Total Maximum Daily Load of Sediment in the Lower Monocacy River Watershed, Frederick, Carroll, and Montgomery Counties, Maryland

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List of Abbreviations

BIBI	Benthic Index of Biotic Integrity
BIP	Buffer Incentive Program
BMP	Best Management Practices
CBP P5	Chesapeake Bay Program Phase 5
CV	Coefficient of Variation
CWA	Clean Water Act
DNR	Maryland Department of Natural Resources
EOF	Edge-of-Field
EOS	Edge-of-Stream
EPA	Environmental Protection Agency
EPSC	Environmental Permit Service Center
EPT	Ephemeroptera, Plecoptera, and Trichoptera
ETM	Enhanced Thematic Mapper
FIBI	Fish Index of Biologic Integrity
GIS	Geographic Information System
IBI	Index of Biotic Integrity
Ind	Indeterminate
LA	Load Allocation
MACS	Maryland Agriculture water quality cost share program
MBSS	Maryland Biological Stream Survey
MD 8-digit	Maryland 8-digit Watershed
MDE	Maryland Department of the Environment
MDL	Maximum Daily Load
MGD	Millions of Gallons per Day
mg/l	Milligrams per liter
MOS	Margin of Safety
MS4	Municipal Separate Storm Sewer System
N/A	Not Applicable
NPDES	National Pollutant Discharge Elimination System
NRCS	Natural Resource Conservation Service

NRI	Natural Resources Inventory
NS	No Sample
PSU	Primary Sampling Unit
RESAC	Regional Earth Science Applications Center
SSDI	Sediment Stream Disturbance Index
TMDL	Total Maximum Daily Load
Ton/yr	Tons per Year
TSD	Technical Support Document
TSS	Total Suspended Solids
TM	Thematic Mapper
USGS	United Stated Geological Survey
WLA	Waste Load Allocation
WTP	Water Treatment Plant
WQIA	Water Quality Improvement Act
WQLS	Water Quality Limited Segment
WWTP	Wastewater Treatment Plant

EXECUTIVE SUMMARY

This document, upon approval by the U.S. Environmental Protection Agency (EPA), establishes a Total Maximum Daily Load (TMDL) for sediment in the Lower Monocacy River watershed (basin number 02140302). Section 303(d) of the federal Clean Water Act (CWA) and the EPA's implementing regulations direct each state to identify and list waters, known as water quality limited segments (WQLSs), in which current required controls of a specified substance are inadequate to achieve water quality standards. For each WQLS, the State is required to either establish a TMDL of the specified substance that the waterbody can receive without violating water quality standards, or demonstrate that water quality standards are being met (CFR 2007b).

The Maryland Department of the Environment (MDE) has identified the waters of the Lower Monocacy River on the State's 303(d) List as impaired by sediments (1996, Lake Linganore – 1996), nutrients (1996, Lake Linganore – 1996), bacteria (2002), and impacts to biological communities (2002, 2004, and 2006)(MDE 2007a). The Lower Monocacy River, upstream of US Route 40, and its tributary Israel Creek are designated as Use IV-P waterbodies (Recreational Trout Waters and Public Water Supply); Downstream of US Route 40, the Lower Monocacy River is designated as a Use I-P waterbody (Water Contact Recreation, protection of Aquatic Life, and Public Water Supply). Additional tributaries of the Lower Monocacy River – Ballenger Creek, Bear Branch, Carroll Creek, Furnace Branch, Little Bennett Creek, and Rocky Fountain Run – are designated as Use III-P waterbodies (Non-tidal Cold Water and Public Water Supply) (COMAR 2007 a,b,c,d). The Lake Linganore watershed is designated as Use IV-P.

A data solicitation for sediments was conducted by MDE, and all readily available data from the past five years have been considered. A TMDL for fecal coliform to address the 2002 bacteria listing was submitted to the EPA in 2007. A TMDL of sediments and phosphorus for the Lake Linganore impoundment was approved by the EPA in 2003. The remaining listings for nutrients and impacts to biological communities will be addressed separately at a future date.

In order to maintain consistency with the 2003 Lake Linganore sediment TMDL and to ensure that the 2003 Lake Linganore sediment TMDL is protective of the tributary streams draining to the impoundment, the Lake Linganore watershed was analyzed separately from the rest of the Lower Monocacy River watershed using MDE's non-tidal sediment TMDL methodology (Currey et al. 2006). The results of this analysis (see Appendix E) indicate that the 2003 Lake Linganore sediment TMDL is more protective of the tributary streams draining to the impoundment than the alternative Lake Linganore sediment TMDL estimated using the non-tidal sediment TMDL methodology. The 2003 Lake Linganore sediment TMDL is not only preserving the impoundment's capacity (the water quality endpoint used to develop the 2003 sediment TMDL in the absence of a TSS criterion for impoundments), but it is also protective of the aquatic health within the tributary streams draining to the impoundment. Therefore, the 2003 Lake Linganore sediment TMDL has been applied in the Lower Monocacy River TMDL analysis and has been presented as an upstream load.

