitivity to Electrostatic Discharge, Joules: | (b) |
| Energy | Unconfined Confined | 0.010 0.012 |
| Underground: Peak Pressure | Heat of: | |
| Impulse Energy | Explosion, cal/gm Gas Volume, cc/gm | 658 1190 |
| | Initiating Efficiency: | |
| | Tetracene is not efficient in high explosives. | n initiating |

Tetracene

Preparation:

(Rinkenbach and Burton, Amy Ordnance 12, 120 (1931)).

Tetracene is prepared by dissolving 5 gms of aminoguanidine dinitrate in 30 cc of water, cooling to 0° C and mixing with a solution of 2.5 gms of sodium nitrate in 15 cc of water. The temperature is maintained at about 10° C and 0.5 gm of acetic acid is added. The tetracene separates out and is washed with water, alcohol and ether. It is then dried.

Tetracene may also be prepared by placing aminoguanidine sulphate and sodium nitrite in a large beaker and adding water heated to 30° C. The heat of reaction causes the mixture to boil; after standing for two or three hours the separated tetracene is filtered off, washed thoroughly and dried.

Oriain:

Tetracene was first prepared in 1910 by Hoffman and Roth (Ber $\frac{43}{2}$, 682) who also studied its chemical reactions and determined. its structure (Hoffman et al, Ber $\frac{43}{2}$, 1087, 1866 (1910); Ber $\frac{44}{2}$, 2496 (1911); and Ann 380, 131 (1911)). W. H. Rinkenbach and O. Burton made an extensive study of tetracene and described its manufacture and explosive properties (Army Ordnance 12, 120 (1931)).

Destruction by Chemical Decomposition:

Tetracene is decomposed by adding it to boiling water and continuing boiling for some time to insure complete decomposition.

References: 70

(a) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III</u> - <u>Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, <u>OSRD Report No.</u> 5746, 27 December 1945.

(b) F. W. Brown, D. H. Kusler and F. C. Gibson, <u>Sensitivity of Explosives to Initiation</u> by Electrostatic Discharges, U. S. Dept of Int, Bureau of Mines, RI 3852, 1946.

(c) Also see the following Picatinny Arsenal Technical Reports on Tetracene:

| <u>o</u> | <u>1</u> | <u>3</u> | 4 | <u>7</u> | <u>8</u> | <u>9</u> |
|----------|----------|----------|----------------|----------|----------|-------------|
| 1450 | 11 | 453 | $1104 \\ 2164$ | 407 | 318 | 859 2179 |

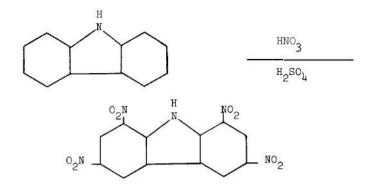
⁷⁰See footnote 1, page 10.

| Composition: | Molecular Weight: $(C_{12}H_5N_5O_8)$ 347 |
|--|--|
| $%$ O_2N H NO_2 c 41.6 | Oxygen Balance; O, % -85 CO % -30 |
| H 1.4 \circ_2 N N \circ_2 | Density: gm/cc |
| N 20.0 | Melting Point: °C Pure 1,3,6,8-isomer 296 |
| 0 37+0 C/H Ratio 1.032 | Freezing Point: °C |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 100+ Sample Wt 20 mg | Boiling Point: °C Refractive Index, n ^o ₂₀ |
| Picatinny Arsenal Apparatus, in. 18 Sample Wt, mg 14 | n ^D ₂₅ |
| Friction Pendulum Test: Steel Shoe Unaffected Fiber Shoe Unaffected | Vacuum Stability Test: cc/40 Hrs, at 90°C |
| Rifle Bullet Impact Test: Trials % Explosions Particls | 100°C 0.2 120°C 0.2 135°C 150°C |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm 41.3 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 5 Decomposes 470 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide 0.20 Tetryl 0.25 |
| 15 20 | Ballistic Mortar, % TNT: |
| | Trauzi Test, % TNT: |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method |
| 100°C Heat Test: % Loss, 1st 48 Hrs 0.15 % Loss, 2nd 48 Hrs 0.05 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT |
| Flammability Index: | Detonation Rate: Confinement |
| Hygroscopicity: % 30 ⁰ C, 90% RH 0.01 | Condition Charge Diameter, in. |
| Volatility: | Density, gm/cc Rate, meters/second |

Tetranitrocarbazole (INC)

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | | |
|---|---|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel C Hole Volume Hole Depth | ones | |
| Total No. of Fragments: For TNT | Color: Lig | ht yellow | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Component of igni pyrotechnic comp | ter and ositions | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: | Pressed | |
| Fragment Velocity: ft/sec | Loading Density: gm/cc | | |
| At 9 ft At 25 ½ ft Density, gm/cc | Storage: | - | |
| | Method | Dry | |
| Blest (Relative to TNT): | Hazard Class (Quantity-Distance) | Class 9 | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | | |
| Air, Confined: Impulse | Solubility in Water, gm/100 gn (%), at: | | |
| Under Water: | 95°C | 0.10 | |
| Peak Pressure Impulse | Qualitative Solubilities: | C - 11-11+ - | |
| Energy | <u>Solvent</u> Nitrobenzene | <u>Solubility</u> Very soluble | |
| Underground: Peak Pressure Impulse Energy | Acetone Benzene Chloroform Carbontetrachlori de Ether Ether, petroleum | Soluble Insoluble Insoluble Insoluble Insoluble Insoluble | |
| | | | |

Preparation:



<u>Sulfonation</u>: Fifty-six gms of carbazole is dissolved in 320 gms of $H_2SO_{\rm h}$ (96%, specific gravity 1.84). The solution is agitated during the addition of the carbazole and the temperature maintained at 25°-35°C. After the addition of the carbazole is completed, the agitation is continued and solution completed by raising the temperature to $80^{\circ}-85^{\circ}C$ and maintaining this temperature \notin or one hour. The sulphate is now cooled to $20^{\circ}C$.

<u>Nitration</u>: The sulfonate solution is slowly added to 168 gms of HNO_3 (Plant grade specific gravity 1.525 at 15°C) maintaining the temperature at 30° to 50°C. (Time required - 1 hour 25 minutes). The temperature is then gradually raised to 70° to 75°C and maintained for one hour after which the temperature is raised to 85° to 90°C and held for one hour, then lowered to room temperature before drowning.

<u>Drowning:</u> The nitration mixture is drowned by pouring it into 2 to 3 volumes of ice and water.

<u>Filtering</u>: The separated light yellow product is filtered on a Buchner Funnel and washed with water twice to remove most of the acid.

<u>Purification</u>: The TNC is placed in hot water $(95^{\circ} \text{ to } 100^{\circ}\text{C})$ and boiled for five to ten minutes with rapid agitation, allowed to settle then filtered and washed once. This procedure is repeated twice, making a total of three "boilings." The final wash is acid free.

Drving: The TNC is spread in a thin layer and dried at 100° to 110°C for four hours.

Yield: 73.3%.

Melting Point of TNC as prepared: 280°C (compares to 296°C for pure 1,3,6,8-isomer in preceding data).

Origin:

The preparation of Tetranitrocarbazole (TNC) was first reported in 1880 by C. Graebe (Ann 202, 26 (1880)) who nitrated carbazole with 94% nitric acid. Similar procedures were followed by R. Escales (Ber <u>37</u>, 3596 (1904)) and P. Zierch (Ber <u>42</u>, 3800 1909)). However, G. L. Ciamician and P. P. Silber observed the formation of four isomeric TNC's when acetyl carbazole was treated with fuming nitric acid (Gazz chim ital <u>12</u>, 272 1882)). In 1912 and 1913 patents were issued to the dyestuff manufacturer, Casella and Company, covering the preparation of polynitrocarbazoles (German Patent 268, 173 and French Patent 464, 538). The Casella process of

Tetranitrocarbazole (TNC)

preparing polynitrocarbazoles by dissolving carbazole in sulfuric acid and treating the solution of sulfonic acids with strong nitrating agents is essentially the process used today in the United States. The crude product, thus prepared, contains principally 1,3,6,8-TNC (W. Borsche and B. G. B. Scholten Ber 50, 596 (1917) and about 10% of the 1,2,6,8-TNC isomer (D. B. Murphy et al J Am Chem Soc $\overline{75}$, 4289 (1953). TNC was used in explosives by the Germans during World War II.

References: 71

(a) D. B. Murphy, F. R. Schwartz, J. P. Picard and J. V. R. Kaufman, "Identification of Isomers Formed in the Nitration of Carbazole," J Am Chem Soc, <u>75</u>, 4289-4291 (1953).

(b) S. Livingston, <u>Preparation of Tetranitrocarbazole</u>, PA Chemical Research Laboratory Report No. 136,330, 11 April 1951.

(c) D. B. Murphy et al, Long Range Basic Technical Research Leading to the Development of Improved Ignition Type Powders - The Chemistry of Tetranitrocarbazole, PA Memorandum Report No. 22, 2 September 1952.

(d) S. Livingston, Development of Improved Ignition Type Powders, PATR No. 2267 July 1956.

(e) Also see the following Picatinny Arsenal Technical Reports on Tetranitrocsrbazole:

| <u>0</u> | 2 | 3 | <u>4</u> | <u>_7</u> |
|----------|------|------|----------|--------------|
| 2180 | 1802 | 1973 | 1984 | 1647 1937 |

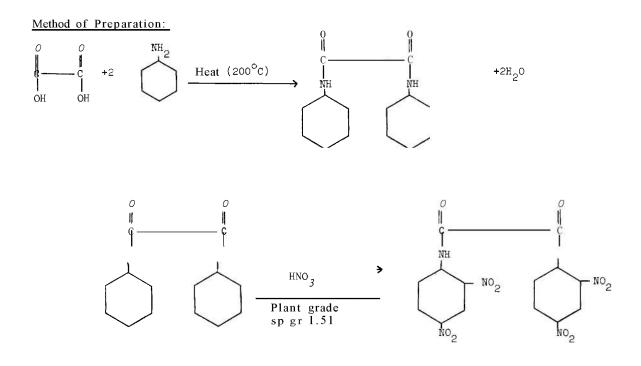
⁷¹See footnote 1, page 10.

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| Composition: | Molecular Weight: $(C_{14}H_8N_6O_{10})$ 420 | | |
|---|--|--|--|
| С 40.0 С О С О С О С О С О С О С О С О С О С | Oxygen Balance: -84 CO, % -31 | | |
| N 20.0 | Density: gm/cc | | |
| | Melting Point: °C Decomposes 313 | | |
| C/H Ratio 0.735 NO2 NO2 | Freezing Point: "C | | |
| Impact Sensitivity, 2 Kg Wt: | Boiling Point: "C | | |
| Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 30 Sample Wt, mg 11 | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | | |
| Friction Pendulum Test: Steel Shoe Unaffected | Vacuum Stability Test: cc/40 Hrs, at | | |
| Fiber Shoe Unaffected | 90°C | | |
| Rifle Bullet Impact Test: Trials % Explosions | - 100°C 120°C 0.11 135°C | | |
| Partials | 150°C | | |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm 16.3 | | |
| Explosion Temperature: "C Seconds, 0. i (no cap used) 1 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate | | |
| 5 392 | Lead Azide 0.20 | | |
| 10 | Tetryl 0.25 | | |
| 15 20 | Ballistic Mortar, % TNT: | | |
| | - Trauzi Test, % TNT: | | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method | | |
| 100°C Heat Test: | Condition | | |
| % Loss, 1st 48 Hrs 0.07 | Confined | | |
| % Loss, 2nd 48 Hrs 0.00 | Density, gm/cc Brisance, % TNT | | |
| Explosion in 100 Hrs None | | | |
| Flammability Index: | Detonation Rate: Confinement | | |
| Hygroscopicity: % 30 ⁰ C, 90% RH Trace | Condition Charge Diameter, in. | | |
| Volatility: | Density, gm/cc Rate, meters/second | | |

2,4,2',4'-Tetranitro-oxanilide (INO)

| Frogmentation lest: | Shaped Charge Effectiveness, $TNT=100$: | | |
|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | | |
| Totol No. of Fragments: For TNT | Color: Light yellow | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: Component of black powder type and pyrotechnic compositions | | |
| Total No. of Fragments: ForTNT For Subject HE | Method of Loading: Pressed and extruded compositions | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc | Loading Density: gm/cc Storage: | | |
| Blast (Relative to TNT): | Method Dry Hazard Class (Quantity-Distance) Class 9 | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | | |
| Air, Confined: Impulse | Solubility, gm/100 cc Solvent, in: <u>o</u> c <u>%</u> | | |
| Under Water: Peak Pressure Impulse | Water100<0.10 | | |
| Energy Underground: Peak Pressure Impulse Energy | SolventSolubilityEthyl alcoholInsolubleBenzeneInsolubleButyl acetateInsolubleCarbontetrachlorideInsolubleEthyl etherInsolubleAcetic acidSolubleNitric acidSolubleCaustic potashSolubleDimethyl formamideVery soluble | | |



Oxanilide:

Two parts of oxalic acid are mixed with one part of aniline in a round bottom flask. The mixture is stirred and heated until the reaction is complete as evidenced by the cessation of effervescence. The mass is cooled to room temperature, poured into several volumes of water $(21^{\circ}-24^{\circ}C)$, filtered on a Büchner funnel and washed free of oxalic acid with water and then washed free of aniline with acetone. The oxanilide is air dried to remove the acetone and then dried at $100^{\circ}-110^{\circ}C$.

Tetranitro-oxanilide (TNO):

A 5 liter round bottom flask is equipped with a stirrer of a type which will produce a downward "swirl." The flask is surrounded with a water jacket for hot and cold water. Fifteen hundred grams (1.5 kilograms) of 98% plant grade nitric acid is placed into the flask. Five hundred (500) grams of oxanilide is slowly added to the acid under rapid agitation while the temperature is maintained below 40° C. After the addition of the oxanilide is completed ($2\frac{1}{2}$ -3 hrs), the agitation is continued 10-15 minutes. The temperature is then raised to 80° C over a period of one hour and maintained at 80° -85°C for 3 hours. The acid slurry is then cooled to room temperature and drowned by pouring over cracked ice. The product is filtered on a Buchner funnel and washed with water until it is almost acid free. The filter cake is placed in a beaker and sufficient water added to form a "slurry." Live steam is run into the "slurry" under agitation for 10 minutes. The slurry is filtered and the residue washed. The latter treatment of the "slurry" is repeated until the wash water is found to be neutral to

2,4,2',4'-Tetranitro-oxanilide (TNO)

litmus paper. The TNO is washed with alcohol, then acetone, air dried and finally dried at $100^{\circ}-110^{\circ}C$.

Yield = 90% to 97.546 of theoretical.

Origin:

A. G. Perkin in 1892 obtained tetranitro-oxanilide directly by heating a solution of finely powdered oxanilide in nitric acid. He also obtained the same compound by the action of a cooled mixture of nitric and sulfuric acids on oxanilide and precipitating the product by pouring the solution into water (J Chem Soc $\underline{61}$, 460 (1892).

References: 72

(a) S. Livingston, Development of Improved Ignition Type Powders, PATR No. 2267, July 1956.

(b) D. Dubrow and J. Kristel, <u>Substitution of Tetranitro Oxanilide and Hexanitro Oxanilide</u> for Tetranitro Carbazole, PA Pyrotechnic Research Laboratory Report 54-TF 1-88, 20 December 1954.

⁷²See footnote 1, page 10.

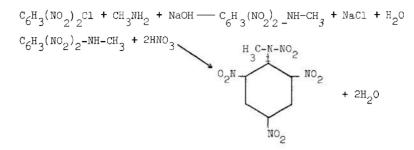
| Composition: | | Molecular Weight: (C7H5N508) | 287 |
|---|------------------------|--|--------------------|
| $^{\%}$ C 29.3 H 1.7 H 0 ₂ N | -NO2 | Oxygen Balance: CO ₂ % CO % | -47 - 8 |
| N 24.4 | 2 | Density: gm/cc Crystal | 1.73 |
| 0 44.6 | | Melting Point: "C | 130 |
| C/H Ratio 0,420 NO | 2 | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 26 8 18 | Boiling Point: °C Refractive Index, n ^D ₂₀ n ^D ₂₅ | |
| Friction Pendulum Test: | | n ^D ₃₀ | |
| Steel Shoe Fiber Shoe | Crackles Unaffected | | |
| Rifle Bullet Impact Test: Trials % | | 120°C | 0.3 1.0 |
| Explosions 13 Partials 54 | | 135°C 150°C | 11+ |
| Burned 10 Unaffected 23 | | 200 Gram Bomb Sand Test: Sand, gm | 54.2 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 340 1 314 5 Ignites 257 10 238 15 236 20 234 | | Sensitivity to Initiation; Minimum Detonating Charge, gm Mercury Fulminate Lead Azide <u>Tetry:</u> <u>*Alternative initiating charges.</u> Bgllistic Mortar, % TNT; (a) | 0.20* 0.10* |
| 20 - 34 | | Trourl Test. % TNT; (b) | 125 |
| 75°C International Heat Test: % Los s in 48 Hrs | 0.01 | Plate Dent lest: (c) Method A | В |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | 0.1 0.0 None | Condition Pressed Confined Yes Density, gm/cc 1.50 1.5 Brisance, % TNT 116 115 | |
| Flammability Index: | 244 | Detonction Rate: Confinement | None |
| Hygroscopicity: % 30°C, 90% RH | 0.04 | Condition Charge Diameter, in. | Pressed |
| Volatility: 25 ^o c | 0.00 | Density, gm/cc Rate, meters/second | 1.71 7850 |

| Booster Sensitivity lest: | (d) | Decomposition Equation: | $\binom{(g)}{10^{15.4}}$ $\binom{(h)}{10^{12.9}}$ |
|---|----------------------------------|--|---|
| Tetryl, gm | 100 | (Z/sec) | |
| Wax, in. for 50% Detonation | 2.01 | Heat, kilocalorie/mole (AH, kcol/mol) | 38.4 34.9 |
| Wax, gm | | Temperature Range, °C | 211-260 132-164 |
| Density, gm/cc | I.58 | Phase | Liquid Liquid |
| | | | |
| Heat of: | 2025 | Armor Plate Impact Test: | |
| Combustion, col/gm | 2925 | | |
| Explosion, col/gm | 1080-1130 760 | 60 mm Mortar Projectile: | |
| Gas Volume, cc/gm | • | 50% Inert, Velocity, ft/ | sec |
| Formation, col/gm Fusion, sol/em_o(e) | -14 22.2 | Aluminum Fineness | |
| Temperatúre, C | 127 | 500-16 General Purpose Bo | mbs; |
| Specific Heat: col/gm/°C | (e) | Plate Thickness, inches | |
| -100 | 0.182 | Flate HILCKIESS, INCHES | |
| - 50 | 0.200 | 1 | |
| 0 50 | 0.212 0.223 | 11/4 | |
| 100 | 0.236 | 11/2 | |
| | | 13⁄4 | |
| Burning Rate: | | | |
| cm/sec | | Bomb Drop Test: | |
| Thermal Conductivity: (f) col/sec/cm/°C 5.81 x 10 ⁻¹ 4 6.83 x 10 ⁻¹ 4 | at 1.394 gm/cc at 1.528 gm/cc | T7, 2000-Ib Semi-Armor-Pi | iercing Bomb vs Concrete: |
| Coefficient of Expansion: | | Max Safe Drop, ft | |
| Linear, %/°C | | 500-1b General Purpose Bo | omb vs Concrete: |
| | | | |
| Volume, %/°C | | Height, ft | |
| Hardness, Mohs' Scale: | | Trials | |
| | | Unaffected | |
| Young's Modulus: | | Low Order | |
| E, dynes/cm ² | | High Order | |
| E, Ib/inch² | | 1000-lb General Purpose B | omb vs Concrete: |
| Density, gm/cc | | | |
| | | Height, ft | |
| Compressive Strength: Ib/inch ² | | Trials | |
| | | Unaffected | |
| Vapor Pressure: | | Low Order | |
| "C mm Mercury | / | High Order | |
| | | | |
| | | | |
| | | | |
| | | | |