The assessment unit of this TMDL will be defined as the Lower Monocacy River watershed, excluding the Lake Linganore watershed, and the remainder of the document will evaluate only this portion of the watershed. However, for the sake of simplicity, the assessment unit will still be referred to as the Lower Monocacy River watershed.

The Lower Monocacy River watershed aquatic health scores, consisting of the Benthic Index of Biotic Integrity (BIBI) and Fish Index of Biotic Integrity (FIBI), indicate that the biological metrics for the watershed exhibit a significant negative deviation from reference conditions (Roth et al. 2005). The objective of the TMDL established herein, is to ensure that there will be no sediment impacts affecting aquatic health, thereby establishing a sediment load that supports the Use I-P/IV-P/III-P designation for the Lower Monocacy River watershed.

Currently in Maryland, there are no specific numeric criteria that quantify the impact of sediment on the aquatic health of non-tidal stream systems. To determine whether aquatic health is impacted by elevated sediment loads, a weight-of-evidence stressor identification approach was used. This approach applies a composite stressor indicator, defined as the *sediment stream disturbance index* (SSDI). Similar to the Index of Biotic Integrity (IBI), the SSDI is based on a comparison of specific watershed parameters with those from streams with a healthy aquatic community (i.e., reference watersheds) and is scored separately for the benthic and fish communities. Watershed specific SSDI values indicate whether sediment is one of the stressors affecting the biological community.

In order to quantify the impact of sediment on the aquatic health of non-tidal stream systems, a reference watershed TMDL approach was used and resulted in the establishment of a *sediment loading threshold* (Currey et al. 2006). This threshold is based on a detailed analysis of sediment loads from watersheds that are identified as supporting aquatic life (i.e., reference watersheds) based on Maryland's biocriteria (Roth et al. 1998, 2000; Stribling et al. 1998). This threshold is then used to determine a watershed specific sediment TMDL.

The computational framework chosen for the Lower Monocacy River watershed TMDL was the Chesapeake Bay Program Phase 5 (CBP P5) watershed model target *edge-of-field* (EOF) land use sediment loading rate calculations combined with a *sediment delivery ratio*. The *edge-of-stream* (EOS) sediment load is calculated per land use as a product of the land use area, land use target loading rate, and loss from the EOF to the main channel. The spatial domain of the CBP P5 watershed model segmentation aggregates to the Maryland 8-digit (MD 8-digit) watersheds, which is consistent with the impairment listing.

EPA's regulations require TMDLs to take into account seasonality and critical conditions for stream flow, loading, and water quality parameters (CFR 2007b). The intent of this requirement is to ensure that the water quality of the waterbody is protected during times when it is most vulnerable. The biological monitoring data used to determine the reference watersheds integrates the stress effects over the course of time and thus inherently addresses critical conditions. Seasonality is captured in two components.

First, it is implicitly included through the use of the biological monitoring data. Second, the Maryland Biological Stream Survey (MBSS) dataset included benthic sampling in the spring and fish sampling in the summer.

All TMDLs need to be presented as a sum of waste load allocations (WLAs) for point sources and load allocations (LAs) for nonpoint sources generated within the assessment unit, natural background, tributary, and adjacent segment loads. Furthermore, all TMDLs must include a margin of safety (MOS) to account for any lack of knowledge and uncertainty concerning the relationship between loads and water quality (CFR 2007a,b). It is proposed that the estimated variability around the reference watershed group used in this analysis already accounts for such uncertainty. This results in an implicit margin of safety of approximately 8%.

The Lower Monocacy River Total Baseline Sediment Load is 146,420.0 tons per year (ton/yr). This baseline load consists of upstream loads generated outside the assessment unit: an Upper Monocacy River Upstream Baseline Load (BL_{UM}) of 98,725.7 ton/yr and a Lake Linganore Upstream Baseline Load (BL_{LL}) of 11,585.0; and loads generated within the assessment unit: a Lower Monocacy River Watershed Baseline Load Contribution of 36,109.3 ton/yr. The Lower Monocacy River Watershed Baseline Load Contribution is further subdivided into nonpoint source baseline loads (Nonpoint Source BL_{LM}) and two types of point source baseline loads: National Pollutant Discharge Elimination System (NPDES) regulated stormwater (NPDES Stormwater BL_{LM}) and regulated process water (Process Water BL_{LM}) (see Table ES-1). Appendix D provides a detailed explanation of the upstream loads.

Table ES-1: Lower Monocacy River Baseline Sediment Loads (ton/yr)

		Upstream Baseline Load[1]				Lower Monocacy River Watershed Baseline Load Contribution				
Total Baseline Load (ton/yr)	=	**BL_{LL}[2]**	+	**BL_{UM}[3]**	+	**Nonpoint Source BL_{LM}**	+	**NPDES Stormwater BL_{LM}**	+	**Process Water BL_{LM}**
146,420.0	=	11,585.0	+	98,725.7	+	27,073.4	+	8,312.5	+	723.4

Notes: [1] Although the upstream values are reported as a single value, they include point and nonpoint sources.
[2] For the Lake Linganore watershed point and nonpoint source characterization, please refer to the "Total Maximum Daily Load of Phosphorus and Sediments for Lake Linganore, Frederick County, Maryland" (MDE 2003).
[3] For the Upper Monocacy River watershed point and nonpoint source characterization, please refer to the "Total Maximum Daily Load of Sediment in the Upper Monocacy River Watershed, Frederick and Carroll Counties, Maryland" (MDE 2008a).

The Lower Monocacy River Average Annual TMDL of Sediment/Total Suspended Solids (TSS) is 90,158.0 ton/yr. The TMDL consists of allocations attributed to loads generated outside the assessment unit referred to as Upstream Load Allocations: an Upper Monocacy River Upstream Load Allocation (LA_{UM}) of 66,707.3 ton/yr and a Lake Linganore Upstream Load Allocation (LA_{LL}) of 7,073.0; and loads generated within the assessment unit: a Lower Monocacy River Watershed TMDL Contribution of 16,377.7

ton/yr. The Lower Monocacy River Watershed TMDL Contribution is further subdivided into point and nonpoint source allocations and is comprised of a Load Allocation (LA_{LM}) of 12,397.5 ton/yr, an NPDES Stormwater Waste Load Allocation (NPDES Stormwater WLA_{LM}) of 3,256.8 tons/yr, and a Process Water Waste Load Allocation (Process Water WLA_{LM}) of 723.4 ton/yr (see Table ES-2). This TMDL will ensure that the sediment loads and resulting effects are at a level to support the Use I-P/IV-P/III-P designation for the Lower Monocacy River watershed, and more specifically, at a level to support aquatic health.

Table ES-2: Average Annual Lower Monocacy River TMDL of Sediment/TSS (ton/yr)

TMDL (ton/yr)	=	**LA**					+	**WLA**			+	**MOS**
		LA_{LL}[1]	+	**LA_{UM}**[2]	+	**LA_{LM}**		**NPDES Stormwater WLA_{LM}**	+	**Process Water WLA_{LM}**		
90,158.0	=	7,073.0	+	66,707.3	+	12,397.5	+	3,256.8	+	723.4	+	Implicit
		Upstream Load Allocations[3,4]				Lower Monocacy River Watershed TMDL Contribution						

Notes:[1] For Lake Linganore watershed WLA and LA characterization, please refer to the "Total Maximum Daily Loads of Phosphorus and Sediments for Lake Linganore, Frederick County, MD" (MDE 2003).
[2] For Upper Monocacy River watershed WLA and LA characterization, please refer to the "Total Maximum Daily Load of Sediment in the Upper Monocacy River Watershed, Frederick and Carroll Counties, Maryland" (MDE 2008a).
[3] Although for the purpose of this analysis the upstream load is referred to as an LA, it could include loads from point and nonpoint sources.
[4] A delivery factor of 1 was used for all of the Upstream Load Allocations.

Table ES-3: Lower Monocacy River Baseline Load, TMDL, and Total Reduction Percentage

Baseline Load (ton/yr)	**TMDL (ton/yr)**	**Total Reduction (%)**
146,420.0	90,158.0	38.4

In addition to the TMDL value, a Maximum Daily Load (MDL) is also presented in this document. The calculation of the MDL, which is derived from the TMDL average annual loads is explained in Appendix C and presented in Table C-1.

Once the EPA has approved this TMDL, and it is known what measures must be taken to reduce pollution levels, implementation of best management practices (BMPs) is expected to take place. MDE intends for the required reduction to be implemented in an iterative process that first addresses those sources with the largest impact to water quality, with consideration given to ease and cost of implementation.