| Fragmentation lest: | | Shaped Charge I | Effectiveness, T | NT = 100 | | |
|--|-----------------|--|--------------------------|------------------------|--------------|-----|
| 90 mm HE, M71 Projectile, Lot WC-91 | | | Glass Cones | Steel Cor | les | |
| Density, gm/cc | 1.58 | Hole Volume | | | | |
| Charge Wt, Ib | 2.052 | Hole Depth | | | | |
| | 2,002 | There Depin | | | | |
| Total No. of Fragments: | | Color: | | Light | yellow | |
| For TNT | 70 3 | | | ÷ | | _ |
| For Subject HE | 864 | Principal Uses: | | | | |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | | | sive mixtu blasting c | | mators, a | ant |
| Density, gm/cc | 1.62 | | brasting d | արե | | |
| Charge Wt, Ib | 0.848 | | | | | |
| | | | | | | |
| Total No. of Fragments: | | Method of Load | lina: | | Pressee | 1 |
| For TNT | 51 ⁴ | | | | | |
| For Subject HE | 605 | | | _ | | |
| | | Loading Density | :gm/cc | See belo | DW . | |
| Fragment Velocity: ft/sec | | | | | | |
| At 9 ft At 25½ ft | | Storage: | | | | |
| Density, gm/cc | | -longe. | | | | |
| | | Method | | | Dry | |
| | | | | | | |
| Blast (Relative to TNT): | | Hazard Class (Quantity-Distance) Class | | |) | |
| | | Compatibility | Group | | Group | 1 |
| Air: | | Compatibility | Gloup | | Group | ∎, |
| Peak Pressure | | Exudation | D | oes not e | kude at 6 | .J. |
| Impulse _ | | Extraction | | | | 2 . |
| Energy | | | | | | |
| Air, Confined: | | Loading Densi | <u>ty:</u> gm/ee | | | |
| Impulse | | Cast 1.62 | Pressed | | 1.03 | |
| | | Cast 1.02 | riesseu | psix | 10 | |
| Under Water: | | 0 3 | 5 10 1.47 1.57 | 12 | 15 | 50 |
| Peak Pressure | | 0.9 1.40 | 1.47 1.57 | 7 1.60 | 1.63 | 167 |
| Impulse | | | 30 | | | |
| Energy | | | 1.73 | _ | | |
| Underground: | | Effect of Ten | nnerature on | | (;) | |
| Peak Pressure | | Rate of Deton | | | (07 | |
| Impulse | | | • | | | |
| Energy | | 16 hrs at, | °C | - 54 | 21 | |
| | | Density, g Rate, m/se | m/ee | - 1.52 71.50 | 1.53 7170 | |
| | | | - | 1 4 7 0 | 1410 | |
| | | | | | | ! |
| | | | | | | |
| | | | | | | |
| | | | | | | |

Preparation:

(Manufacture of Tetryl by Dinitromonomethylaniline Process, Wannamaker Chemical Co., Inc.)



To a solution of 202.5 gm dinitrochlorbenzene in 200 cc benzene, at 75° C with good agitation, in 15 to 20 minutes, add 112 gm of 30% aqueous monomethylamine. Then add 129 gm of 31%aqueous sodium hydroxide, in 15 to 20 minutes, at such a rate as to cause refluxing; continue agitation for 3 hours at 70° C. The mixture is concentrated to a liquid temperature of 101° - 102° C, cooled, filtered and the precipitate washed with distilled water until the washings give no test with silver nitrate, dried at 60° C (melting point 167.2° C).

The dinitromethylaniline is nitrated to tetryl by solution of it in 88% sulf'uric acid (197 gm nitroaniline/1190 gm sulfuric) at 25°C, followed by addition of nitric acid. The process is carried out so that the water content remains at 16%. Solution (per 197 gm nitroaniline) requires 5 to 10 minutes, nitration, by addition of the sulfuric acid solution to nitric acid, about 1 hour at 30°C, plus 48 minutes at 50° to 55°C at the end. The mixture is then cooled to 20°C and filtered. The tetryl is dumped into 1 liter water, washed 2 or 3 times with 200 cc cold water, and then stirred 10 to 15 minutes at 50°C with 500 cc water, filtered warm and then washed with water until the washings are neutral to methyl orange. The tetryl dried to constant weight at 70°C weighs about 270 gm.

Tetryl filtered from an acid containing 87% sulfuric acid (or more) -13\% water, at $40^{\circ}C$ (or over) may fire in 30 minutes to 1 hour and 30 minutes, if not drowned in water. A safe nitration procedure, even on plant scale involves:

1. The concentration of sulfuric in the spent acid is maintained at a low level (approx 80/1.8/18.2 sulfuric/nitric/water).

- 2. Nitration maximum temperature is 50°C.
- 3. The slurry is cooled to 35°C before filtration.
- 4. Filtration time prior to drowning, is minimized (15 minutes maximum).

The crude tetryl produced is recrystallized to remove impurities and occluded acid and to control its granulation.

| Sensitivity of tetryl electrostatic | discharge, joules; | <u>through 100 mesh:</u> (| (i) |
|-------------------------------------|--------------------|----------------------------|-----|
|-------------------------------------|--------------------|----------------------------|-----|

| Uncc Conf | onfined fined | | 0.007 4.4 | | | | | | |
|---------------------------------|---|----------------------|----------------------------------|----------------------------------|------------------|-----------------------------|----------------------------------|---------------------------------|---|
| <u>Solubility</u> | of tetryl, | grams in 10 | 0 grams (%) | of: | | | | | |
| Wa | ter | Carbo | on tetrachlo | ride | | Eth | ier | 95 | Se Alcohol |
| <u>°c</u> | <u>%</u> | <u>°c</u> | | % | | <u>°c</u> | <u>%</u> | <u>00</u> | <u>%</u> |
| 0 20 40 80 100 | 0.0050 0.0075 0.0110 0.0810 0.184 | 0 20 40 60 | (| 0.007 0.015 0.058 0.154 | | 0 10 20 30 | 0.188 0.330 0.418 0.493 | 0 10 20 30 50 75 | 0.320 0.425 0.563 0.76 1.72 5.33 |
| <u>Chlo</u> | roform | <u>Carbon</u> d | sulfide | Ethy1 | Lene dic | hloride | | Aceton | e |
| <u>°c</u> | <u>%</u> | <u>°c</u> | <u>%</u> | <u>°c</u> | | Z | <u>0</u> , | c | <u>%</u> |
| 0 20 40 60 | 0.28 0.39 1.20 2.65 | 0 10 20 30 | 0.009 0.015 0.021 0.030 | 25 75 | | 4.5 45 | 2 3 4 5 | | 75 95 116 138 |
| Trichlor | oethylene | Ethyl ac | etate | | Benzene | | | Toluer | ie |
| <u>°c</u> | <u>%</u> | <u>°c</u> | <u>%</u> | <u>°c</u> | | <u>%</u> | 0 | c | <u>%</u> |
| 0 20 40 60 80 86 | 0.07 0.12 0.26 0.67 1.50 1.76 | 20 | ~ 40 | 20 30 40 50 | | 7.8 10.0 12.5 16.0 | 2 | 0 | 8.5 |
| | | Xy | lene | | T | <u>TN</u> | | | |
| | | <u>°c</u> | <u>%</u> | | °C | K | | | |
| | | 20 30 40 50 | 3,3 4.4 5.4 6.0 | | 80 100 120 | 82 149 645 | | | |

Origin:

Tetryl was first described in 1879 by Michler and Meyer (Ber 12, 1792), van Romburgh and Martens studied its properties and proved its structure (Rec trav chim 2, 108 (1883); 6, 215 (1887); and Ber 19, 2126 (1886)). Tetryl was not used as an explosive until World War I.

Destruction by Chemical Decomposition:

Tetryl is decomposed by dissolving in 12 times its weight of a solution prepared from 1 part, by weight of sodium sulfite $(Na_2SO_2^*7H_2O)$ in 4 parts water. The sulfite solution may be heated to $80^{\circ}C$ to facilitate decomposition of the Tetryl.

References: 73

(a) L. C. Smith and E. G. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III</u> - <u>Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, OSRD Report No. 5746, 27 December 1945.

(b) Ph Naoum, Z ges Schiess---Sprengstoffw, pp. 181, 229, 267 (27 June 1932).

(c) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(d) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wex Mixtures as a Substitute for</u> Tetryl in Poosters, NOL Mamo 10, 303; 15 June 1949.

(e) C. A. Taylor and Wm H. Rinkenbach, "The Solubility of Trinitro-Phenylmethyl-Nitramine (Tetryl) in Organic Solvents," J Am Cham Soc 45, (1923) p. 104.

(f) E. Hutchinson, <u>The Thermal Sensitiveness of Explosives</u> The Thermal Conductivity of Explosive Materials, AC 2861, First Report, August 1942.

(g) R. J. Finkelstein and G. Gemow, <u>Theory of the Detonation Process</u>, NAVORD Report No. 90-46, 20 April 1947.

(h) M. A. Cook and M. T. Abegg, "Isothermal Decomposition of Explosives," University of Utah. <u>Ind Eng Chem</u> 1090-1095 (June 1956).

(i) J. W. Brown, D. H. Kusler and F. C. Gibson, <u>Sensitivity of Explosives to Initiation</u> by <u>Electrostatic Discharges</u>. U. S. Dept of Int, Bureau of Mines, R1 3852, 1946.

(j) W. F. McGarry and T. W. Stevens, <u>Detonation Rates of the More Important Military</u> <u>Explosives at Several Different Temperatures</u>, PAIR No. 2383, November 1956.

| <u>0</u> | <u>1</u> | <u>2</u> | 3 | <u>4</u> | د | 6 | I | 8 | 2 |
|--|--|---|---|---|--|---|---|---|---|
| 30 Goo 7770 810 1380 1350 1350 1400 1450 1450 1510 1510 | 11 361 381 621 861 1041 1261 1261 1431 1431 1431 1651 | 132 582 832 1192 1352 1372 1402 1452 1592 | 453 493 623 833 863 1113 1373 2053 2163 2233 | 84 144 294 314 694 774 784 874 1134 1164 1234 1264 2024 2204 | 65 195 425 525 625 635 925 1145 1285 1405 1585 1935 2105 2125 2205 | 266 556 986 1086 1126 1316 1416 1466 1466 1556 1636 1956 | 117 197 637 707 807 857 1047 1137 1287 1337 1367 14 37 1737 1797 1937 | 28 438 628 708 788 838 1418 1788 1828 1838 | 129 179 319 609 709 849 999 1029 1209 1209 1429 1489 1819 1969 |

(k) Also see the following Picatinny Arsenal Technical Reports on Tetryl:

⁷³See footnote 1, page 10.

| Composition: % | | Molecular Weight: | 274 |
|---|---------|--|----------------|
| Tetryl | 80 | Oxygen Balance: CO, % CO % | -52 -11 |
| TNT | 20 | Density: gm/cc Cast | 1.51 |
| | | Melting Point: °C | 68 |
| C/H Ratio | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | 28 | Boiling Point: °C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 9 17 | Refractive Index, N ^D ₂₀ N ^D ₂₅ N ^D ₃₀ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| Steel Shoe Fiber Shoe | | cc/40 Hrs, at 90°C | |
| Rifle Bullet Impact Test: Trials | | 100°C 120°C | 3.0 11+ |
| Explosions 0 | | 135°C 150°C | |
| Partials 20 Burned 0 | | 200 Gram Bomb Sand Test: | |
| Unaffected 80 | | Sand, gm | 54.0 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Ignites 290 | | Sen si tivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide | 0.22* 0.17* |
| 10 | | *Alternative initiating charges. | |
| 15 20 | | Ballistic Mortar, % TNT: | |
| | | Trauri Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | | Plate Dent Test: Method | |
| 100°C Heat lest: | | Condition | |
| % Loss, 1st 48 Hrs | 0.1 | Confined | |
| % Loss, 2nd 48 Hrs | 0.5 | Density, gm/cc | |
| Explosion in 100 Hrs | None | Brisance, % TNT | |
| Flammability Index: Will not continue | to burn | Detonation Rote: Confinement | |
| Hygroscopicity: % | 0.02 | Condition Charge Diameter, in. | |
| Volatility: | | Density, gm/cc Rate, meters/second | |

| Fragmentation Test: | Shaped Charge Effectiveness, TNT $=$ 100: | | | |
|--|---|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | | | |
| Total No. of Fragments: For TNT | Color: Light yellow to buff | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, lot KC-5: Density, gm/cc Charge Wt, lb Total No. of Fragments: | Principal Uses: Bursters, demolition blocks Method of Loading: | | | |
| For TNT For Subject HE | Loading Density: gm/cc | | | |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc | Storage: | | | |
| Blast (Relative to TNT): | Method Dry Hazard Class (Quantity-Distance) Class 9 | | | |
| Air: Peak Pressure Impulse Energy | Compatibility GroupGroupIExudationExudes at 65° C | | | |
| Air, Confined: Impulse | | | | |
| Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | | | | |

Tetrytol, 75/25

| Composition: | Molecular Weight: | 270 |
|---|---|----------------------------|
| % Tetryl 75 TNT 25 | Oxygen Balance: COୁ % CO % | -54 -12 |
| | Density: gm/cc Cast | 1.59 |
| | Melting Point: °C | 68 |
| C/H Ratio | Freezing Point: °C | |
| Impact sensitivity, 2 Kg Wt:Bureau of Mines Apparatus, cm28Sample Wt 20 mg28Picatinny Arsenal Apparatus, in.10Sample Wt, mg17 | Boiling Point: "C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| Friction Pendulum lest: Steel Shoe Cracks Fiber Shoe Unaffected | Vacuum Stability lest: cc/40 Hrs, at 90°C | |
| Rifle Bullet Impact lest:TrialsSectors0Partials30 | | 3.0 11+ |
| Burned 0 Unaffected 70 | 200 Gram Bomb Sand lest: Sand, gm | 53.7 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 Ignites 310 10 15 20 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide *Alternative initiating charges. Ballistic Mortar, % TNT: (a) Irauzl lest, % TNT: | 0.23* 0.19* 122 |
| 75°C International Heat lest: % Loss in 48 Hrs | Plate Dent Test: (b) Method B | В |
| 100°C Heat lest: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | ConditionCastConfinedNoDensity, gm/cc1.66Brisance, % TNT118 | Cast Yes 1.62 114 |
| Flammability Index: Will not continue to burn | Detonation Rate: Confinement | None |
| Hygroscopicity: % 0.03 | Condition Charge Diameter, in. | Cast 1.0 |
| Volatility: | Density, gm/cc Rate, meters/second | 1.60 7385 |

Tetrytol, 75/25

| Fragmentation Test: | | Shaped Charge Effectiveness, TNT = | 100: |
|---|----------------------------------|--|---|
| 90 mm HE, M71 Projectile, Lot WC-91 Density, gm/cc Charge Wt, Ib | 1.59 2.101 | Glass Cones Steel Hole Volume 127 Hole Depth 120 | Cones (d) |
| Total No. of Fragments: For TNT For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5 Density, gm/cc Charge Wt, Ib | 703 557 : 1.60 0.845 | Color: Light yell Principal Uses: Bursters, demol | ow to buff ition blocks |
| Total No. of Fragments: For TNT For Subject HE | 514 591 | Method of Loading: | Cast |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc Blast (Relative to TNT): | | Loading Density: gm/cc Storage: Method Hazard Class (Quantity-Distance) | 1.59 Dry Class 9 |
| Air: Peak Pressure Impulse Energy | | Compatibility Group Exudation | Group I Exudes at 65 ⁰ C |
| Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | | Eutectic Temperature, ^o C: gn Tetryl/100 gn TNT 67.5°C Booster Sensitivity Test: Condition Tetryl, gn Wax, in. for 50% Detonation Density, gm/cc | 67.5 54-82 (c) Cast 100 1.66 1.66 |

Tetrytol, 70/<u>3</u>0

| Composition: % | Molecular Weight: | |
|---|--|------------|
| Tetryl 70 | Oxygen Balance: CO, % CO % | -55 -13 |
| TNT 30 | Density: gm/cc Cast | 1.60 |
| | Melting Point: °C | 68 |
| C/H Ratio | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: | Boiling Point: °C | |
| Bureau of Mines Apparatus, cm28Sample Wt 20 mgPicatinny Arsenal Apparatus, in.11Sample Wt, mg18 | Refractive Index, n ^D ₂₀ n ^D ₂₃ | |
| Friction Pendulum lest: | Vacuum Stability lest: | |
| Steel Shoe Unaffected | cc/40 Hrs, at 90°C | |
| Fiber Shoe Unaffected | 100°C | 3.2 |
| Rifle Bullet Impact lest: Trials | 100 C | 11+ |
| % | 135°C | |
| Explosions 0 | 150°C | |
| Partiols 55 | 150 C | |
| Burned 0 | 200 Gram Bomb Sand lest: | 0 |
| Unaffected 45 | Sand, gm | 53.2 |
| Explosion Temperature: "C | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) 416 | Minimum Detonating Charge, gm | |
| 1 387 | Mercury Fulminate | 0.23* |
| 5 Ignites 320 | Lead Azide | 0.22* |
| 10 302 | Tetry *Alternative initiating charges. | |
| 15 289 | Ballistic Mortar, % TNT: (a) | 120 |
| 20 275 | Trauzi lest, % TNT: | |
| 75°C International Heat lest: | Plate Dent lest: (b) | |
| % Loss in 48 Hrs | Method | В |
| 100%0 Hast Is st | Condition | Cast |
| 100°C Heat lest: % Loss 1st 48 Hrs 0.1 | Confined | Yes |
| ,o | Density, gm/c c | 1.60 |
| % Loss, 2nd 48 Hrs 0.1 Explosion in 100 Hrs None | Brisance, % TNT | 117 |
| | Detonation Rate: | |
| Flammability Index: Will not continue to but | | None |
| - is not continue to but | Condition | Cast |
| Hygroscopicity: % 0.02 | Charge Diameter, in. | 1.0 |
| | Density, gm/cc | 1.60 |
| Volatility: | Rate, meters/second | 7340 |

<u>Tetrytol, 70/30</u>

| Fragmentation Test: | | Shaped Charge Effectiveness, TNT = 10 | 00: |
|---------------------------------------|-------------|---------------------------------------|-----------------------|
| 90 mm HE, M71 Projectile, Lot WC | C-91: | Gloss Cones Steel C | ones |
| Density, gm/cc | 1.60 | Hole Volume | |
| Charge Wt, Ib | 2.090 | Hole Depth | |
| Total No. of Fragments: | | Color: Light vel | low to buff |
| For TNT | 703 | | |
| For Subject HE | 840 | Principal Uses: Bursters, demolit | tion blocks |
| 3 inch HE, M42A1 Projectile, Lot K | C-5: | | |
| Density, gm/cc | 1.60 | | |
| Charge Wt, Ib | 0.842 | | |
| Total No. of Fragments: | | Method of Loading: | Cast |
| For TN T | 514 | include of Louding. | Cast |
| For Subject HE | 58 5 | Loading Density: gm/cc | 1.60 |
| Fragment Velocity: ft/sec | | | |
| At 9 ft At 25½ ft | | Storage: | |
| Density, gm/cc | | Method | Dry |
| | | _ | - |
| Blast (Relative to TNT): | | Hazard Class (Quantity-Distance) | Class 9 |
| Air: | | Compatibility Group | Group I |
| Peak Pressure | | | - (- ⁰ ~ |
| Impulse | | Exudation Exud | les at 65° C |
| Energy | | | |
| Air, Confined: Impulse | | | |
| Under Water : Peak Pressure | | | |
| Impulse | | | |
| Energy | | | |
| Underground: Peak Pressure | | | |
| Impulse | | | |
| Energy | | | |
| | | | |
| | | | |
| | | | |
| | | | |

<u>Tetrytol</u>, 65/35

| Composition: | | Molecular Weight: | 264 |
|---|----------------|--|------------|
| % Tetryl | 65 | Oxygen Balance: CO ₂ % CO % | -56 -14 |
| TNT | 35 | Density: gm/cc | 1.60 |
| | | Melting Point: °C | 68 |
| C/H Ratio | | Freezing Point: °C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | 28 | Boiling Point: °C | |
| Sample Wt 20 mg | 11 | Refractive Index, $\mathbf{n}_{z_0}^{D}$ | |
| Picatinny Arsenal Āpporotus, in. Sample Wt, mg | 17 | n ₂₅ | |
| Campie Wi, mg | -1 | n ^D ₃₀ | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| Steel Shoe | Cracks | cc/40 Hrs, at | |
| Fiber Shoe | Unaffected | 90°C | |
| | | 100°C | 2.8 |
| Rifle Bullet Impact Test: Trials | | 120°C | 11+ |
| Explosions 0 | | 135°C | |
| | | 150°C | |
| l'altiais | | 200 Gram Bomb Sand Test: | |
| Baillea | | Sand, gm | 52.6 |
| _ | | | |
| Explosion Temperature: °C | | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) | | Minimum Detonating Charge, gm Mercury Fulminate | 0.23* |
| 1 5 Ignites 325 | | Leod Azide | 0.23* |
| 5 ignites 5-0 | | | |
| 10 | | *Alternative initiating charges. | |
| 20 | | Ballistic Mortar, % TNT: | |
| 20 | | Trauzl Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | | Plate Dent Test: | |
| | | Method | |
| 100°C Heat Test: | | Condition | |
| % Loss, 1st 48 Hrs | | Confined | |
| % Loss, 2nd 48 Hrs | | Density, gm/cc | |
| Explosion in 100 Hrs | | Brisance, % TNT | |
| | | Detonation Rate: | |
| Flammability Index: Will not com | ntinue to burn | Confinement | None |
| | | Condition | Cast |
| Hygroscopicity: % | 0.02 | Charge Diameter, in. | 1.0 |
| | | — Density, gm/cc | 1.60 |
| Volatility: | | Rate, meters/second | 7310 |

| Fragmentation Test: | | Shaped Charge Effectiveness, TNT = 10 | 0: | | |
|---------------------------------------|-------|---------------------------------------|------------|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: | | (d) (e) Glass Cones Steel Cones | | | |
| Density, gm/cc | 1.61 | Hole Volume 133 126 | | | |
| Charge Wt, Ib | 2.010 | Hole Depth 120 119 | | | |
| Total No. of Fragments: | | | | | |
| For TNT | 703 | Color: Light yellow | to buff | | |
| For Subject HE | 856 | Principal lients D | | | |
| 3 inch HE, M42A1 Projectile, Lot KC-5 | : | Principal Uses: Bursters, demolitie | DI DIOCKS | | |
| Density, gm/cc | 1.60 | | | | |
| Charge Wt, Ib | 0.845 | | | | |
| Total No. of Fragments: | | | | | |
| For TNT | 514 | Method of Loading: | Cast | | |
| For Subject HE | 585 | | | | |
| Fragment Velocity: ft/sec | | Loading Density: gm/cc | 1.60 | | |
| At 9 ft | | | | | |
| At 25½ ft | | Storage: | | | |
| Density, gm/cc | | | _ | | |
| | | Method | Dry | | |
| Blast (Relative to TNT): | | Hazard Class (Quantity-Distance) | Class 9 | | |
| Air: | | Compatibility Group | Group I | | |
| Peak Pressure Impulse | | Fundation Funda | es at 65°C | | |
| Energy | | Exudation Exude | es at op c | | |
| Lincigy | | | | | |
| Air, Confined: Impulse | | | | | |
| mpulse | | | | | |
| Under Water: Peak Pressure | | | | | |
| Impulse | | | | | |
| Energy | | | | | |
| | | | | | |
| Underground: Peak Pressure | | | | | |
| Impulse | | | | | |
| Energy | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |

Compatibility with Metals:

<u>Dry:</u> Copper, brass, aluminum, magnesium, stainless steel, mild steel, mild steel conted with acid proof black paint and mild steel plated with copper, cadmium, zinc or nickel are unaffected. Magnesium-aluminum alloy is slightly affected.

Wet: Stainless steel and mild steel coated with acid-proof black paint are unaffected. Copper, brass, aluminum, magnesium, magnesium-aluminum alloy, mild steel and thild steel plated with cadmium, copper, zinc or nickel are slightly affected.

Preparation:

Tetrytols are manufactured by heating TNT in a melting kettle, equipped with a stirrer, until all the TNT is melted. The necessary amount of tetryl is added and heating snd stirring are continued. The temperature is allowed to drop from 100° C until the mixture is of maximum viscosity suitable for pouring. Part of the tetryl dissolves in TNT forming a eutectic mixture which contains 55 percent tetryl. This mixture freezes at 67.5°C.

Origin:

Tetrytols were developed during World War II. The 70/30 tetryl/INT castable mixture is the most important in military applications.

References: 74

(a) L. C. Smith and E. G. Eyster, Physical Testing of Explosives, Past III, Miscellaneous Sensitivity Tests, Performance Tests, OSRD Report No. 5746, 27 December 1945.

(b) D. P. MacDougall, <u>Methods of Physical Testing</u>, OSRD Report No. 803, 11 August 1942.

(c) L. C. Smith and S. R. Walton, A Consideration of RDX/Wax Mixtures as a Substitute for Tetryl in Boosters, NOL Mano 10,303, 15 June 1949.

(d) Eastern Laboratory, du Pont, Investigation of Cavity Effect, Sec III, Variation of Cavity Effect with Explosive Composition, NDRC Contract W672-ORD-5723.

(e) Eastern Laboratory, du Pont, Investigation of Cavity Effect, Final Report, Easter:? Lab, du Pont, 18 September 1943, NDRC Contract W-672-ORD-5723.

(f) Also see the following Picatinny Arsenal Technical Reports on Tetrytol:

| 0 | <u>1</u> | 2 | <u>3</u> | <u>5</u> | 6 | I | 8 | 2 |
|--------------------------------------|--------------------------------------|------|------------------------------|------------------------------|------------------------------|----------------------|----------------------|------|
| 1260 1360 1420 1500 1530 | 1291 1311 1451 1651 1951 | 1372 | 1193 1213 1363 1493 | 1285 1325 1885 2125 | 1376 1436 1466 1506 | 1477 1737 1797 | 1158 1388 1838 | 1379 |

TNT (Trinitrotoluene)

| Composition: % | | Molecular Weight: (C ₇ H ₅ N | 3 ⁰ 6) | 227 |
|--|--------------------------|---|-------------------|---------------------------|
| | ^H 3 | Oxygen Balance: CO, % CO % | | -74 -25 |
| 0 ₂ N- | NO ₂ | | | |
| N 18.5 | | Density: gm/cc Crys | tal | 1.65 |
| 0 42.3 | | Melting Point: "C | | 81 |
| C/H Ratio 0.549 | ° ₂ | Freezing Point: "C | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | 95- 100+ | Boiling Point: °C | | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 14-15 17 | Refractive Index, n_{20}^{D} | α β Τ | 1.5430 1.6742 1.717 |
| Friction Pendulum Test: | | | | |
| Steel Shoe | Unaffected Unaffected | Vacuum Stability Test: cc/40 Hrs, at 90°C | | |
| Rifle Bullet Impact Test: Trials | | 100°C | | 0.10 |
| % | | 120°C | | 0.23 |
| Explosions 4 | | 135°C | | 0.44 |
| Partials 0 | | 150°C | | 0.65 |
| Burned 0 | | 200 Gram Bomb Sand lest; | | |
| Unaffected 6 | | Sand, gm | | 48.0 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 570 | | Sensitivity to Initiation: Minimum Detonating Char | ge, gm | |
| 1 520 | | Mercury Fulminate | | 0.24* |
| 5 kcomposes 475 | | Lead Azide | | 0.27* |
| 10 465 15 | | Tetryl *Alternative initiating | charges. | |
| 20 | | Ballistic Mortar, % TNT: | | d=100 |
| | | Trauzl Test, % TNT: | st | d=100 |
| 75°C International Heat Test: % Loss in 48 Hrs | 0.04 | Plate Dent Test: Method A | (a) A | В |
| 1002011 | | Condition Cas | | D |
| 100°C Heat Test: | | Confined Yes | Yes | No |
| % Loss, 1st 48 Hrs | 0.2 | Density, gm/cc 1.61 | | 1.61 |
| % Loss, 2nd 48 Hrs Explosion in 100 Hrs | 0.2 None | Brisance, % TNT 100 | 100 | 100 |
| | None | | | |
| Flammability Index: (b) | 100 | Detonation Rate: Confinement U | Inconfined | Unconfined |
| | | | ressed | Cast |
| Hygroscopicity: % 30 ⁰ C, 90% RH | 0.03 | | .0 | 1.0 |
| | | • | .56 | 1.56 |
| Volatility: 30 ⁰ ℃ | Ni 1 | | 825 | 6640 |

| Beester Considuity Test | | | | 4. 1 | 1.5 |
|---|---|---|---|---|--|
| Booster Sensitivity Test: Condition | (c) Pressed | Cast | Decomposition Equation: Oxygen, atoms/sec | (h) 10 ^{11.4} | (i) 10 ^{12.2} |
| Tetryl, gm | 100 | 100 | (Z/sec) | | |
| Wax, in. for 50% Detor | | 0.82 | Heat, kilocolorie/mole | 34.4 | 43.4 |
| | | 0102 | (AH, kcɑl/mol) Temperature Range, ℃ | 275-310 | 238-277 |
| Wax, gm Density, gm∕cc | 1.55 | 1.60 | | | |
| Density, gin/cc | | 1.00 | Phase | Liquid | Liquid |
| Heat of: | (d) | | Armor Plate Impact Test: | | |
| Combustion, cal/gm | | 3620 | Annor Plate impact rest. | | |
| Explosion, cal/gm | | 1080 | 60 mm Mortar Projectile: | | (j) |
| Gas Volume, cc/gm | | 730 | 50% Inert, Velocity, ft/ | 'sec | >1100 |
| Formation, col/gm | | 78.5 | Aluminum Fineness | | |
| Fusion, cal/gm | | 22.34 | | | |
| Temperature, °C | | 79 | 500-1b General Purpose Bo | mbs; | (j) |
| Specific Heat: col/gm/°C | | | | | d - |
| | | 0.309 | Plate Thickness, inches | Trials | % Inert |
| 20 | | 0.328 | 1 | 0 | |
| 50 | | 0.353 | | 0 0 | |
| 80 | | 0.374 | 11/4 | | 100 |
| | | | 11/2 | 4 | 100 |
| | | | 13/4 | 4 | 50 |
| Burning Rate: cm/sec | | | | | |
| | | | Bomb Drop Test: | | |
| Thermal Conductivity: | | | | | |
| cal/sec/cm/°C | See next p | age. | T7, 2000-1b Semi-Armor-F | Piercing Bomb | vs Concrete: |
| | | | Max Safe Drop, ft | 500 | 00-6000 |
| Coefficient of Expansion: | (b) | | Wax Sale Diop, It | 200 | 00-0000 |
| Linear, $\%/^{\circ}C - 40^{\circ}$ to | о 60°C 5.4 х о 60°C 6.7 х | 10^{-5} (b) | 500-Ib General Purpose B | | ~ . |
| Volume, %/°C 27 ⁰ t d | | na - 5 | | <u>No Seal</u> | Seal |
| volume, $\%$ / C 27 to 16° to | o 70 ⁰ C 26.3 : | $x 10^{-5}$ (b) (n) | Height, ft | 4,000 | 4-5,000 |
| | | <u>(n)</u> | | | |
| hardnoce Maha' Coole: | (a) | 11 | Trials | 26 | 20 |
| hardness, Mohs' Scale: | (e) | 1.4 | Trials Unaffected | 26 24 | 20 20 |
| | | 1.4 | | | |
| Young's Modulus: | (b) | 10 | Unaffected | 24 | 20 |
| Young's Modulus: E', dynes/cm ² | (b) | 5.45 x 10 ¹⁰ | Unaffected Low Order | 24 2 | 20 0 |
| Young's Modulus: E', dynes/cm ² E, lb/inch ² | (b) | 5.45 x 10 ¹⁰ 0.79 x 10 ⁶ | Unaffected Low Order | 24 2 0 Somb vs Concre | 20 0 0 |
| Young's Modulus: E', dynes/cm ² | (b) | 5.45 x 10 ¹⁰ | Unaffected Low Order High Order 1000-Ib General Purpose E | 24 2 0 Bomb vs Concre <u>No Seal</u> | 20 0 0 ete: <u>Sca 1</u> |
| Young's Modulus: E', dynes/cm ² E, lb/inch ² Density, gm/cc | (b) | 5.45 x 10 ¹⁰ 0.79 x 10 ⁶ 161 | Unaffected Low Order High Order 1000-Ib General Purpose E Height, ft | 24 2 0 30mb vs Concre <u>No Seal</u> 5,000 | 20 0 ote: <u>Sea 1</u> 5,000 |
| Young's Modulus: E', dynes/cm ² E, lb/inch ² Density, gm/cc Compressive Strength: lb/in | (b) | 5.45 x 10 ¹⁰ 0.79 x 10 ⁶ 161 | Unaffected Low Order High Order 1000-Ib General Purpose E Height, ft Trials | 24 2 0 30mb vs Concre <u>No Seal</u> 5,000 2 1 | 20 0 0 ete: <u>Sca 1</u> 5,000 26 |
| Young's Modulus: E', dynes/cm ² E, lb/inch ² Density, gm/cc Compressive Strength: lb/in Density, gm/cc | (b) | 5.45 x 10 ¹⁰ 0.79 x 10 ⁶ 161 | Unaffected Low Order High Order 1000-Ib General Purpose E Height, ft Trials Unaffected | 24 2 0 Romb vs Concrete No Seal 5,000 21 18 | 20 0 0 ete: 5,000 26 22 |
| Young's Modulus: E', dynes/cm ² E, lb/inch ² Density, gm/cc Compressive Strength: lb/in Density, gm/cc Vapor Pressure: | (b) (nch ² 13800 | 5.45 x 10 ¹⁰ 0.79 x 10 ⁶ 161 | Unaffected Low Order High Order 1000-Ib General Purpose E Height, ft Trials Unaffected Low Order | 24 2 0 Somb vs Concre $\frac{No Seal}{5,000}$ 21 18 0 | 20 0 0 ete: <u>Sea 1</u> 5,000 26 22 0 |
| Young's Modulus: E', dynes/cm ² E, lb/inch ² Density, gm/cc Compressive Strength: lb/in Density, gm/cc Vapor Pressure: "C mm | (b) (c) nch ² 13800 Mercury | 5.45 x 10 ¹⁰ 0.79 x 10 ⁶ 161 0-14000 1.62 | Unaffected Low Order High Order 1000-Ib General Purpose E Height, ft Trials Unaffected | 24 2 0 Romb vs Concrete No Seal 5,000 21 18 | 20 0 0 ete: 5,000 26 22 |
| Young's Modulus: E', dynes/cm ² E, lb/inch ² Density, gm/cc Compressive Strength: lb/in Density, gm/cc Vapor Pressure: "C mm 80 | (b) (c) nch ² 13800 Mercury 0.042 | 5.45 x 10 ¹⁰ 0.79 x 10 ⁶ 161 0-14000 1.62 | Unaffected Low Order High Order 1000-Ib General Purpose E Height, ft Trials Unaffected Low Order | 24 2 0 Somb vs Concre $\frac{No Seal}{5,000}$ 21 18 0 | 20 0 0 ete: <u>Sea 1</u> 5,000 26 22 0 |
| Young's Modulus: E', dynes/cm ² E, lb/inch ² Density, gm/cc Compressive Strength: lb/in Density, gm/cc Vapor Pressure: "C mm | (b) (c) nch ² 13800 Mercury | 5.45 x 10 ¹⁰ 0.79 x 10 ⁶ 161 0-14000 1.62 | Unaffected Low Order High Order 1000-Ib General Purpose E Height, ft Trials Unaffected Low Order | 24 2 0 Somb vs Concre $\frac{No Seal}{5,000}$ 21 18 0 | 20 0 0 ete: <u>Sea 1</u> 5,000 26 22 0 |
| Young's Modulus: E', dynes/cm ² E, lb/inch ² Density, gm/cc Compressive Strength: lb/in Density, gm/cc Vapor Pressure: "C mm 80 85 90 95 | (b) (c) nch ² 13800 Mercury 0.042 0.053 0.067 0.085 | 5.45 x 10 ¹⁰ 0.79 x 10 ⁶ 161 0-14000 1.62 | Unaffected Low Order High Order 1000-Ib General Purpose E Height, ft Trials Unaffected Low Order | 24 2 0 Somb vs Concre $\frac{No Seal}{5,000}$ 21 18 0 | 20 0 0 ete: <u>Sea 1</u> 5,000 26 22 0 |
| Young's Modulus: E', dynes/cm ² E, lb/inch ² Density, gm/cc Compressive Strength: lb/in Density, gm/cc Vapor Pressure: "C mm 80 85 90 | (b) (c) nch ² 13800 Mercury 0.042 0.053 0.067 | 5.45 x 10 ¹⁰ 0.79 x 10 ⁶ 161 0-14000 1.62 | Unaffected Low Order High Order 1000-Ib General Purpose E Height, ft Trials Unaffected Low Order | 24 2 0 Somb vs Concre $\frac{No Seal}{5,000}$ 21 18 0 | 20 0 0 ete: <u>Sea 1</u> 5,000 26 22 0 |