Maryland has several well-established programs to draw upon, including the Water Quality Improvement Act of 1998 (WQIA) and the Federal Nonpoint Source Management Program (§ 319 of the Clean Water Act). Several potential funding sources for implementation are available, such as the Buffer Incentive Program (BIP), the State Water Quality Revolving Loan Fund, and the Stormwater Pollution Cost Share Program.

1.0 INTRODUCTION

This document, upon approval by the U.S. Environmental Protection Agency (EPA), establishes a Total Maximum Daily Load (TMDL) for sediment in the Lower Monocacy River watershed (basin number 02140302). Section 303(d)(1)(C) of the federal Clean Water Act (CWA) and the EPA's implementing regulations direct each state to develop a TMDL for each impaired water quality limited segment (WQLS) on the Section 303(d) List, taking into account seasonal variations, critical conditions, and a protective margin of safety (MOS) to account for uncertainty (CFR 2007b). A TMDL reflects the total pollutant loading of the impairing substance a waterbody can receive and still meet water quality standards.

TMDLs are established to determine the pollutant load reductions needed to achieve and maintain water quality standards. A water quality standard is the combination of a designated use for a particular body of water and the water quality criteria designed to protect that use. Designated uses include activities such as swimming, drinking water supply, protection of aquatic life, and shellfish propagation and harvest. Water quality criteria consist of narrative statements and numeric values designed to protect the designated uses. Criteria may differ among waters with different designated uses.

The Maryland Department of the Environment (MDE) has identified the waters of the Lower Monocacy River on the State's 303(d) List as impaired by sediments (1996, Lake Linganore – 1996), nutrients (1996, Lake Linganore – 1996), bacteria (2002), and impacts to biological communities (2002, 2004, 2006)(MDE 2007a). The Lower Monocacy River, upstream of US Route 40, and its tributary Israel Creek are designated as Use IV-P waterbodies (Recreational Trout Waters and Public Water Supply); Downstream of US Route 40, the Lower Monocacy River is designated as a Use I-P waterbody (Water Contact Recreation, protection of Aquatic Life, and Public Water Supply). Additional tributaries of the Lower Monocacy River–Ballenger Creek, Bear Branch, Carroll Creek, Furnace Branch, Little Bennett Creek, and Rocky Fountain Run – are designated as Use III-P waterbodies (Non-tidal Cold Water and Public Water Supply) (COMAR 2007a,b,c,d). The Lake Linganore watershed is designated as Use IV-P.

A data solicitation for sediments was conducted by MDE, and all readily available data from the past five years have been considered. A TMDL for fecal coliform to address the 2002 bacteria listing was submitted to the EPA in 2007. A TMDL of sediments and phosphorus for the Lake Linganore impoundment was approved by the EPA in 2003. The listings for nutrients and impacts to biological communities will be addressed separately at a future date.

In order to maintain consistency with the 2003 Lake Linganore sediment TMDL and to ensure that the 2003 Lake Linganore sediment TMDL is protective of the tributary streams draining to the impoundment, the Lake Linganore watershed was analyzed separately from the rest of the Lower Monocacy River watershed using MDE's non-tidal sediment TMDL methodology (Currey et al. 2006). The results of this analysis (see Appendix E) indicate that the 2003 Lake Linganore sediment TMDL is more protective of the tributary streams draining to the impoundment than the alternative Lake Linganore sediment TMDL estimated using the non-tidal sediment TMDL methodology. The 2003 Lake Linganore sediment TMDL is not only preserving the impoundment's capacity (the water quality endpoint used to develop the 2003 sediment TMDL in the absence of a TSS criterion for impoundments), but it is also protective of the aquatic health within the tributary streams draining to the impoundment. Therefore, the 2003 Lake Linganore sediment TMDL has been applied in the Lower Monocacy River TMDL analysis and has been presented as an upstream load.

The assessment unit of this TMDL will be defined as the Lower Monocacy River watershed, excluding the Lake Linganore watershed, and the remainder of the document will evaluate only this portion of the watershed. However, for the sake of simplicity, the assessment unit will still be referred to as the Lower Monocacy River watershed.