INT (Trinitrotoluene)

| Fragmentation Test: | | Shaped Charge Effectiveness, TNT = | 100: |
|---|------------|---|--------------------------|
| 90 mm HE, M71 Projectile, Lot WC-91: | | Glass Cones Steel | l Cones |
| Density, gm/cc | 1.60 | Hole Volume 100 1 | 00 |
| Charge Wt, ib | 2.104 | Hole Depth 100 1 | 00 |
| Total No. of Fragments: | | | |
| ForTNT | 703 | Color: Light, | yellow |
| For Subject HE | 703 | | |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | | Principal Uses: GP bombs, HE pa demolition charges, dep grecades, propellant co | pth charges, |
| Densitv, gm/cc | 1.60 | ground, propertant of | |
| Charge Wt, Ib | 0.848 | | |
| Total No. of Fragments: | | Method of Loading: 1. Cast | |
| For TNT | 514 | Method of Loading: 1. Cast 2. Pressed | |
| For Subject HE | 514 | | |
| | | Loading Density: gm/cc | See below |
| ra gment Velocity: ft/sec At 9 ft | (k) | | |
| At 9 If At 251/2 ft | 260 236 | Storage: | |
| Density, gm/cc | 1.5 | Method | Dry |
| lost (Relative to | | Hazard Class (Quantity-Distance) | Class 9 |
| Air: | | Compatib i⊪ty Group | Group I |
| Peak Pressu | 100 | | |
| Impulse | 100 | Exudation No | one at 65 ⁰ 0 |
| - | 100 | | |
| Air, Confined: | | Loading Density: gm/cc | |
| Impulre | 100 | 1. Cast 1.58-1.59 2. Press | ed psi x 10 ³ |
| Under Water: | | 3 5 10 15 2 | - 20 30 50 |
| Peak Pressur | 100 | | 55 1.59 1. |
| impulse | 100 | Thermal Conductivity: | |
| France | 100 | cal/sec/cm/°C | |
| Underground: | | Density 1.19 gm/cc (g) 5.28 | x 10-4 |
| Peak Pressure | 100 | 1.51 gm/cc (g) 7.12 1.54 gm/cc (b) 5.6 | $x 10^{-4}$ x 10^{-4} |
| Impulse | 100 | 1.54 gm/ec (b) $5.61.67 gm/ec$ (q) 12.21 | x 10-4 |
| Energy | 100 | 'iscosity, poi.ses: | |
| | | Temp, 85°C 100°C | 0.139 |
| | | ulk Modulus at Room | 0.095 |
| | | | (m) |
| | | Dynes/cm ² x 10 ⁻¹⁰ | 2.92 |

| Effect of Temperature on Rat | te of Detona | tion: (1 |) | | |
|---|----------------|------------|-----------------|----------|--|
| Temperature of Charge, ^o C | - 54 | 21 | 60 | 60 | |
| Hours at Temperature | 16 | 16 | 24 | 72 | |
| Density, gm/cc | 1.63 | 1.62 | 1.64 | 1.64 | |
| Rate, meters/second | 6700 | 6820 | 6770 | 6510 | |
| Sensitivity to Electrostatic | Discharge, | Joules; ' | Through 10 | 0 Mesh: | |
| Unconfined Confined | 0.06 4.4 | | | | |
| Impact Sensitivity versus Te | emperature: | | | | |
| Picatinny Arsenal Apparat | us, 2 kg wt, | inches: | | | |
| ° <u>C</u> | inches | | | | |
| -40 Room | 17 14 | | | | |
| 80 90 | 7 | | | | |
| 105-110 | 3 2 (5 exp) | L in 20 ti | rials) | | |
| Impact Sensitivity versus Lo | ading Metho | d, Large I | Impact Ap | paratus, | Inches: |
| Pressed at 1.60 gm/cc Cast at 1.60 gm/cc | 70 26 | | | | |
| Rifle Bullet Impact Sensitiv | ity versus ' | Femperatu | re, Confin | ement: | |
| Standard Iron Bomb | | Ten | xm iperature | | <u>105⁰ to 110⁰C</u> |
| No Air Space Trials | | | 10 | | 10 |
| Explosions | | 1 very | low order | | 7 |
| Air Space Trials Explosions | | | 10 0 | | 10 0 |

Tin or Cardboard Bombs:

| With or Without Air Space | | |
|---------------------------|----|----|
| Trials | 10 | 10 |
| Explosions | 0 | 0 |

Explosion Temperature versus TNT Initial Temperature:

| Explosio | n lemperature | e versus . | INI INITIAL | Temper | ature: | | |
|-----------------------------------|--|---------------------|--|---------------------------|--------------------------------------|---------------------------|------------------|
| TNT Te | mperature, In | niti al | | Ex | plosion Tempera | ture, ^o (| 2 |
| R | 000 05 ⁰ -100 ⁰ C | | | | 470 (Decompose 480 (Decompose | | |
| Explosion | n Temperature | e versus (| Confinement | •C: | | | |
| | nfined d in glass ca y at 80.5 ⁰ C: | apillary | Decompos Explodes | es | 470 320-335 | | |
| S = % | sity, X, cp I solid in slu cle size effe | irry | | 26 | | | |
| Density, | gm/cc: | | | | | | |
| <u>°c</u> | | | State | | gm/cc | | |
| 27 80 82 87 95 | | | Flaked Flaked Liquid Liquid Liquid | | 1.65 1.64 1.48 1.48 1.48 | | |
| Solubili | ty of TNT, gm | n/100 gm (| %), in: (f) |) | | | |
| Wa | ater | Acet | one | B | enzene | T | oluene |
| °c | <u>%</u> | <u>°c</u> | ₽/2 | <u>°c</u> | <u>%</u> | <u>°c</u> | |
| 0 20 40 60 | 0.0100 0.0130 0.0285 0.0675 | 0 20 40 60 | 57 109 228 600 | 0 20 40 60 80 | 13 67 180 478 ? 2000 | 0 20 40 60 80 | 19 30 >170 |
| <u>C</u> | Carbon | | | | | Tri | chloro |

| 60 | 0.0675 | 60 | 600 | 60 80 | 478 ? 2000 | 60 80 | 367 >1700 |
|--------------------|------------------------------|-----------|--------------|---------------------|----------------------|-------------------------------|--------------|
| | <u>arbon</u> chloride | Etl | her | Chlore | oform | <u>Trichl</u> <u>ethyl</u> | |
| °C | % | <u>°c</u> | <u>%</u> | °c | <u>%</u> | °C | <u>%</u> |
| 0 0 40 60 | 0.20 0.65 1.75 6.90 | 0 20 | 1.73 3.29 | 0 20 40 60 | 6 19 66 302 | 25 55 | 3.5 60 |

Z

28 1393

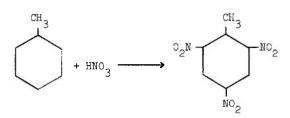
70 75 17.34 24.35

| | | | | | otoruene) | | |
|------------------------------------|---------------------------|------------------------------|--------------------------------|-----------------------|------------------------|---------------------------|--|
| <u>Pyri</u> | dine | Methy | l acetate | <u>Eth</u> dich | <u>ylene</u> loride | A-Ethernet | noxy- a cet at e |
| °c | 1/2 | <u>°c</u> | K | <u>°c</u> | <u>%</u> | <u>°c</u> | % |
| 20 40 60 70 | 140 250 640 1250 | 20 40 50 | 73 135 280 | 20 40 60 | 34 123 460 | 20 40 50 | 29. 5 49 96 |
| | <u>hloro-</u> ane | A | niline | | <u>ropyl</u> ohol | Etha | <u>nol</u> |
| ° _C | % | °c | <u>%</u> | <u>°c</u> | <u>%</u> | °C | Ź |
| 20 40 50 | 18 50 100 | 10 30 50 70 80 | 6.1 11.5 29 74 130 | 20 40 50 | 0.76 1.96 2.95 | 0 20 40 60 70 | 0.62 <i>1.25</i> 2.85 8.4 15 |
| Isobı | ıtyl alcoh | 01 | | Carbon disu | lfide | Chlorobe | enzene |
| <u>°</u> с | | <u>%</u> | | o _C | <u>%</u> | <mark>о</mark> с | <u>%</u> |
| 0 20 40 50 | | 0.20 0.61 1.41 2.35 | | 0 20 40 | 0.14 0.44 1.4 | 20 30 40 50 | 85 51 79 116 |

TNT (Trinitrotoluene)

Preparation:

(AC 7258, 7259, 7260 - Nitration Kinetics) (Chemistry of Powder and Explosives, Davis)



In older processes trinitrotoluene (TNT) was slowly and laboriously nitrated in three stages using successively stronger acids. Today, however, a single stage nitration is possible, in a short time (less than one hour) producing TNT at a cost of a little less than $6\phi/lb$. In England, a two stage continuous process was developed during World War 11; in the first counter current stage, toluene was nitrated to the mono stage mononitrotoluene (MNT); in the second stage, also counter current, MNE was nitrated to TNT.

TNT (Trinitrotoluene)

It was the British work, on the kinetics of nitration of toluene to TNT, that first pointed out the basic importance to nitration processes of the nitroxyl ion (NO_2^+) , on the one hand, and the role of the bisulfate ion (HSO_4^-) and unionized sulfuric acid on the other. These concepts were successful in explaining the maximum in nitration rate occurring at a sulfuric acid content of 92%. This work, for instance, leads to the following equation for the rate of formation of TNT from DNE

$\frac{d (\text{INT})}{dt} = K (\text{NO}_2^+) [K' (\text{HSO}_4^-) + K'' (\text{H}_2\text{SO}_4)] (\text{DNT})$

<u>Three Stage Process</u>: Toluene (100 gm) is nitrated to the mono derivative by slowly adding a mixture of 294 gm sulf'uric acid (sp gr 1.84) and 147 gm nitric acid (sp gr 1.42) to it at $30^{\circ}-40^{\circ}$ C, with good agitation. Acid addition requires 1-1.5 hour, and stirring at $30^{\circ}-40^{\circ}$ C is continued 30 minutes longer. The mixture is cooled and the lower layer of spent acid drawn off.

Half the crude mono is dissolved in 109 gm sulfuric acid (sp gr 1.84) with cooling, the solution heated to 50° C and a mixture of 54.5 gm nitric acid (sp gr 1.50) and 54.5 gm sulfuric acid (sp gr 1.84) added, under agitation, at such a rate that the temperature is maintained between 90° and 100° C. Acid addition requires 1 hour, and stirring at 90° - 100° C is continued 2 more hours.

While the dinitration mixture is still at 90° C, 145 gm fuming sulfuric acid (oleum containing 15% free $$0_3$) is added slowly. A mixed acid of 92.5 gm each nitric acid (sp gr 1.50) and 15% oleum is slowl added, under good agitation at 100° -115°C over 1½-2 hours. The mixture is stirred at 100 -115°C for 2 more hours, cooled, filtered, and the TNT cake broken up and washed with water. The TNT is washed 3-4 times with hot water (85° -95°C) with good agitation. The product can be purified either by recrystallization from alcohol or by washing it with 5 times its weight of 5% sodium bisulfite solution at 90°C for ½ hour with vigorous stirring, washing with hot water until the washings are colorless, and cooling slowly with stirring to granulate the product.

Origin:

TNT was first prepared in 1863 by Wilbrand (Ann 128, 178), later by Beilstein and Kuhlberg (Ber 3, 202 (1870) and also Tiemann (Ber 3, 217 (1870), each using different methods of starting materials. It was nearly 30 years later when Hausermann undertook its manufacture on an industrial scale (Z angew Chem, 1891, p. 508; J Chem Ind, 1891, p. 1028). After 1901 TNT began to be used extensively as a military explosive and Germany became the first nation to adopt it as a standard shell filler (1902-1904). During World War I all the major powers of the world were using TNT, with the quantity used limited only by the available supply of toluene. Prior to World War II the development of synthetic toluene from petroleum made available in the United States, an almost unlimited supply of this raw material. Because of the general suitability of TNT for melt-loading and its extensive use in binary and ternary explosive mixtures, TNT is considered the most important military explosive known today.

Destruction by Chemical Decomposition:

TNT is decomposed by adding it slowly, while stirring, to 30 times its weight of a solution prepared by dissolving 1 part of sodium sulfide ($Na_2S \cdot 9H_2O$) in 6 parts of water.

References:75

(a) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

⁷⁵See footnote 1, page 10.

(b) Philip C. Keenan and Dorothy Pipes, <u>Table of Military High Explosives</u>, Second Revision, NAVORD Report No. 87-46, 26 July 1946.

(c) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute for</u> <u>Tetryl in Boosters</u>, NOL Mano 10, 303, 15 June 1949.

(d) L. C. Smith and E. H. Eyster, <u>Physical Testing of Explosives</u>, <u>Part III</u>, <u>Miscellaneous</u> <u>Sensitivity Tests</u>, <u>Performance Tests</u>, <u>OSRD Report No. 5746</u>, 27 December 1945.

(e) Report AC-2587.

(f) International Critical Tables and various other sources in the open literature.

(g) E. Hutchinson, The Thermal Sensitiveness of Explosives. The Thermal Conductivity of Explosive Materials, AC-2861, First Report, August 1942.

(h) A. J. B. Robertson, Trans Farad Society, <u>44</u>, 977 (1948).

(i) M. A. Cook and M. T. Abegg, "Isothermal Decomposition of Explosives," University of Utah, <u>Ind Eng Chem</u> (June 1956), pp. 1090-1095.

(j) Committee of Div 2 and 8, NDRC, <u>Report on HBX and Tritonal</u>, OSRD No. 5406, 31 July 1945.

(k) R. W. Drake, <u>Fragment Velocity and Panel Penetration of Several Explosives in Simulated Shells</u>, OSRD Report No. 5622, 2 January 1946.

(1) W. F. McGarry and T. W. Stevens, Detonation Rates of the More Important Military Explosives at Several Different Temperatures, PAIR No. 2383, November 1956.

(m) W. S. Cramer, Bulk Compressibility Data on Several High Explosives, NAVORD Report No. 4380, 15 September 1956.

(n) Mantrov, Journal of Chemical Industry (Russia) 6, 1929, pp. 1686-1688.

(o) Also see the following Picatinny Arsenal Technical Reports on TNT:

| <u>0</u> | <u>1</u> | 2 | 3 | 4 | <u>5</u> | 6 | 7 | ھ | ٩ |
|---|--|---|--|---|---|---|--|--|--|
| $\begin{array}{c} 10\\ 30\\ 240\\ 350\\ 630\\ 760\\ 810\\ 1120\\ 1140\\ 1170\\ 1260\\ 1270\\ 1360\\ 1400\\ 1400\\ 1400\\ 1500\end{array}$ | 291 551 731 861 901 971 1041 1121 1391 1431 1431 1451 1491 1651 1821 | 132 582 782 892 972 1072 1182 1272 1272 1272 1342 1352 1352 1352 1352 1402 1452 1472 | 43 83 133 273 513 643 673 743 853 863 1063 1123 1123 1193 1243 1323 | 364 694 904 1094 1124 1224 1284 1294 1304 1314 1344 1444 1454 | 65 195 425 555 695 735 805 975 1145 1285 1305 1315 1395 1425 | 86 266 556 986 1046 1276 1446 1446 1446 1466 1456 1556 1636 1756 | 47 87 507 597 707 807 817 837 1107 1147 1217 1247 1307 1417 1427 | 118 288 638 738 768 838 1088 1098 1128 1148 1158 1158 1158 1198 1228 1258 1308 | 99 249 269 319 389 499 709 739 779 799 889 929 939 1099 1109 1129 |

TNT (Trinitrotoluene)

| <u>o</u> | 2 | 3 | 4 | <u>5</u> | 6 | Z | 8 | <u>9</u> |
|--|--------------------------------------|--|--|---|--------------|--|--|--|
| 1530 1540 1550 1730 2010 2100 2160 | 1492 1562 1582 1712 1862 | 1373 1493 1553 1633 1693 1823 2063 2163 | 1524 1544 1564 1604 1674 1754 1924 2064 2214 | $1435 \\ 1445 \\ 1495 \\ 1515 \\ 1535 \\ 1605 \\ 1605 \\ 1665 \\ 1865 \\ 1965 \\ 1715 \\ 1885 \\ 2125 \\ 2175 \\$ | 1956 2216 | $1437 \\ 1457 \\ 1497 \\ 1537 \\ 1547 \\ 1557 \\ 1577 \\ 1597 \\ 1677 \\ 1737 \\ 1797 \\ 1827 \\ 1847 \\ 2007 \\ 2147 \\ 2167 \\ $ | 1318 1338 1418 1428 1578 1618 1688 1728 1828 1828 1838 1858 2008 2138 2168 | $\begin{array}{c} 11 39 \\ 1179 \\ 1259 \\ 1289 \\ 1339 \\ 1369 \\ 1379 \\ 1419 \\ 1429 \\ 1429 \\ 1489 \\ 1529 \\ 1549 \\ 1529 \\ 1689 \\ 1529 \\ 1689 \\ 1709 \\ 1729 \\ 1749 \\ 1809 \end{array}$ |

| Composition: % | | Molecular Weight: | 97 |
|--|-----------------------------|---|----------------------------|
| RDX | 42 | Oxygen Balance: CO, % CO % | - 55 - 26 |
| INT | 40 | Density: gm/cc Cast | 1.76-1.81 |
| Aluminum | 18 | Melting Point: "C | 1.10-1.01 |
| C/H Ratio | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | 42 9 15 | Boiling Point: °C Refractive Index, n ^o ₂₀ n ^b ₂₅ n ^b ₃₀ | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | | Vacuum Stability Test: cc/40 Hrs, at 90°C | |
| Rifle Bullet Impact Test:Trials%20Partials80 | | 100°C 120°C 135°C 150°C | 1.0 |
| Burned 0 Unaffected 0 | | 200 Gram Bomb Sand Test: Sand, gm | 59•5 |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) 1 5 Decomposes 260 10 | | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl | 0.18 |
| 15 20 | | Ballistic Mortar, % TNT: (a) | 138 |
| | | Trauzl Test, % TNT : (b) | 164 |
| 75°C International Heat Test:% Loss in 48 Hrs | | Plate Dent Test: (c) Method | В |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | 0.00 0.10 None | Condition Confined Density, gm/cc Brisance, % TNT | Cast No 1.83 120 |
| Flammability Index: | 196 | Detonation Rate: (d) Confinement | None |
| Hygroscopicity: % 30 [°] C, 90% RH | 0.00 | Condition Charge Diameter, in. | Cast 1.0 |
| Volatility: | | Density, gm/cc Rate, meters/second | 1.81 7495 |

| Booster Sensitivity Test: Condition Tetryl, gm Wax, in. for 50% Detona Wax, gm Density, gm/cc Heat of: Combustion, cal/gm Explasion, cal/gm Formation, cal/gm Fusion, cal/gm | (c) Pressed 10 ation 2 1.64 (a) | Cast 5 0 1.81 3740 1800 | Decomposition Equation: Oxygen, otoms/sec (Z/sec) Heat, kilocalorie/mole (AH, kcal/mol) Temperature Range, °C Phase Armor Plate Impact Test: 60 mm Mortar Projectile: 50% Inert, Velocity, ft/sec Aluminum Fineness 500-ib General Purpose Bombs: |
|--|---|--|---|
| Specific Heat: col/gm/°C | (b) | | |
| A t -5° C | | 0.22 | Plate Thickness, inches |
| Density, gm/cc | | 1.82 | 1 |
| At 15°C | | 0.24 | 11/4 |
| AT LY U | | 0.24 | 11/2 |
| | | | 13⁄4 |
| Burning Rate: cm/sec Thermal Conductivity: cal/sec/cm/"C Density, gm/cc Coefficient of Expansion: Linear, %/°C -73 to Volume, %/°C Hardness, Mohs' Scale: Young's Modulus: E, dynes/cm ² E, lb/inch ² Density, gm/cc Compressive Strength: lb/inc Density, gm/cc Vapor Pressure: °C mm M | (b) 9.53 1.38 | 7×10^{-4} 1.82 0^{-5} (b) 1.77 1.77 1.77 1.77 1.77 | Bomb Drop Test: 17, 2000-Ib Semi-Armor-Piercing Bomb vs Concrete: Max Safe Drop, ft 500-Ib General Purpose Bomb vs Concrete: Height, ft Trials Unaffected Low Order High Order 1000-Ib General Purpose Bomb vs Concrete: Height, ft Trials Unaffected Low Order High Order High Order |
| | | | |

| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/ccGlass ConesSteel ConesDensity, gm/cc1.75Hole Volume150145Charge Wt, Ib2.316Hole Depth127131Total No. of Fragmentt: For TNT703Color:GrayFor Subject HE891Principal Uses:Depthcharges, bombs3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc1.79Principal Uses:Depthcharges, bombsTotal No. of Fragments: For TNT514Method of Loading:CastFor Subject HE647Loading Density: gm/cc1.76-1.8Fragment Velocity:ft/sec At 9 ft At 25½ ft2960 2800Storage: MethodDryBlast (Relative to TNT):(e)Hazard Class (Quantity-Distance)Class | Fragmentation Test: | | Shaped Charge Effectiveness, TNT = 100 50/36.5/13.5 |): |
|---|--------------------------------------|--------------|--|-----------|
| Density, gm/cc1.75Hole Volume150145Charge Wt, lb2.316Hole Volume150145Total No. of Fragmentt: For TNT703 For Subject HE891Color:Gray3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc1.79Depth charges, bombsPrincipal Uses:Depth charges, bombs7 total No. of Fragments: | 90 mm HE, M71 Projectile, Lot WC-9 | 1: | | nes |
| Charge Wt, Ib2.316Hole Depth127131Total No. of Fragmentt: For Subject HE691Color:Gray3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc1.79Principal Uses:Depth charges, bombs3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc1.79Principal Uses:Depth charges, bombsTotal No. of Fragments: For Subject HE647Method of Loading:CastFragment Velocity: ft/sec A125½ ft2960Loading Density: gm/cc1.76-1.8Fragment Velocity: ft/sec A125½ ft2960Storage:MethodDrzyBlast (Relative to TNT):(e)Hazard Class (Quantity-Distance)ClassAir: Peak Pressure126Effect of Temperature on Tempe SizeTompe C Sensitivity: TompTompe C Sensitivity: TompUnder Water: Peak Pressure116Tompe C Sensitivity: Size7 Total SizeYiscosity, poises: Temp, 83°C2.3Underground: peak Pressure127327 Total Size1.5 Size2.5 Tomp, 83°C4.5 Size | | | Hole Volume 150 145 | |
| For TNT 703 For Subject HE 891 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc 1.79 Charge Wt, Ib 0.940 Total No. of Fragments: For TNT 514 For Subject HE 647 Fragment Velocity: ff/sec At 25½ ft 2960 At 25½ ft 2800 Density, gm/cc Blast (Relative to TNT): (e) Air: Peak Pressure 122 Impulse 125 Energy 146 Air, Confined: Impulse 116 Under Water: Peak Pressure 116 Under Water: Peak Pressure 116 Under Water: Peak Pressure 116 Under ground: Peak Pressure 127 Impulse 127 Storage: Impulse 125 Innuise 127 Storage: Impulse 153 Underground: Peak Pressure 126 Underground: Impulse 127 Temp, 83 ³⁰ C 4.5 Stocast; Peak Pressure 153 Underground: Impulse 53 ³⁰ C Peak Pressure 126 Stocast; Peak Pressure 127 Temp, 83 ³⁰ C 4.5 | | 2.316 | Hole Depth 127 131 | |
| For TNT 703 For Subject HE 891 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Density, gm/cc 1.79 Charge Wt, Ib 0.940 Total No. of Fragments: For Subject HE For Subject HE 647 Fragment Velocity: ff/sec 2960 At 9 ft 2800 Density, gm/cc Method of Loading: Cast Loading Density: gm/cc 1.76-1.8 Fragment Velocity: ff/sec 2960 At 25½ ft 2800 Density, gm/cc Blast (Relative to TNT): (e) Air: Peak Pressure Impulse 125 Energy 146 Air, Confined: 116 Impulse 127 Peak Pressure 116 Undergound: 25 Peak Pressure 116 Undergound: 25 Undergound: 25 Peak Pressure 126 Impulse 127 32 7 104 8 Viscosity, poises: 1.5 Temp, 83 ⁰ C 4.5 | Total No. of Fragmentt: | | Color | Grav |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc 1.79 Density, gm/cc 1.79 Charge Wt, Ib 0.940 Total No. of Fragments: For TNT For Subject HE 647 Fragment Velocity: ft/sec 2960 At 9 ft 2800 Density, gm/cc Blast (Relative to TNT): (e) Air: Peak Pressure Impulse 125 Energy 146 Air, Confined: 116 Impulse 127 Peak Pressure 116 Under Water: Peak Pressure Peak Pressure 127 Energy 153 Underground: Peak Pressure Impulse 127 Sidout B 7 Job 8 Viscosity, poises: Temp, $\frac{83^0 \circ}{9 \circ \circ}$ Underground: Peak Pressure Impulse 153 | For TNT | 703 | | eruj |
| 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc 1.79 0.940 Total No. of Fragments: For TNT 514 For Subject HE Method of Loading: Cast For Subject HE 647 Loading Density: gm/cc 1.76-1.8 Fragment Velocity: ft/sec At 9ft At 25½ ft 2960 2800 Storage: Density: gm/cc 1.76-1.8 Blast (Relative to TNT): (e) Hazard Class (Quantity-Distance) Class Air: Peak Pressure 122 Impulse Compatibility Group Group Air, Confined: Impulse 116 Impact Sensitivity: Top Top Under Water: Peak Pressure 116 Impact Test 25 15 32 7 1.04 Undergound: Peak Pressure 127 25 15 32 7 1.04 8 Undergound: Peak Pressure 127 25 15 32 7 2.5 15 3 104 8 Undergound: Peak Pressure 153 104 8 Viscosity, poises: 7 2.3 | For Subject HE | 891 | Principal Uses: Depth charges, borr | bs |
| Charge Wi, Ib0.940Total No. of Fragments: For TNT514For Subject HE647Fragment Velocity: ff/sec At 9 ft At 25½ ft2960Density, gm/ccBlast (Relative to TNT):(e)Air: Peak Pressure122 ImpulseImpulse125 EnergyAir, Confined: Impulse116Under Water: Peak Pressure116Under ground: Peak Pressure127 153Underground: Peak Pressure153Underground: Peak Pressure153Under ground: Peak Pressure7 153Under Ground: Peak Pressure7 153Under Ground: Peak Pressure7 153Under Ground: Peak Pressure7 153Under Ground: Peak Pressure7 153Temp. 168 25 2 104Under Ground: Peak Pressure7 153Temp. 16830° 2 2 Under Ground: Peak Pressure7 | 3 inch HE, M42A1 Projectile, Lot KC- | 5: | | |
| Total No. of Fragments: For TNT 514 For Subject HE 647 Fragment Velocity: ft/sec At 9 ft At 25 ft 2960 2800 Density. gm/cc Blast (Relative to TNT): (e) Air: Peak Pressure 122 Impulse Energy 146 Air, Confined: Impulse 116 Under Water: Peak Pressure 116 Under Water: Peak Pressure 116 Under Water: Peak Pressure 116 Under Water: Peak Pressure 116 Under ground: Peak Pressure 127 Underground: Peak Pressure 127 Underground: Peak Pressure 127 Temp, 83°C 4.5 Underground: Peak Pressure 13 Underground: Peak Pressure 153 | Density, gm/cc | 1,79 | | |
| For TNT 514 For Subject HE 647 Fragment Velocity: ft/sec 2960 At 9 ft 2800 Density, gm/cc Blast (Relative to TNT): (e) Air: Peak Pressure Impulse 125 Energy 146 Air, Confined: 116 Impulse 127 Peak Pressure 116 Under Water: Peak Pressure Peak Pressure 116 Under Water: 116 Peak Pressure 116 Underground: 25 Peak Pressure 116 Impulse 127 32 7 104 8 Underground: Viscosity, poises: Peak Pressure 153 Impulse 25 104 8 | Charge Wt, Ib | 0.940 | | |
| For TNT 514 For Subject HE 647 Fragment Velocity: ft/sec 2960 At 9 ft 2800 Density. gm/cc Blast (Relative to TNT): (e) Air: Peak Pressure Peak Pressure 122 Impulse 125 Energy 146 Vinder Water: 116 Peak Pressure 116 Impulse 127 Peak Pressure 116 Under Water: 116 Peak Pressure 116 Underground: 127 Peak Pressure 116 Impulse 127 Size 7 104 8 Underground: Peak Pressure Impulse 127 Size 7 104 8 Viscosity, poises: 127 104 8 | Total No. of Fragments: | | Method of Loading: | Cast |
| Fragment Velocity: ft/sec 2960 At 9 ft 2800 Density, gm/cc Blast (Relative to TNT): (e) Air: Peak Pressure Impulse 125 Energy 146 Air, Confined: Impulse Impulse 116 Under Water: Peak Pressure Peak Pressure 116 Under Water: 116 Peak Pressure 116 Under Water: 127 Peak Pressure 116 Under Water: 127 Peak Pressure 116 Underground: 25 Peak Pressure 116 Impulse 127 32 7 104 8 Underground: Viscosity, poises: Peak Pressure 153 Impulse 27 32 7 104 8 Viscosity, poises: 7 Temp, 83% C 4.5 95% C 2.3 | For TNT | 514 | | |
| Fragment Velocity: ft/sec 2960 At 9 ft 2800 Density, gm/cc Blast (Relative to TNT): (e) Air: Peak Pressure Peak Pressure 122 Impulse 125 Energy 146 Air, Confined: Impulse Impulse 116 Under Water: Peak Pressure Peak Pressure 116 Under Water: 116 Peak Pressure 116 Under Water: 116 Peak Pressure 116 Under Water: 116 Peak Pressure 116 Underground: 25 Peak Pressure 127 Bigs 0 153 Underground: Viscosity, poises: Peak Pressure 16 Impulse 25 104 8 | For Subject HE | 647 | Loading Density: gm/cc | 1.76-1.81 |
| At 9 ft At 25½ ft 2960 2800 Density, gm/cc Blast (Relative to TNT): (e) Air: Peak Pressure 122 Impulse Impulse 125 Energy Air, Confined: Impulse 116 Under Water: Peak Pressure 116 Density, gm/cc Method Dry Hazard Class (Quantity-Distance) Class Compatibility Group Group Effect of Temperature on Impact Sensitivity: Impact Test OC 25 15 32 7 104 8 Underground: Peak Pressure 127 Peak Pressure 126 Impulse 127 Impulse 127 Temp, 83°C 4.5 Impulse Viscosity, poises: Temp, 83°C 4.5 Temp, 83°C 4.5 | Fragment Velocity: ft/sec | | | - , |
| MethodDryBlast (Relative to TNT):(e)Hazard Class (Quantity-Distance)ClassAir: Peak Pressure122Compatibility GroupGroupImpulse125ExudationEffect of Temperature on Impact Sensitivity:Feffect of Temperature on 2 Kg Wt, inchesImpact Test 2 Kg Wt, inchesUnder Water: Peak Pressure116Impact Test 2 Kg Wt, inchesTemp. 2 Kg Wt, inchesUnder Water: Peak Pressure116Z Kg Wt, inches 2 Kg Wt, inchesUnderground: Peak Pressure1272515 32Underground: Peak Pressure153Uiscosity, poises: 30°CViscosity, poises: 2 Kg %C | At 9 ft | 2960 2800 | Storage: | |
| Blast (Relative to TNT): (e) Air: Peak Pressure 122 Impulse 125 Exudation Energy 146 Effect of Temperature on Air, Confined: 116 Impact Sensitivity: Impulse 116 Impact Test Under Water: Peak Pressure 116 Peak Pressure 116 Impact Test Impulse 127 2 Kg Wt, inches Energy 153 104 Underground: Viscosity, poises: Peak Pressure Temp, 83°C Impulse 2,3 | Density, gm/cc | | Method | Dry |
| Peak Pressure 122 Impulse 125 Energy 146 Air, Confined: 116 Impulse 116 Under Water: Peak Pressure Peak Pressure 116 Impulse 127 Energy 153 Underground: 153 Underground: Viscosity, poises: Peak Pressure 153 Underground: Viscosity, poises: Temp, 83°c 4.5 95°c 2.3 | Blast (Relative to TNT): | (e) | Hazard Class (Quantity-Distance) | Class 9 |
| Impulse 125 Exudation Impulse 125 Exudation Air, Confined: 116 Impact Sensitivity: Impulse 116 Impact Test Under Water: OC 2 Kg Wt, inches Peak Pressure 116 25 Impulse 127 25 Impulse 127 32 Energy 153 32 Underground: Viscosity, poises: Peak Pressure Temp, 83°C Impulse Temp, 83°C | Air: | | Compatibility Group | Group I |
| Impulse149Energy146Air, Confined: Impulse116Impulse116Impact Sensitivity:Under Water: Peak PressurePA Impact Test 2 Kg Wt, inchesPeak Pressure116Impulse127Energy153Underground: Peak PressureViscosity, poises: 95°cPeak PressureTemp, 83°c 95°c | Peak Pressure | 122 | | |
| Air, Confined: ImpulseI16Effect of Temperature on Impact Sensitivity:Under Water: Peak Pressure116 $\overline{Temp.}$ $2 Kg Wt, inchesImpulse12725Energy15332104Underground:Peak PressureViscosity, poises:Peak PressureTemp. 83^{\circ}c95^{\circ}c4.52.3$ | Impulse | 125 | Exudation | |
| Air, Confined: ImpulseIIfImpact Sensitivity:Under Water: Peak Pressure116 $\overline{\frac{\text{Temp.}}{\text{OC}}}$ <u>PA Impact Test</u> Impulse1272515Signal153 32 7Underground: Peak PressureViscosity, poises:Viscosity, poises:Peak PressureImpulseTemp, 83° C4.595^{\circ}C2.31515 | Energy | 146 | | |
| Impulse116Impulse bension valueUnder Water: Peak Pressure116 $\frac{Temp.}{OC}$ PA Impact Test 2 Kg Wt, inchesImpulse1272515Energy1531048Underground: Peak Pressure ImpulseViscosity, poises: 95^{OC} 4.5 | Air. Confined: | | Effect of Temperature on | |
| Under Water: Peak Pressure116 $\overline{00}$ 2 Kg Wt, inchesImpulse1272515Energy153 $\overline{153}$ $\overline{32}$ 7Underground: Peak Pressure ImpulseViscosity, poises: $\overline{153}$ $\overline{104}$ Temp, 83^{0} C 4.5 95^{0}C2.3 | | 116 | THDACC BENELOTATON: | |
| Peak Pressure1162515Impulse127 25 15Energy153 104 8Underground:Viscosity, poises:Peak PressureTemp, 83° C 4.5 Impulse 25° C 2.3 | | | | |
| Impulse1272515Impulse127 32 7Energy153 104 8Underground:Viscosity, poises:Peak PressureTemp, 83° C 4.5 Impulse 95° C 2.3 | | 116 | 2 Kg Wt, inches | |
| Impulse121327Energy153327Underground:Viscosity, poises:Peak PressureTemp, 83°c4.5Impulse25°c2.3 | | | 25 15 | |
| Energy1031048Underground:Viscosity, poises:Peak PressureTemp, 83°CImpulse25°C2,3 | | • | 32 7 | |
| Peak Pressure Impulse Temp, 83°C 4.5 95°C 2.3 | Energy | 723 | 104 8 | |
| Impulse Temp, 83°C 4.5 Energy 95°C 2.3 | | | | |
| Energy 95 [×] C 2,3 | Impulse | | Temp, 83°C | 4.5 |
| | | | 95 [~] C | 2.3 |
| | | | | |
| | | | | |
| | | | | |

Preparation:

Torpex is manufactured by heating TNT to approximately 100°C in a steam-jacketed kettle equipped with a stirrer. Water wet RDX is added slowly to the molten TNT, while mixing and heating, until all the water is evaporated. Aluminum is added and the mixture is stirred until uniform. The mixture is cooled, with continued stirring, until it is suitable for pouring. Torpex can also be made by adding the calculated amount of TNT to Composition B to maintain the desired proportion of RDX/TNT, heating and stirring, and adding 18 percent of aluminum to complete the mixture.

Origin:

Torpex, a castable high explosive, was developed in England during World War II for use as a filler in warheads, mines and depth bombs. Several variations in the composition of torpex have been evaluated but the following are those used in service munitions:

| | <u>Torpex 2</u> <u>unwaxed</u> | Torpex 2 waxed | Torpex 3 |
|--|-----------------------------------|-----------------------------|------------------------------------|
| | (a) | (b) | (c) |
| RDX, % TNT, % Aluminum, % Wax, % Calcium chloride, % | 42 40 18 | 41.6 39•7 18.0 0•7 | 41.4 39.5 17.9 0.7 0.5 |

(a) Made from Composition B-2 or 60/40 Cyclotol.

(b) Made by the addition of aluminum to Composition B.

(c) Made by the addition of calcium chloride to Torpex 2.

Wax has the undesirable effect of (1)tending to coagulate the aluminum, thus giving a less homogeneous and more viscous product, (2) lowering the density of the cast explosive from 1.72-1.75 to 1.66-1.70 for waxed torpex, and (3) lowering the compressive strength from 3700 psi to 1970 psi for waxed torpex. However, wax is used in service torpex for reasons of safety, since there is evidence that its presence lowers the sensitivity of the explosive to impact as measured by laboratory drop tests and bullet sensitivity tests of small charges (Bureau of Ord Res Mano Rpt No. 24, January 1945).