The objective of the TMDL established herein is to ensure that there will be no sediment impacts affecting aquatic health, thereby establishing a sediment load that supports the Use I-P/IV-P/III-P designation for the Lower Monocacy River watershed. Currently in Maryland, there are no specific numeric criteria that quantify the impact of sediment on the aquatic health of non-tidal stream systems. To determine whether aquatic health is impacted by elevated sediment loads, a weight-of-evidence stressor identification approach was used. This approach applies a composite stressor indicator, defined as the *sediment stream disturbance index* (SSDI). Similar to the Index of Biotic Integrity (IBI), the SSDI is based on a comparison of specific watershed parameters with those from streams with a healthy aquatic community (i.e., reference watersheds) and is scored separately for the benthic and fish communities. Watershed specific SSDI values indicate whether sediment is one of the stressors affecting the biological community.

In order to quantify the impact of sediment on the aquatic health of non-tidal stream systems, a reference watershed TMDL approach was used and resulted in the establishment of a *sediment loading threshold* (Currey et al. 2006). This threshold is based on a detailed analysis of sediment loads from watersheds that are identified as supporting aquatic life (i.e., reference watersheds) based on Maryland's biocriteria (Roth et al. 1998, 2000; Stribling et al. 1998). This threshold is then used to determine a watershed specific sediment TMDL.

2.0 SETTING AND WATER QUALITY DESCRIPTION

2.1 General Setting

Location

The Monocacy River is a free flowing stream that originates in Pennsylvania and flows 58 miles within Maryland where it finally empties into the Potomac River. The watershed covers approximately 966 square miles, with approximately 224 square miles located in Pennsylvania and 742 square miles in Maryland. The basin can be subdivided into three distinct watersheds: the Upper Monocacy River, Lower Monocacy River, and Double Pipe Creek.

The assessment unit for this TMDL, referred to here as the Lower Monocacy River watershed, excludes the Lake Linganore watershed. Both the Upper Monocacy River watershed and the Lake Linganore watershed drain into the Lower Monocacy River watershed, and consequently the sediment loads from both watersheds will be treated as upstream loads within this analysis.

The Lower Monocacy River watershed is situated primarily in Frederick County but includes a small portion of Montgomery County as well. The watershed covers 215 square miles and is characterized by a moderately steep to flat terrain. Approximately 5% of the total watershed is covered by water (i.e. streams, ponds, etc.). There is a significant amount of agriculture within the watershed, which consists mostly of row crops, but also includes dairy production. The largest urban center within the watershed is the City of Frederick, and the total population within the watershed is estimated to be approximately 96,000 (MDE 2007b).

Upstream Loads

Lake Linganore

The Lake Linganore impoundment is located along Linganore Creek, a tributary of the Lower Monocacy River, in the northeastern portion of the watershed. A separate TMDL for sediments has already been approved for Lake Linganore and the load established therein is incorporated as an upstream load in this TMDL (MDE 2003). Additionally, the Lake Linganore watershed was analyzed using the non-tidal sediment TMDL methodology. The results of this analysis (see Appendix E) indicated that the 2003 Lake Linganore sediment TMDL is more protective of the tributary streams draining to the impoundment than the alternative Lake Linganore sediment TMDL that was estimated using the non-tidal sediment TMDL methodology. Therefore, the 2003 Lake Linganore sediment TMDL has been applied in the Lower Monocacy River TMDL analysis and has been presented as an upstream load.

Upper Monocacy

The Upper Monocacy River watershed is located in Frederick and Carroll Counties, Maryland and empties into the Lower Monocacy River watershed to the northeast of the city of Frederick. A separate TMDL for sediments in the Upper Monocacy River watershed is currently under development and is also included in this TMDL as an upstream load (MDE 2008a).

The hydrological relationship between the three Maryland 8-digit watersheds (MD 8-digit) within the Monocacy system and the subsequent effect on sediment loads are further explained in Appendix D.

Geology/Soils

The Lower Monocacy River watershed lies within the Western Division of the Piedmont geologic province of Maryland. The outstanding features of the Piedmont's Western Division are the Frederick Valley and the Triassic Upland. The broad, flat Frederick Valley is underlain by limestone as well as dolomite, and has an average elevation of 300 feet. The Triassic Upland borders much of the Frederick Valley. The low to moderate relief of the Triassic Upland is underlain by layered sandstone, siltstone, and red shale. The average elevation of the Upland is approximately 500 feet. A prominent topographic feature of the Piedmont is an erosion resistant monadnock, known as Sugarloaf Mountain, which is composed of highly weather resistant quartz (DNR 2007b; MGS 2007; MDE 2000).