References: 76

(a) Committee of Div 2 and 8, NDRC, <u>Report on HBX and Tritonal</u>, OSRD No. 5406, 31 July 1945.

(b) Philip C. Keenan and Dorothy C. Pipes, <u>Table of Military High Explosives</u>, Second Revision, NAVORD Report No. 87-46, 26 July 1946.

(c) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

L. C. Smith and E. H. Eyster, Physical Testing of Explosives, Part III, Miscellaneous Sensitivity Tests, Performance Tests, OSRD Report No. 5746, 27 December 1945.

⁷⁶See footnote 1, page 10.

(d) G. H. Messerly, <u>The Rate of Detonation of Various Explosive Compounds</u>, OSRD Report No. 1219, 22 February 1943.

M. D. Hurwitz, <u>The Rate of Detonation of Various Compounds and Mixtures</u>, OSRD Report No. 5611, 15 January 1946.

(e) W. R. Tomlinson, Jr., <u>Blast Effects of Bomb Explosives</u>, PA Tech Div Lecture, 9 April 1948.

(f) Eastern Laboratory, du Pont, <u>Investigation of Cavity Effect</u>, <u>Sec</u> 111, <u>Variation of</u> <u>Cavity Effect with Explosive Composition</u>, NDRC Contract W672-ORD-5723.

(g) Also see the following Picatinny Arsenal Technical Reports on Torpex:

| <u>o</u> | <u>1</u> | 2 | 3 | <u>5</u> | <u>6</u> | <u>7</u> | <u>8</u> |
|----------|----------|------|------|------------------------------|----------|----------|----------|
| 1530 | 1651 | 1292 | 2353 | 1585 1635 1885 2355 | 1796 | 1797 | 1838 |

| Composition: % | Molecular Weight: (C ₆ H ₆ N ₆ O ₆) | 258 |
|---|--|-----------------|
| [%] ^{NH} ₂ | Oxygen Balance: | |
| | CO . % | -56 |
| H 2.3 0_2^{N} N 0_2 | CO, % CO % | - 19 |
| N 32.6 H ₂ N NH ₂ | Density: gm/cc Crystal | 1.93 |
| 0 37.2 ^{NO} 2 | Melting Point: °C 330 (b, e) | 360 (a) |
| C/H Ratio 0.302 | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | Boiling Point: "C | |
| Sample Wt 20 mg | Refractive Index, n ^D | |
| Picatinny Arsenal Apparatus, in. 11 Sample Wt, mg 7 | N25 | |
| Sample Wit, mg | n ₃₀ | |
| Friction Pendulum Test: | | |
| Steel Shoe | Vacuum Stability Test: cc/40 Hrs. at | |
| Fiber Shoe | 90°C | |
| | 100°C (a, b) | 0.3 6 |
| Rifle Bullet Impact Test: Trials | 120°C | |
| % Explosions | 135°C | |
| Portials | 150°C | |
| Burned | 200 Gram Bomb Sand Test: | |
| Unaffected | | |
| _ | Sand, gm | 42.9 |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) | Sensitivity to Initiation: Minimum Detonating Charge, gm | |
| 1 | Mercury Fulminate | |
| 5 | Lead Azide | 0,30 |
| 10 | Tetryl | |
| 15 20 | Ballistic Mortar, % TNT: | |
| 20 | Trauzi Test, % TNT: | |
| 75°C International Heat Te st: | | |
| % Loss in 48 Hrs | Plate Dent Test: Method | |
| 100°C Heat Test: | Condition | |
| % Loss, 1st 48 Hrs | Confined | |
| | Density, gm/cc | |
| | Brisance, % TNT | |
| Explosion in 100 Hrs None | | |
| Flammability Index: | Detonation Rate: Confinement | Non- |
| | Condition | None Brossod |
| Hygroscopicity: % | Charge Diameter, in. | Pressed 0.5 |
| | | |
| Volatility: | Density, gm/cc Rate, meters/second | 1.80 |

| Fragmentation Test: | Shaped Charge Effectiveness, TNT = 100: | | |
|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Stee Hole Volume Hole Depth | l Cones | |
| Total No. of Fragments: For TNT | Color: | Yellow | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib Total No. of Fragments: For TNT For Subject HE Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc | Principal Uses: Method of Loading: Loading Density: gm/cc At 50,000 p s i Storage: | Pressed 1.80 | |
| Blost (Relative to TNT): | Method Hazard Class (Quontity-Distance) | Dry | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation | | |
| Air, Confined: Impulse | Detonation Velocity: Density, gm/cc | (a, b. c) Meters/sec | |
| Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | 1.290 1.345 1.675 1.675 1.882 1.835 <u>Heat of:</u> Explosion, cal/gm | 5380 5628 6550 6575 7035 7220 2831 | |

Preparation:

(a)

Absolute alcohol (200 milliliters) was saturated with ammonia and then 12.5 gm (0.028 mol) of 1,3,5-tribromo-2,4,6-trinitrobenzene, prepared according to Hill (NAVORD Report No. 3709, 2 February 1953), was added. The flask was stoppered and allowed to stand at room temperature for a day. Additional ammonia was bubbled into the mixture, which was then heated under reflux for thirty minutes, filtered hot, and the insoluble product collected on a Buchner funnel. The product was washed with water, alcohol, and dried. The 4.7 gm of material recovered was recrystallized from nitrobenzene.

A disadvantage of the above method was that it could not be used for the preparation of large quantities of TATNB. Since it did not seem feasible to develop a new method of preparation, an investigation was made of the reported amination reactions (see Origin below). An attempt was made (Ref f) to find a modification which would produce high yields of a pure product. The process which evolved from this study may be summarized as follows (Ref f): 1,3,5-trichlorobenzene was nitrated "in one step" to 1,3,5-trichloro-2,4,6-trinitrobenzene in 85% yield. The crude nitration product was aminated in benzene with ammonia gas to TATNB, in yields of at least 95%.

Origin:

TATNE was prepared for the first time in 1888 by C. L. Jackson and J. F. Wing, who found the compound insoluble in alcohol, ether, chloroform, benzene, and glacial acetic acid; and soluble in nitrobenzene and aniline (Amer Chem Journal 10, 282 (1888)). B. Flurscheim and E. L. Holmes prepared TATNE from benzene free pentanitroaniline by gradually adding it to 10%aqueous ammonia (J Chem Soc, Pt 2,3045 (1928)). After boiling, an orange-yellow powder melting above 300° C was obtained. This product corresponded to that described by Jackson and Wing. These authors, as well as Palmer (Amer Chem Journal 14, 378 (1892)), attempted to reduce TATNE to hexa-aminobenzene. Either decomposition occurred or a hydrochloride of penta-aminobenzene was formed. Flurscheim and Holmes succeeded in reducing TATNE with phenylhydrazine by heating them together up to 200° C (J Chem Soc, Pt 1,334 (1929)) (Beil 13, 301 and EII, 147).

References: **

(a) F. Taylor, Jr., Synthesis of New High Explosives 11, Derivatives of 1,3,5-Tribromo-2,4,6-Trinitrobenzene, NAVORD Report No. 4405, 1 November 1956.

(b) L. D. Hampton, <u>Small Scale Detonation Velocity Measurements from May 1951 to May 1954</u>, NAVORD Report No. 3731, June 1954.

(c) E. M. Fisher and E. A. Christian, <u>Explosion Effects Data Sheets</u>, NAVORD Report No. 2986, 14 June 1955.

⁷⁷See footnote 1, page 10.

| Composition : % | Molecular Weight: $(C_6H_{12}N_2O_8)$ | 240 |
|--|--|----------------|
| c 29.9 H_2c H 5.4 H_2c | Oxygen Balance: CO, % CO % | -89 -27 |
| N 11.7 | Density: gm/cc 20°C 25°C | 1.33 1.32 |
| o 53.0 ^H 2 ^C | Melting Point: "C | |
| C/H Ratio 0.177 $H_2C < 20NO_2$ | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm 100+ | Boiling Point: °C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 43 Sample Wt, mg | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | 1.4540 |
| Friction Pendulum Test:Steel ShoeUnaffectedFiber ShoeUnaffected | Vacuum Stability Test: cc/40 Hrs, at 90°C | 0.45 |
| Rifle Bullet Impact Test: Trials % Explosions Partiols | 100°C 120°C 8 hours 135°C 150°C | 0.45 0.8 |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm | 14.7 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 223 10 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl | |
| 15 20 | Ballistic Mortar, % TNT: | |
| | Trauzl Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method | |
| 100°C Heat Test: % Loss, 1st 48 Hrs 1.8 % Loss, 2nd 48 Hrs 1.6 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement | Shelby steel |
| Hygroscopicity: % | Condition Charge Diameter, in. | Liquid 1.25 |
| Volatility: 60°C, mg/cm ² /hr 40 | Density, gm/cc Rate, meters/second | 1.33 Fails |

| Fragmentation Test: | |
|--|---|
| regnonation root. | Shaped Charge Effectiveness, $TNT = 100$: |
| 90 mm HE, M71 Projectile, Lot WC-91: | Glass Cones Steel Cones |
| Density, gm/cc | Hole Volume |
| Charge Wt, Ib | Hole Depth |
| Total No. of Fragments: | |
| For TNT | Color: |
| For Subject HE | |
| | Principal Uses: Ingredient of rocket and double |
| 3 inch HE, M42A1 Projectile, Lot KC-5: | base propellants |
| Density, gm/cc | |
| Charge Wt, Ib | |
| Total No. of Fragments: | |
| For TNT | Method of Loading: |
| For Subject HE | |
| | Loading Density: gm/cc |
| Fragment Velocity: ft/sec | |
| At 9 ft At 25½ ft | Storage: |
| Density, gm/cc | |
| | Method Liquid |
| Blast (Relative to TNT); | Hazard Class (Quantity-Distance) |
| A : | |
| Air: Peak Pressure | Compatibility Group |
| Impulse | Exudation |
| Energy | |
| | Solubility in Water, |
| Air, Confined: Impulse | $\frac{m/100 \text{ gm. at:}}{c^{-9}}$ |
| | 25 [°] C 0.55 60°C 0.68 |
| Under Water: | Solubility, gm/100 gm, |
| Peak Pressure | at 25°C, in: |
| Impulse Energy | Ether w |
| Energy | Alcohol ∞ 2: 1 Ether: Alcohol w |
| Underground: | Acetone |
| Peak Pressure | Viscosity, centipoises: |
| Impulse | Temp, 20 ^o C 13.2 |
| Energy | Hydrolysis, % Acid: |
| €eat of: | 10 days at 22°C 0.032 |
| Combustion, cal/gm 3428 | 5 days at 60°C 0.029 Japor Pressure: |
| Explosion, cal/gm 357 Gas Volume, cc/gm 851 | <u>oc</u> mm Mercury |
| 0)1 | 25 < 0.001 |
| | — <u> </u> |

Origin:

Lourenco prepared triethylene glycol in 1863 by heating glycol with ethylene bromide in a sealed tube at $115^{\circ}-120^{\circ}C$ (Ann (3) <u>67</u>, 275). Later in the same year Wurtz prepared triethylene glycol by heating ethylene oxide with glycol at $100^{\circ}C$. By action of nitric acid triethylene glycol was oxidized to $(H_2 \circ C \cdot C H_2 \circ - C H_2)_2$ (Ann (3) <u>69</u>, 331, 351).

The Germans and Italians were the first to prepare and use TECN during World War II as an ingredient of rocket and propellant powders. The commercial production of TEGN in quantity is still difficult and its use as a plasticizer for nitrocellulose is being replaced by other liquid nitrates.

Preparation:

Triethylene glycol is purified by fractional distillation under vacuum in an 18-inch Vigeaux fractioning column. The assembly as a whole is equivalent to 4.5 theoretical plates. The distillation is conducted using a 5 to 1 reflux ratio, at a pot temperature of approximately 180° C, and a take-off temperature of approximately 120° C.

The purified triethylene glycol (TEG) is nitrated by carefully stirring it into 2.5 parts of 65/30/5 nitric acid/sulphuric acid/water maintained at $0 \pm 5^{\circ}$ C. The rate of cooling is sufficient that 300 gm of TEG can be added within 40 minutes. The mixture is stirred and held at $0 \pm 5^{\circ}$ C, for 30 additional minutes. It is then drowned by pouring onto a large quantity of ice and extracted three times with ether. The combined extract is water-washed to a pH of about 4, shaken with an excess of sodium bicarbonate solution, and further washed with 1% sodium bicarbonate solution until the washings are colorless. The ethereal solution is water-washed until it has the same pH value as distilled water. It is carefully separated from excess water, treated with chemically pure calcium chloride to remove dissolved water, and filtered. The ether is removed by bubbling with dry air until a minimal rate of loss in weight is attained. The yield is 1.34 gm per gm TEG (84% of theoretical) and the nitrogen content of different batches range from 11.60 to 11.69% by the nitrometer method (calculated 11.67%).

References: 78

(a) See the following Picatinny Arsenal Technical Reports on TEGN:

| <u>3</u> | <u>5</u> | <u>6</u> | _7 | <u>8</u> |
|--------------|----------|-----------------------|---------------------|----------|
| 1953 2193 | 1745 | 1 78 6 2056 | 1767 1817 | 1638 |

⁷⁸See footnote 1, page 10.

Trimonite

| Copposition: | Molecular Weight | 217 |
|---|---|--------------------------|
| Picric Acid 88 - 90 Mononitronaphthalene 12 - 10 | Oxygen Belance: CO ₂ % CO % Density: gm/cc Cast Melting Point: "C int: "C | -62 -14 1.60 90 |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 10 | Boiling Point: "C Exp todes Refractive Index, n ^o ₂₀ n ^o ₂₅ n ^o ₃₀ | 300 |
| Friction Pendulum Test: Steel Shoe Fiber Shoe Rifle Bullet Impact Test: Trials | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C 120°C | 0.9 |
| %Explosions0Partials0Burned0Unaffected100 | 135°C 150°C 200 Gram Bomb Sand Test: Sand, gm | 44.2 |
| Explosion Temperature: °C Seconds, 0.1 (no cap used) ¹ ⁵ Decomposes 315 10 15 20 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl Ballistic Mortar, % TNT: | 0.20 0.04 |
| 75°C International Heat Test: % Lass in 48 Hrs 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Traurl Test, % TNT: Plate Dent Test: Method Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement Condition | None Cast |
| Hygroscopicity: % Volatility: | Charge Diameter, in. Density, gm/cc Rate, meters/second | 1.0 1.60 7020 |

<u>Trimonit e</u>

| Shaped Charge Effectiveness, TNT == 100: | | |
|---|---|--|
| Glass Cones Steel Cone Hole Volume Hole Depth | s | |
| Color: | | |
| Principal Uses: TNT substitute in pro and bombs |)jectiles | |
| Method of Loading: | Cast | |
| Loading Density: gm/cc | 1.60 | |
| Storage: Method | Dry | |
| Hazard Class (Quantity-Distance) | Class 9 | |
| Compatibility Group Exudation Exude | Group I a t 50°C | |
| Preparation: Picric acid and alpha-mononitron are melted together in an aluminum jacketed melt kettle equipped with Although picric acid alone requires perature for its melt loading (120° mixture forms a eutectic melting an must be taken to prevent the forman gerous metallic picrates. Trimonit interest as an emergency substitute | or tin steam a stirrer. s a high tem- C), the t 49°C. Care tion of dan- te is of | |
| | Glass Cones Steel Cone Hole Volume Hole Depth Color: Principal Uses: TNT substitute in proand bombs Method of Loading: Loading Density: gm/cc Storage: Method Hazard Class (Quantity-Distance) Compatibility Group Exude Preparation: Picric acid and alpha-mononitror are melled together in an aluminum jacketed melt kettle equipped with Although picric acid alone requires perature for its melt loading (1200 mixture forms a eutectic melting at must be taken to prevent the formatigerous metallic picrates. Trimonities | |

Trimonit e

Origin:

Trimonite, a castable mixture of picric acid/mononitronaphthalene was developed by the British during World War II as an improvement over tridite which is a mixture of 80/20 picric acid/dinitrophenol. Both mixtures are suitable for melt-loading below $100^{\circ}C$ and therefore represent an improvement over melt-loading picric acid alone (melting point $122^{\circ}C$). However, tridite is slightly inferior to picric acid as an explosive and dinitrophenol is objection-able because of its toxicity. Trimonite is also slightly inferior to picric acid and TNT as an explosive. Because of the low eutectic temperature of the picric acid-mononitronaphthalene mixture ($49^{\circ}C$), Tridite exudes when stored at elevated temperatures. It does not possess the disadvantages of picric acid (corrosive action on metals, ease of decomposition, etc.) and is a comparatively inexpensive substitute for TNT.

References: 79

(a) See the following Picatinny Arsenal Technical Reports on Trimonite:

| 2 | <u>5</u> | <u>6</u> | 8 |
|------|----------|----------|------|
| 1352 | 1325 | 926 | 1098 |
| 1372 | | 976 | 1838 |

⁷⁹See footnote 1, page 10.