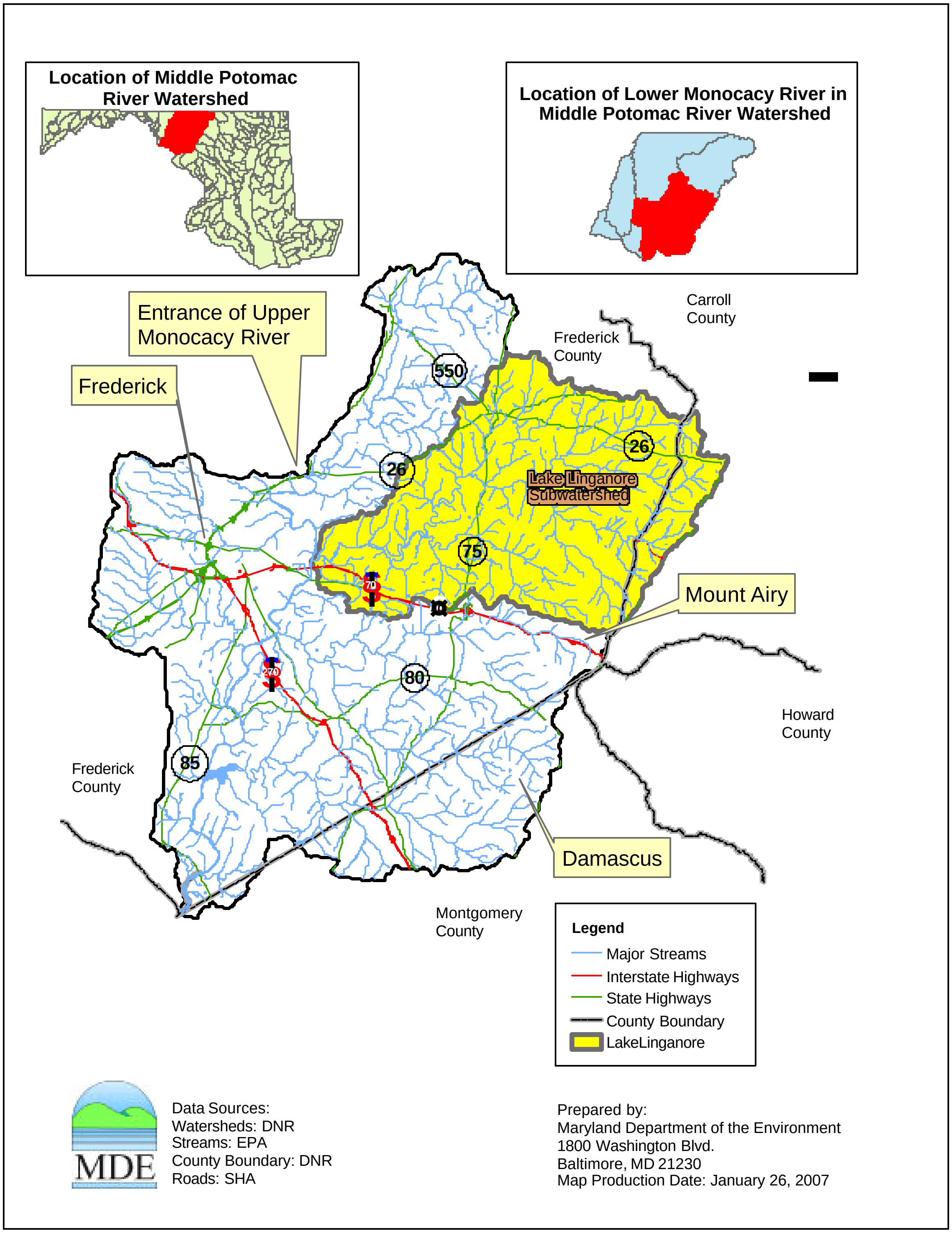

Figure 1: Location Map of the Lower Monocacy River Watershed

2.1.1. Land Use

Land Use Methodology

The land use framework used to develop this TMDL was originally developed for the Chesapeake Bay Program Phase 5 (CBP P5) watershed model.[1] The CBP P5 land use Geographic Information System (GIS) framework was based on two distinct layers of development. The first GIS layer was developed by the Regional Earth Science Applications Center (RESAC) at the University of Maryland and was based on satellite imagery [Landsat 7-Enhanced Thematic Mapper (ETM) and Landsat 5-Thematic Mapper (TM)] (Goetz et al. 2004). This layer did not provide the required level of accuracy that is especially important when developing agricultural land uses. In order to develop accurate agricultural land use calculations, the CBP P5 used county level U.S. Agricultural Census data as a second layer (USDA 1982, 1987, 1992, 1997, 2002).