2,2,2-Trinitroethyl-4,4,4-Trinitrobutyrate (TNETB)

AMCP 706-177

| Composition: | Molecular Weight: $(C_{6}H_{6}N_{6}O_{14})$ | 386 |
|---|--|---------------------------------|
| % C 18.6 H 1.6 | Oxygen Balance: <i>CO, %</i> CO % | -4.2 20.8 |
| H 1.6 N 21.8 (NO 2) 3 | Density: gm/cc Form I | 1.78 |
| c = 0 0 58.0 | Melting Point: "C | 93 |
| C/H Rotio 0.202 | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | Boiling Point: °C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg 50% point, cm (a) 20 | Refractive Index, n₂oForm I(e)Crvstal AxisαβΥ | 1.518 1.5 27 1.546 |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability lest: cc/40 Hrs, at 90°C | 0.60 |
| Rifle Bullet Impact Test: Trials % Explosions Partials | - 100°C 48 hrs 120°C 135°C 150°C | 0.60 |
| Burned Unaffected | 200 Gram Bomb Sand lest: Sand, gm | |
| Explosion Temperature: 0 Seconds, 0.1 (no cap used) 1 5 50% point (Alhot bar) (a) 225 10 45 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl | |
| 15 20 | Ballistic Mortar, % TNT: (b) | 136 |
| | Trauzi Test, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method | |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement | |
| Hygroscopicity: % 30°C, 90% RH 75°C, 5 months Nil (a) | Condition Charge Diameter, in. | |
| Volatility: | Density, gm/cc 1.60 Rate, meters/second 7760 | 1.76 8290 |

| Booster Sensitivity Test: Condition | | Decomposition Equation: Oxygen, otoms/sec | 4.4 x 10 ²¹ |
|--|------|--|------------------------|
| Tetryl, gm | | (Z/sec) | |
| Wax, in. for 50% Detonation | | Heat, kilocolorie/mole | 43.4 |
| Wax, gm | | (∆H, kcol/mol) Temperature Range, °C | |
| Density, gm/cc | | Phose | Liquid |
| | | | |
| Heat of: Combustion, col/gm | 1685 | Armor Plate Impact Test: | |
| Explosion, cal/gm | | 60 mm Mortar Projectile: | |
| Gas Volume, cc/gm | | 50% Inert, Velocity, ft/sec | |
| Formation, col/gm | 307 | Aluminum Fineness | |
| Fusion, cal/gm | 901 | | |
| Sublimation, cal/gm (est) | 804 | 500-16 General Purpose Bombs: | |
| Specific Heat: col/gm/°C | | Plate Thickness, inches | |
| | | 1 | |
| | | 11/4 | |
| | | 14 | |
| | | 13/4 | |
| Burning Rate: | | - · /+# | |
| cm/sec | | | |
| | | Bomb Drop Test: | |
| Thermal Conductivity: col/sec/cm/°C | | T7, 2000-15 Semi-Armor-Piercin | g Bomb vs Concrete: |
| | | | |
| Coefficient of Expansion: | | Max Safe Drop, ft | |
| Linear, %/°C | | 500-16 General Purpose Bomb | s Concrete: |
| Volume, %/°C | | Height, ft | |
| | | Trials | |
| Hardness, Mohs' Scale: | | Unaffected | |
| | | Low Order | |
| Young's Modulus: | | High Order | |
| E', dynes/cm ² | | | |
| E, Ib/inch ² | | 1000-lb General Purpose Bomb | vs Concrete: |
| Density, gm/cc | | | |
| | | Height, ft | |
| Compressive Strength: lb/inch ² | | Trials | |
| | | Unaffected | |
| Vapor Pressure: | (e) | Low Order | |
| °C mm Mercury 65 3.3 x 10_4 | | High Order | |
| 75 1.3 x | | | |
| $85 42 \times 10$ | | | |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | |
| 120 1.4×10^{-2} | | | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: |
|--|--|
| 90 mm HE, M71 Projectile , Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth |
| Total No. of Fragments: For TNT | Color: Colorless |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: |
| Fragment Velocity: ft/sec * A t9 ft | Loading Density: gm/cc Form I 1.783 Form II 1.677 Liquid, 99 ⁰ C , 1.551 |
| At 25½ ft Density, gm/cc | Storage: Method Wct |
| Blast (Relative to $H-6$; <u>Sphere</u> <u>Cylinder</u> (h) | Hazard Class (Quantity-Distance) |
| Air: 1-1b Charge: EW# EV# EW# EV# Peak Pressure 0.91 0.84 0.81 0.75 Impulse 0.73 0.67 0.74 0.69 Energy Energy Energy EN# EN# | Compatibility Group Exudation |
| | Bruceton Safety Test Results: (g) |
| | Mean and standard deviation of lengths of 0.300 diameter cylinder across which initia- tion is possible for 50% certainty: |
| | TNT 0.391 ± 0.040 RDX Comp B 0.381 ± 0.042 TNETB 0.920 ± 0.059 |
| Underground: Peak Pressure | Absolute Viscosity, poises: (e) |
| Impulse Energy *EW, equivalent weight of H-6 for a unit weight of test mixture for equal performance at the same test distance; EV, equivalent volume of E-6 for a unit volume of test mixture for equal performance at the same test distance. | Temp, 98.9°C 0.173 106.5°C 0.138 |
| | |

2,2,2-Trinitroethyl-4,4,4-Trinitrobutyrate (TNETB)

| Solubility (Room Temperature): | (a) | |
|---|--|--------------------|
| Solvent | Solubility | |
| Water n-Hexane Carbon tetrachloride Ethanol Chloroform Benzene Nitromethane Glacial acetic acid Ethyl acetate | Insoluble Insoluble Insoluble 5 gm/100 gm solvent 10 gm/100 gm solvent Very soluble Very soluble Very soluble Very soluble | And a statistic as |

| TNETB Forms | Eutectics | With | the | Following | Compounds: | (a) |
|-------------|-----------|------|-----|-----------|------------|-----|
| | | | | | | |

| a di manana panta provan | TNT BTNES (bis(trinitroethyl) succinate) BTNEN (bis(trinitroethyl) nitramine) TNB (trinitrobenzene) Compound A (C4HGN 07 formed by condensation of 1,1-dinitroethane) Trinitroethyl trinitrobenzoate (27%) | 57 80+ 68.5 65 77 80.5 (f) |
|--------------------------|--|---|
| - | Timitioenyi minitiobenzoate (21%) | |

Crystallographic Data:

Prenaration.

Three polymorphic crystalline forms have been observed. Low temperature Form I goes through a solid-solid transition at 89° C giving Form II. Form II has a melting point of 92.5° to 93°C. On cooling, Form II does not transform reversibly to Form I when 89° C is reached. However, Form II will transform to Form I at room temperature, usually taking a few hours to do so. Form III was observed, which appeared to be stable over a very narrow temperature range on the order of 0.2° to 0.3° C near 92.5°C.

(d)

(a)

| (NO2)3ссн ⁵ сн ⁵ сн ⁵ сост + (NO ⁵) ³ сн | DOH . | H2SO4 |
|--|-----------------|------------------|
| trinitrobutyryl chloride trinitroet | | sulfuric acid |
| (NO2) 3 CCH 2 CH 2 COOCH 2 C (NO2) 3 + | HCl | ~~~~~ |
| 2,2,2-trinitroethyl-4,4,4-trinitro- butyrate | hydrocl acid | |

Laboratory experiments indicate that the present slow step involving overnight treatment of 4,4,4-trinitrobutyryl chloride with 2,2,2-trinitroethanol and aluminum chloride can be replaced by a fast and simple esterification in sulfuric acid. Using 100% sulfuric acid or fortified H_2SO_h , the ester can be prepared in yields of 95% to 98% in 24 hours at 25°C, in 5 hours at 50°C, or in 3 hours at 65°C. Above 65°C the reaction time is less, but the yield falls off" and a less pure product is obtained. The crude white crystalline product on recrystallization from dilute methanol gives a material melting at 92° to 93°C.

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Origin:

(e)

TNETE belongs to a new class of explosives characterized by trinitromethyl groups, $-C(NO_2)_2$. The chemistry of this class of compounds was studied in Germany by Drs. Schenck and Schimmelschmidt, who discovered in 1942-1943 that trinitromethane or nitroform, HC(NO₂)₃, was the source of new explosive derivatives. Dr. Schenck prepared the stable solid alcohol, 2,2,2-trinitroethanol, from nitroform and formaldehyde. Dr. Schimmelschmidt reacted nitroform with unsaturated organic compounds, such as acrylic acid, and predicted in 1943 that the ester of 4,4,4-trinitrobutyric acid with trinitroethanol would be an interesting explosive.

In 1947 the U.S. Navy began a program to explore these compounds. The initial task of investigating the chemistry of trinitroethanol was undertaken by the Hercules Powder Company (Navy Contract Nord-19925). The U.S. Rubber Company studied the chemistry of nitroform (Navy Contract Nord-10,129). After preparation of the first laboratory samples of TNETB, considerable interest was aroused. In early 1950 the Naugatuck Chemical Division of U.S. Rubber Company was assigned to prepare 100 pounds of TNETB. The Bureau of Ordnance in July 1953 raised the production to 800 pounds with the assistance of the Hercules Powder Company in augmenting the production at Naugatuck (Navy Contract NOrd-11,280). TNETB is a high oxygen content explosive.

References: 80

(a) J. M. Rosen, <u>Properties of Trinitroethyl Trinitrobutyrate TNETB</u>, NAVORD Report No. 1758, 17 December 1950.

(b) Bureau of Mines Report No. 3107, Part IX, <u>Ballistic Mortar Tests on Trinitroethyl</u> <u>Trinitrobutyrate</u>, 5 April 1950.

(c) L. D. Hampton and G. Svadeba, Evaluation of 2,2,2-Trinitroethyl-4,4,4-Trinitrobutyrate as a Constituent of Castable Explosives, NAVORD Report No. 2614, 30 September 1952.

(d) U.S. Rubber Company Quarterly Progress Report No. 23, <u>Synthesis of New Propellants</u> and <u>Explosives</u>, Navy Contracts Nord-10-129 and -12,663, 19 August 1953.

(e) M. E. Hill, O. H. Johnson, J. M. Rosen, D. V. Sickman and F. Taylor, Jr., <u>Preparation</u> and Properties of TNETB, a New Castable High Explosive, NAVORD Report No. 3885, 27 January 1955.

(f) M. E. Hill, Synthesis of New High Explosives, NAVORD Report No. 2965, 1 April 1953.

(g) Jacob Savitt, A Sensitivity Test for Castable Liquid Explosives, Including Results for Some New Materials, NAVORD Report No. 2997, 22 October 1953.

(h) R. W. Gipson, <u>Sensitivity of Explosives</u>, IX: <u>Selected Physico-Chemical Data of Ten</u> <u>Pure High Explosives</u>, <u>NAVORD Report No. 6130</u>, 18 June 1958.

⁸⁰See footnote 1, page 10.

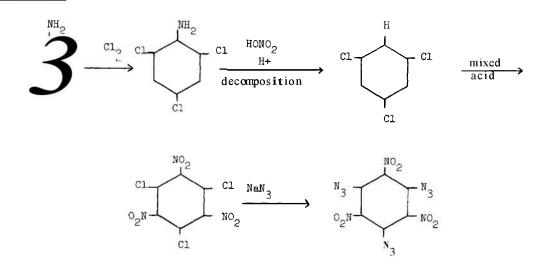
| Composition: | Molecular Weight: $(C_6O_6N_{12})$ | 3 36 |
|--|--|-------------|
| $\begin{array}{c} \text{NO}_2\\ \text{C} & 21.4\\ \text{N} & 50.0 \end{array}$ | Oxygen Balance: CO, % CO % | -29 0.0 |
| | Density: gm/cc Crystal | 1.81 |
| 0 20.0 2 7 - | Melting Point: "C Decomposes | 1.31 |
| C/H Ratio | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm(a) ≤ 25 | Boiling Point: "C | |
| Sample Wt 20 mg Picatinny Arsenal Apparatus, in. Sample Wt, mg | Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| Friction Pendulum Test: Steel Shoe Fiber Shoe | Vacuum Stability Test: cc/40 Hrs, at 90°C 100°C | |
| Rifle Bullet Impact Test: Trials % Explosions Partials | 120°C 135°C 150°C | |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm | |
| Explosion Temperature: "C (a) Seconds, 0.1 (no cap used) 1 5 150 10 15 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl | |
| 20 | Ballistic Mortar, % TNT: | |
| | Trausl Test, % PETN: | 90 |
| 75°C International Heat Test: % Loss in 48 Hrs | Plate Dent Test: Method | |
| 100°C Heat Test: % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs Explosion in 100 Hrs | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement | |
| Hygroscopicity: % 30 [°] C, 90% RH 0.00 | Condition Charge Diameter, in. | |
| Volatility: | Density, gm/cc Rate, meters/second | |

Trinitro Triazidobenzene

| Fragmentation Test: | Shaped Charge Effectiveness, TNT = 100: | : | | |
|---|--|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Con Hole Volume Hole Depth | es | | |
| Total No. of Fragments: For TNT | Color: Greenish-ye | ellow | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: | Principal Uses: (c) Ingredient of | primer mix | | |
| Density, gm/cc Charge Wt, lb | | | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Pr Dead presses at about 42,000 p | ressed osi | | |
| Fragment Velocity: ft/sec | Loading Density: gm/cc A t 42,000 p s i | 1.75 | | |
| At 9 ft At 25½ ft Density, gm/cc | Storage: | | | |
| Blast (Relative to TNT): | Method Hazard Class (Quontity-Distance) | | | |
| Air: Peak Pressure | Compatibility Group | | | |
| Impulse Energy | | None | | |
| Air, Confined: Impulse | Qualitative Solubilities at Room Temperature: Solvent | Solubility | | |
| Under Water: Peak Pressure Impulse | Chloroform Mode | ily soluble erately soluble ingly soluble luble | | |
| Energy Underground: Peak Pressure | Commatibility with Metals: Wet: Does not attack iron, st or brass. | Wet: Does not attack iron, steel, copper | | |
| Impulse Energy | Heat of: Combustion, cal/gm (a) | 2554 | | |
| | Burning Rate: (b) cm/sec | 0.65 | | |
| | | | | |

Trinitro Triazidobenzene

Preparation: (e)



Aniline is chlorinated to form trichloroaniline. The amino group is eliminated by the diazo reaction. The resulting sym-trichlorobenzene is nitrated. This nitration is carried out by dissolving the material in warm 32% oleum, adding strong nitric acid, and heating to $140^{\circ}-150^{\circ}$ C until no trinitro trichlorobenzene (melting point 187° C) precipitates (Ref f). The chlorine groups are then replaced by azo groups. This is accomplished by adding an acetone solution of the trinitro trichlorobenzene, or better, and powdered substance alone, to an actively stirred solution of sodium azide in alcohol. The precipitated trinitro triazidobenzene is collected on a filter, washed with alcohol, water and dried. It may be purified by dissolving in chloroform, allowing the solution to cool, and collecting the greenish yellow crystals (melting point 131° C with decomposition).

Origin:

This initiating explosive was first prepared in 1923 by Turek who also perfected its manufacture.

References:81

(a) S. Helf, <u>Tests of Explosive Compounds Submitted by Arthur D. Little</u>, Inc., PATR 1750, 24 October 1949.

(b) A. F. Belyaeva and A. E. Belyaeva CR a.s. USSR <u>52</u>, 503-505 (1946) Chemical Abstracts <u>41</u>, 4310.

A. E. Belyaeva and A. F. Belyaeva, Doklady Akad Nauk. USSR 56, 491-494 (1947).

(c) French Patent 893,941, 14 November 1944 (Chemical Abstracts 47, 8374).

(d) A. D. Yoffe, "Thermal Decomposition and Explosion of Azides," Proc. Roy Soc A208, 188-199 (1951).

(e) T. L. Davis, The Chemistry of Powder and Explosives, John Wiley and Sons, Inc.,

(f) 0. Turek, Chim et Ind <u>26</u>, 781 (1931); German Patent 498,050; British Patent 298,981.

New York (1943), p. 436.

⁸¹See footnote 1, page 10.

| Composition: | Molecular Weight: (C ₁₅ H ₂₄ N ₈ O ₂₆) | 732 |
|--|---|----------------|
| % C 24.6 H 3.3 N 15.3 O 56.8 | Oxygen Balance: CO ₂ % CO % | -35 |
| $\begin{array}{c} \text{CH} \text{ONO} \text{CH} \text{ONO} \text{CH} \text{ONO} \\ 1 & 2 & 1 & 2 & 1 & 2 \\ 1 & 2 & 1 & 2 & 1 & 2 \\ \end{array}$ | Density: gm/cc Crystal | 1.58 |
| 02NOCH2CH2OCH2CCH2OCH2CCH2ON02 | Melting Point: "C 82 | to 84 |
| C/H Rotic 0.115 | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm Sample Wt 20 mg Picatinny Arsenal Apparatus, in. 9 Sample Wt, mg 24 | Boiling Point: "C Refractive Index, n ^D ₂₀ n ^D ₂₅ n ^D ₃₀ | |
| Friction Pendulum Test: Steel Shoe Unaffected Fiber Shoe Unaffected | Vacuum Stability Test: cc/40 Hrs, at 90°C | |
| | 100°C Pure | 2.45 |
| Rifle Bullet Impact Test: Trials % Explosions Partials | 120°C Specially purified 135°C 150°C | 1.94 |
| Burned Unaffected | 200 Gram Bomb Sand Test: Sand, gm | 58.9 |
| Explosion Temperature: "C Seconds, 0.1 (no cap used) 1 5 225 10 15 | Sensitivity to Initiation: Minimum Detonating Charge, gm Mercury Fulminate Lead Azide Tetryl | 0.30 |
| 20 | Ballistic Mortar, % TNT: | |
| 75°C International Heat Test: % Loss in 48 Hrs | Trauzl Test, % TNT: Plate Dent Test: Method | |
| 100°C Heat Test: % Loss, 1st 48 Hrs 1.15 % Loss, 2nd 48 Hrs 0.75 Explosion in 100 Hrs None | Condition Confined Density, gm/cc Brisance, % TNT | |
| Flammability Index: | Detonation Rate: Confinement | None |
| Hygroscopicity: % | Condition Charge Diameter, in. | Pressed 0.5 |
| Volatility: | Density, gm/cc Rate, meters/second | 1.56 7650 |

Tripentaerythritol Octanitrate (TPEON)

| Booster Sensitivity Test: Condition Tetryl, gm Wax, in. for 50% Detonation Wax, gm Density, gm/cc Heat of: Combustion, cal/gm Explosion, cal/gm Formation, cal/gm Fusion, cal/gm | 2632 1085 762 | Decomposition Equation: Oxygen, otoms/sec (Z/sec) Heat, kilocalarie/mole (AH kcal/mol) Temperature Range, °C Phase Armor Plate Impact Test: 60 mm Mortar Projectile: 50% Inert, Velocity, ft/sec Aluminum Fineness 500-lb General Purpose Bombs: | 23.1 215 to 250 Liquid |
|--|---------------------|---|------------------------------|
| Specific Heat: col/gm/°C <u>Specific Impulse:</u> | | Plate Thickness, inches | |
| lb-sec/lb (calculated) | 240 | 1 1 ¼ 1 ¼ 1 ¾ | |
| Burning Rate: cm/sec | | Bomb Drop Test: | |
| Thermal Conductivity: col/sec/cm/ "C | | T7, 2000-Ib Semi-Armor-Piercing E | Bomb vs Concrete: |
| Coefficient of Expansion: Linear, %/"C | | Max Safe Drop, ft 500-Ib General Purpose Bomb vs 0 | Concrete: |
| Volume, %/°C | | Height, ft | |
| Hardness, Mohs' Scale: | | Trials Unoffected | |
| Young's Modulus: E', dynes/cm² E, lb/inch² Density, gm/cc | | Low Order High Order 1000-Ib General Purpose Bomb vs (| Concrete: |
| Compressive Strength: Ib/inch ² | | Height, ft Trials Unaffected | |
| Vopor Pressure: °C mm Mercury | | Low Order High Order | |
| | | | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | | | |
|--|---|--|--|--|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | | | |
| Total No. of Fragments: For TNT | Color: White | | | |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: High explosive and as possible plasticizer for nitrocellulose | | | |
| Total No. of Fragments: For TNT For Subject HE | Method of Loading: Cast or pressed | | | |
| Fragment Velocity: ft/sec At 9 ft | Loading Density: gm/cc Pressed at 60,000 psi 1.565 | | | |
| At .25½ ft Density, gm/cc | Storage: Method Dry | | | |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | | | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation None | | | |
| Air, Confined: Impulse | Hygroscopicity,, Gain or Loss in Wt, %: <u>Time, Hrs</u> % RH at 30 ⁰ C | | | |
| Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | |
| | Acetone, hot Very soluble Benzene, hot Very soluble | | | |

| | NTN | PEIN , | RDX | TPEON |
|--|-----|--------|-----|-------|
| | | | | |
| | | | | |
| | | | | |
| | | | | |

Origin:

Twenty grams (0.054 mol) of nitration grade tripentaerythritol (TPE) (99%) minimum purity) were slowly added, with stirring, to 160 gm (2.55 mol) of 99% nitric acid at a temperature of -25° to 0°C. On equivalent weight basis, this quantity of 99% nitric acid corresponds to an excess of 6.3 times the TPE used. After addition of the TPE, the reaction mixture was stirred for about one hour at 0° to 5°C and poured into eight times its volume of cracked ice. The product, when allowed to stand overnight, was crushed under water; filtered with suction; and washed copiously with water. It was then treated twice with about 5 times its weight of a 1% ammonium carbonate solution, stirred for several hours, filtered and washed with water until the final washings were neutral to litmus. The final product was washed successively with 50 cc each of ethanol and ether. The material dried in air weighed 37.8 gm or 96% of theory based on TPE. It had a melting range of 71° to 74°C. Crystallization of the crude TPEON from chloroform was found to be the most suitable method of obtaining pure TPEON.