Given that land cover classifications based on satellite imagery are likely to be least accurate at edges (i.e., boundaries between covers), the RESAC land uses bordering agricultural areas were analyzed separately. If the agricultural census data accounted for more agricultural use than the RESAC's data, appropriate acres were added to agricultural land uses from non-agricultural land uses. Similarly, if census agricultural land estimates were smaller than RESAC's, appropriate acres were added to non-agricultural land uses.

Adjustments were also made to the RESAC land cover to determine developed land uses. RESAC land cover was originally based on the United States Geological Survey (USGS) protocols used to develop the 2000 National Land Cover Database. The only difference between the RESAC and USGS approaches was RESAC's use of town boundaries and road densities to determine urban land covered by trees or grasses. This approach greatly improved the accuracy of the identified urban land uses, but led to the misclassification of some land adjacent to roads and highways as developed land. This was corrected by subsequent analysis. To ensure that the model accurately represented development over the simulation period, post-processing techniques that reflected changes in urban land use have been applied.

The result of this approach is that CBP P5 land use does not exist in a single GIS coverage; instead it is only available in a tabular format. The CBP P5 watershed model is comprised of 25 land uses. Most of these land uses are differentiated only by their nitrogen and phosphorus loading rates. The land uses are divided into 14 classes with distinct sediment erosion rates. Table 1 lists the CBP P5 generalized land uses, detailed land uses, which are classified by their erosion rates, and the acres of each land use in the Lower Monocacy River watershed. Details of the land use development methodology have been summarized in the report entitled "Chesapeake Bay Phase 5 Community Watershed Model: Tracking Nutrient and Sediment Loads on a Regional and Local Scale" (US EPA 2007).

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[1] The EPA Chesapeake Bay Program developed the first watershed model in 1982. There have been many upgrades since the first phase of this model. The CBP P5 was developed to estimate flow, nutrient, and sediment loads to the Bay.

Lower Monocacy River Watershed Land Use Distribution

The land use distribution in the Lower Monocacy River watershed consists of nearly equal amounts of crop (26%), forest (31%), and urban (32%) land uses. There is also a small amount of pasture (11%) and extractive (0.1%) land use. A land use map is provided in Figure 2 and a summary of the watershed land use areas is presented in Table 1.

Table 1: Land Use Percentage Distribution for the Lower Monocacy River Watershed

General Land Use	Detailed Land Use	Area (Acres)	Percent	Grouped Percent of Total
Crop	Animal Feeding Operations	59.8	N/A[1]	
	Hay	12,951.4	9.8	
	High Till	9,286.2	7.0	
	Low Till	11,096.4	8.4	
	Nursery	607.2	0.5	25.8
Extractive	Extractive	160.7	0.1	0.1
Forest	Forest	40,577.9	30.8	
	Harvested Forest	409.9	0.3	31.1
Pasture	Natural Grass	3,252.7	2.5	
	Pasture	11,574.7	8.8	
	Trampled Pasture	60.6	N/A[1]	11.3
Urban	Urban: Barren	594.0	0.5	
	Urban: Imp	7,853.0	6.0	
	Urban: perv	33,376.7	25.3	31.7
Total		131,861.3	100.0	100.0

Note: [1] Percentage of total land area is minimal.