TPEON prepared by the reaction of tripentaerythritol and 99% nitric acid at 0° to 10° C was reported by Wyler in 1945 (J. A. Wyler to Trojan Powder Company: U.S. Patent 2,389, 228, 20 November 1945).

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(b) K. Namba, J. Yamashita and S. Tanaka, "Pentaerythritol Tetranitrate," J Ind Explosives Soc (Japan) 15, 282-9 (1954); CA 49, 11283 (1955).

(c) S. D. Brewer and H. Henkin, The Stability of PEIN and Pentolite, OSRD Report No. 1414.

(d) E. Berlow, R. H. Barth and J. E. Snow, <u>The Pentaervthritols</u>, ACS Monograph No. 136, Reinhold Publishing Corporation, New York, 1958.

⁸²See footnote 1, page 10.

Tritonal, 80/20

| Composition: % | | Molecular Weight: | | 81 |
|--|------------|---|----------|-------------------------------|
| TNT | 80 | Oxygen Balance: | | |
| | 00 | 00, % | | -77 |
| Aluminum | 20 | CO % | | -38 |
| | | Density: gm/cc | Cast | 1.72 |
| | | Melting Point: "C | | |
| C/H Ratio | | Freezing Point: "C | | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | 85 | Boiling Point: "C | | |
| Sample Wt 20 mg | 10 | Refractive Index, n ^o ₂₀ | | |
| Picatinny Arsenal Apparatus, in, Sample Wt, mg | 13 16 | Π <mark>2</mark> 5 | | |
| | 10 | n ₃₀ | | |
| Friction Pendulum Test: | | Vacuum Stability Test: | | |
| Steel Shoe | Unaffected | cc/40 Hrs, at | | |
| Fiber Shoe | Unaffected | 90°C | | |
| Rifle Bullet Impoct Test: Trials | | 100°C | | 0.1 |
| 0/- | | 120°C | | 0.2 |
| | | 135°C | | |
| | | 150°C | | 0.8 |
| | | 200 Gram Bomb Sand Test: | | |
| | | Sand, gm | | |
| | | Sensitivity to Initiation: | | |
| | | Minimum Detonating Ch | arge, gm | |
| | | Mercury Fulminate | | |
| | | Lead Azide | | 0.20 |
| | | Tetryl | | 0.10 |
| | | Ballistic Mortar, % TNT: | (a) | 124 |
| ⁷ 5°C International Heat Test: | | Traurl Test, % TNT: | (b) | 125 |
| % Loss in 48 Hrs | | Plate Dent Test: Method | (c) | В |
| 00°C Heat Test: | | Condition | | Cast |
| | | Confined | | NO |
| % Loss, 1st 48 Hrs | | | | |
| % Loss, 1st 48 Hrs % Loss, 2nd 48 Hrs | | Density, gm/cc | | 1.75 |
| | | | | |
| % Loss, 2nd 48 Hrs Explosion in 100 Hrs | | Density, gm/cc | | 1.75 9 3 |
| % Loss, 2nd 48 Hrs | 100 | Density, gm/cc Brisance, % TNT | None | 1.75 |
| % Loss, 2nd 48 Hrs Explosion in 100 Hrs Iammability Index: | | Density, gm/cc Brisance, % TNT Detonation Rate: Confinement Condition | Cast | 1.75 93 None Pressed |
| % Loss, 2nd 48 Hrs Explosion in 100 Hrs | 100 | Density, gm/cc Brisance, % TNT Detonation Rate: Confinement | | 1.75 93 None |

Tritonal, 80/20

AMCP 706-177

.

| Booster Sensitivity lest: (d) Condition Tetryl, gm Wax, in. for 50% Detonation Wax, gm Density, gm/cc | Cast 100 0.58 1.75 | Decomposition Equation: Oxygen, otoms/sec (Z/sec) Heat, kilocolorie/mole (AH kcol/mol) Temperature Range, °C Phase | | |
|---|---|--|---|--|
| Heat of: (c) Combustion, col/gm Explosion, col/gm Gas Volume, cc/gm Formation, col/gm Fusion, col/gm | 4480 1770 | Armor Plate Impact lest: 60 mm Mortar Projectile: 50% Inert, Velocity, ft/se Aluminum Fineness 500-Ib General Purpose Boml | 100 | >1100 12 |
| Specific Heat: col/gm/°C (b) At -5 [°] C Density, gm/cc At 20 [°] C | 0.23 1.74 0.31 | Plate Thickness, inches 1 11/4 11/ <u>4</u> 13/4 | <u>Trials</u> 0 16 6 0 | <u>% Inert</u> 100 33 |
| Burning Rate: cm/sec Thermal Conductivity: col/sec/cm/"C, (b) Density, gm/cc Coefficient of Expansion: Linear, %/°C | 11 x 10 ⁻⁴ 1.73 | Bomb Drop lest: (e 17, 2000-lb Semi-Armor-Pier Max Safe Drop, ft | rcing Bomb vs | |
| Volume, %/°C Hardness, Mohs' Scale: | | 500-Ib General Purpose Bon Height, ft Trials Unaffected | <u>Seal</u> <u>4,000</u> 34 32 | s: <u>Seal</u> 5,000 14 14 |
| Young's Modulus: (b) E, dynes/cm ² E, Ib/inch ² Density, gm/cc | 6.67 x 10 ¹⁰ 0.97 x 10 ⁶ 1.72 | Low Order High Order 1000-Ib General Purpose Bor | 0 2 mb vs Concrete | 0 0 <u>Seal</u> 5,000 |
| Compressive Strength: Ib/inch ² (b) Density, gm/cc Vapor Pressure: °C mm Mercury | 2340 1.75 | Height, ft Trials Unaffected Low Order High Order | | 24 23 0 1 |
| | | | | |

| Fragmentation Test: | | Shaped Charge Effectiveness, $TNT = 100$ | : |
|--|----------------------|--|--|
| 90 mm HE, M71 Projectile, Lot WC-9 Density, gm/cc Charge Wt, Ib | 1: 1.71 2.272 | Glass Cones Steel Con Hole Volume Hole Depth | nes |
| Total No. of Fragments: For TNT For Subject HE | 7 03 616 | Calor: | Gray |
| 3 inch HE, M42A1 Projectile, Let KC-5 Density, gm/cc Charge Wt, Ib | | Principal Uses: OP bombs | |
| Total No. of Fragments: For TNT For Subject HE | 514 485 | Method of Loading: | Cast |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc | 2460 2380 1.72 | Loading Density: gm/cc l | 65-1.72 |
| Bbst (Relative to TNT): | (f) | Hazard Class (Quantity-Distance) | Class 9 |
| Air: Peak Pressure Impulse Energy | 110 115 119 | Compatibility Group Exudation | Group I |
| Air, Confined: Impulse | 130 | Preparation: Tritonal is prepared by adding ' aluminum separately to a steam-ja | |
| Under Water: Peak Pressure Impulse Energy | 105 118 119 | kettle equipped with a stirrer. I the kettle and mixing of the ingre- continued until all the TNT is me the viscosity of the mixture is c satisfactory (about 85°C), the tr: | Heating of edients are elted. When onsidered itonal is |
| Underground: Peak Pressure Impulse Energy | 117 127 136 | poured into projectiles or bombs TNT. | the same as |
| | | | |

Origin:

The Addition of aluminum to increase the power of explosives was proposed by Escales in 1899 and patented by Roth in 1900 (German Patent 172, 327). Some recent studies, directed towards establishment of the optimum amount of aluminum in the TNT/Aluminum system, have shown that (1)the blast effect increases to a maximum when the aluminum content is 30% (Ref g); the brisance, as measured by the Sand Test, passes through a maximum at about 17% aluminum (Ref h); in Fragmentation Tests, no maximum is observed, additions of aluminum causing a decrease in efficiency over the entire range from 0% to 70% aluminum (Ref i); and (4) the rate of detonation of cast charges is continuously decreased by additions of aluminum up to 40% (Ref j). For all practical purposes it is concluded that the addition of 18% to 20% aluminum to TNT improves its performance to a maximum. This conclusion is in agreement with that of British workers who measured performance of aluminized TNT-mixtures based on extensive Lead Block Test data (Ref k).

Tritonal, consisting of 80% TNT and 20% aluminum, was developed and standardized in the United States during World War II for use in bombs.

References:83

(a) L. C. Smith and E. H. Eyster, <u>Physical Testing of Explosives</u>, <u>Part 111</u>, <u>Miscellaneous</u> <u>Sensitivity Tests</u>; <u>Performance Tests</u>, OSRD Report No. 5746, 27 December 1945.

(b) Philip C. Keenan and Dorothy Pipes, <u>Table of Military High Explosives</u>, Second Revision, NAVORD Report No. 87-46, 26 July 1946.

(c) D. P. MacDougall, Methods of Physical Testing, OSRD Report No. 803, 11 August 1942.

(d) L. C. Smith and S. R. Walton, <u>A Consideration of RDX/Wax Mixtures as a Substitute for Tetryl in Boosters</u>, NOL Mano 10,303, 15 June 1949.

(e) Committee of Div 2 and 8, NDRC, <u>Report on HBX and Tritonal</u>, OSRD No. 5406, 31 July 1945.

(f) W. R. Tomlinson, Jr., <u>Blast Effects of Bomb Explosives</u>. PA Tech Div Lecture, 9 April 1948.

(g) W. B. Kennedy, R. F. Arentzen and C. W. Tait, <u>Survey of the Performance of TNT/A1 on</u> the Basis of Air-Blast Pressure and Impulse, OSRD Report No. 4649, Division 2, Monthly Report No. AES-6, 25 January 1945.

(h) W. R. Tomlinson, Jr., <u>Develop New High Explosive Filler for AP Shot</u>, PAIR No. 1290, First Progress Report, 19 May 1943.

(i) W. R. Tomlinson, Jr., <u>Develop New High Explosive Filler for AP Shot</u>, PATR No. 1380, Second Progress Report, 12 January 1944.

(j) L. S. Wise, Effect of Aluminum on the Rate of Detonation of TNT, PATR No. 1550, 26 July 1945.

(k) Armament Research Dept, <u>The Effect of Aluminum on the Power of Explosives</u>, British Report AC-6437, May 1944 (Explosives Report 577/44).

83See footnote 1, page 10.

<u>Tritonal, 80/20</u>

(1) Also see the following Picatinny Arsenal Technical Reports on Tritonal:

| <u>o</u> | 3 | 4 | <u>5</u> | 6 | <u></u> <i>Z</i> | 8 |
|----------------------|--------------|------|----------|------|------------------|------|
| 1530 1560 2010 | 1693 2353 | 1444 | 1635 | 1956 | 1737 2127 | 2138 |

| Composition: | | Molecular Weight: | 281 |
|---|------------|---|--------------|
| % HMX | 70.0 | Oxygen Balance: | |
| Nitrocellulose (13.15% N) | 15.0 | CO ₂ % | -26 |
| Nitroglycerin | 10.7 | co % | -0.5 |
| 2-Nitrodiphenylamine | 1.3 | Density: gm/cc Pressed | 1.72 |
| Triacetin | 3.0 | | |
| | | Melting Point: "C | |
| C/H Ratio | | Freezing Point: "C | |
| Impact Sensitivity, 2 Kg Wt: Bureau of Mines Apparatus, cm | | Boiling Point: "C | |
| Sample Wt 20 mg | | Refractive Index, n ^D ₂₀ | |
| Picatinny Arsenal Apparatus, in. Sample Wt, mg | | n ₂₅ | |
| campo IV, mg | | n _{so} | |
| Friction Pendulum Test: | | Vacuum Stability Test: | |
| Steel Shoe | Unaffected | cc/40 Hrs, at | |
| Fiber Shoe | Unaffected | 90°C | |
| Rifle Bullet Impact lest: Trials | | 100°C | 1.29 |
| ········- | | 120°C 29 hours | 11+ |
| % Explosions | | 135°C | |
| Partiols | | 150°C | |
| Burned | | 200 Gram Bomb Sand Test: | |
| | | | CC 1 |
| Unaffected | | Sand, gm | 66.4 |
| Explosion Temperature: "C | | Sensitivity to Initiation: | |
| Seconds, 0.1 (no cap used) | | Minimum Detonating Charge, gm | |
| 1 | | Mercury Fulminate | |
| 5 | | Lead Azide | 0.30 |
| 10 | | Tetryl | |
| 15 | | | |
| 20 | | Ballistic Mortar, % TNT: | |
| 75°C International Heat Test: | | Trauzi Test, % TNT: | |
| % Loss in 48 Hrs | | Plate Dent Test: | |
| | | Method | |
| 90 'C Heat Test: | | Condition | |
| % Loss, 1st 48 Hrs | 0.28 | Confined | |
| % Loss, 2nd 48 Hrs | 1.12 | Density, gm/cc | |
| Explosion in 100 Hrs | None | Brisance, % TNT | |
| | | Detonation Rate: | |
| Flammability Index: | | Confinement | |
| | | - Condition | |
| Hygroscopicity: % | | Charge Diameter, in. | |
| | | Density, gm/cc | |
| Volatility: | | Rate, meters/second (calculated) | 8 500 |

*See footnote on following page.

.

| Booster Sensitivity Test: Condition Tetryl, gm Wax, in. for 50% Detonation Wax, gm Density, gm/cc | Decomposition Equation: Oxygen, atoms/sec (Z/sec) Heat, kilocolorie/mole (AH kcol/mol) Temperature Range, °C Phase |
|--|---|
| Hoot of: Combustion, co l/gm 2359 Explosion, col/gm 1226 Gas Volume, cc/gm Formation, col/gm Fusion, col/gm | Armor Plate Impact Test: 60 mm Mortor Projectile: 50% Inert, Velocity, ft/sec Aluminum Fineness 500-lb General Purpose Bombs: |
| Compression at Rupture:\$8.26Work to Produce Rupture:ft-lb/inch ³ 9.62 | Plate Thickness, inches 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 |
| Burning Rate: cm/sec Thermal Conductivity: col/sec/cm/"C | Bomb Drop Test: T7, 2000-Ib Semi-Armor-Piercing Bomb vs Concrete: |
| Coefficient of Expansion: Linear, %/°C | Max Safe Drop, ft 500-lb General Purpose Bomb vs Concrete: |
| Volume, %/°C Hardness, Mohs' Scale: | Height, ft Trials Unaffected |
| Young's Modulus:E', dynes/cm2 0.24×10^{10} E, lb/inch2 0.35×10^{5} Density, gm/cc | Low Order High Order 1000-Ib General Purpose Bomb vs Concrete: |
| Compressive Strength: Ib/inch ² 2720 | Height, ft Trials Unaffected |
| Vapor Pressure: "C mm Mercury | Low Order High Order |
| *Name assigned by Dr. Mark M. Jones, formerly of PA; based on original development by James H. Veltman. | |

| Fragmentation Test: | Shaped Charge Effectiveness, $TNT = 100$: | |
|---|--|-------------------|
| 90 mm HE, M71 Projectile, Lot WC-91: Density, gm/cc Charge Wt, Ib | Glass Cones Steel Cones Hole Volume Hole Depth | |
| Total No. of Fragments: For TNT | Color: | Orange |
| For Subject HE 3 inch HE, M42A1 Projectile, Lot KC-5: Density, gm/cc Charge Wt, Ib | Principal Uses: High mechanical strength machinable explosive | 1 |
| Total No. of Fragments: For TNT For Subject HE | Method of Looding: | Pressed |
| Fragment Velocity: ft/sec At 9 ft At 25½ ft Density, gm/cc | Loading Density: gm/cc A t 6,700 psi Storage: Method | 1.72 Dry |
| Blast (Relative to TNT): | Hazard Class (Quantity-Distance) | |
| Air: Peak Pressure Impulse Energy | Compatibility Group Exudation Machinability | None Excellent |
| Air, Confined: Impulse Under Water: Peak Pressure Impulse Energy Underground: Peak Pressure Impulse Energy | | |
| | | |

Preparation:

The preparation of this class of explosive compositions is illustrated by the method used for Veltex No. 448: Place 675 cc of water in a slurry kettle equipped with an agitator. Add 5.85 gn of 2-nitrodiphenylamine and agitate for several minutes to obtain dispersion. Then add 93.7 gm of water-west nitrocellulose (dry weight 67.5 gm) in small portions. Raise the temperature to 48° C and maintain this temperature, but continue the agitation. A mixture of 48.2 gm of nitroglycerin and 13.5 gm of triacetin is added over a 5-minute period, with the mixing continuing for an additional 10 minutes at 48° C. The HMX (350 gm) is added over a 5-minute period with agitation continued for 30 minutes at 48° C. The slurry is cooled to room temperature and filtered. The filter cake is dried to a moisture content between 8% and 12%. The incorporation of this mix is completed by rolling 50 gm portions at a temperature of approximately 90°C. The finished colloid is then preheated on a heat table at 66° C. Increments of 25 gm each are pressed at 6700 psi for four minutes at 71° C. A cylinder is then built up by pressing together four 25 gm increments for a dwell time of 15 minutes.

Origin:

Veltex is the name given to a series of closely related nitrocellulose compositions prepared in 1957 at Picatinny Arsenal by the solventless process used for propellants. These compositions all contain a high percentage of solid high explosive. They were investigated to determinate the suitability of the Holtex type explosive developed by Hispano Suiza of Switzerland, France and Spain, but for which the composition was not reported (Ref a). Compositions similar to Veltex No. 448 and containing 60% to 80% HMX, with either nitroglycerin or triethyleneglycol dinitrate as colloiding agent for nitrocellulose, have also been prepared. In general these compositions showed lower heat stability than that of conventional high explosive compositions.

Reference: 84

(a) U. S. Air Intelligence Information Report IR-269-55, <u>Holtex--Hispano Suiza Explosive</u>,
 4 May 1955.

⁸⁴See footnote 1, page 10.

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| 10 Experimental Statistics, Section 1, Basic Con- control of Proximity, Electrical, Part Twe (U) 111 Experimental Statistics, Section 2, Analysis of Experimental Statistics, Section 2, Analysis of Experimental Statistics, Section 5, Planning and Analysis of Comparative Experiments and Analysis of Comparative Experiments end Analysis of Comparative Experiments and Analysis of Comparative Experiments end Index for Control of Mobile end Index for Series end Index for Seri | 109 | | | |
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