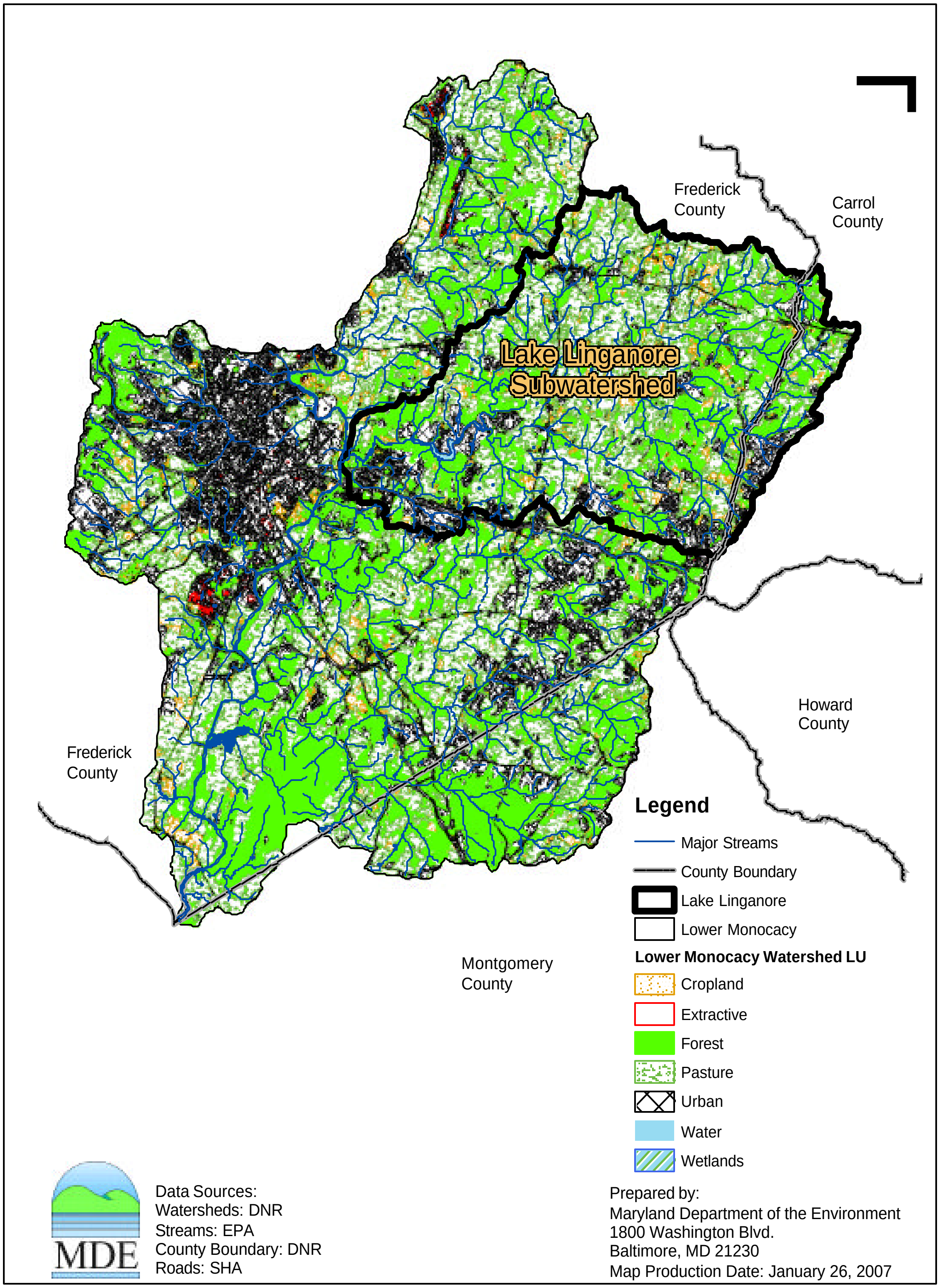


Figure 2: Land Use of the Lower Monocacy River Watershed

2.2 Source Assessment

The Lower Monocacy River Total Baseline Sediment Load consists of loads generated outside the 8-digit assessment unit, referred to as Upstream Baseline Loads, and loads generated within the assessment unit, referred to as the Lower Monocacy River Watershed Baseline Load Contribution. The Lower Monocacy River Watershed Baseline Load Contribution is further subdivided into nonpoint and point source loads. This section summarizes the methods used to derive each of these distinct source categories.

2.2.1 Nonpoint Source Assessment

In this document, the nonpoint source loads account for sediment loads from unregulated storm water runoff within the Lower Monocacy River watershed. This section provides the background and methods used to characterize the nonpoint source baseline loads generated within the Lower Monocacy River watershed (Nonpoint Source BL_{LM}).

General Load Estimation Methodology

Nonpoint source sediment loads generated within the Lower Monocacy River watershed are estimated based on the *edge-of-stream (EOS)* calibration target loading rates from the CBP P5 model. This approach is based on the fact that not all of the *edge-of-field* (EOF) sediment load is delivered to the stream or river (some of it is stored on fields down slope, at the foot of hillsides, or in smaller rivers or streams that are not represented in the model). To calculate the actual EOS loads, a *sediment delivery ratio* (the ratio of sediment reaching a basin outlet compared to the total erosion within the basin) is used. Details of the methods used to calculate sediment load have been summarized in the report entitled "Chesapeake Bay Phase 5 Community Watershed Model: Tracking Nutrient and Sediment Loads on a Regional and Local Scale" (US EPA 2007).

Edge-of-Field Target Erosion Rate Methodology

EOF target erosion rates for agricultural land uses and forested land use were based on erosion rates determined by the Natural Resource Inventory (NRI). NRI is a statistical survey of land use and natural resource conditions conducted by the Natural Resources Conservation Service (NRCS) (USDA 2007). Sampling methodology is explained by Nusser and Goebel (1997).

Estimates of average annual erosion rates for pasture and cropland are available on a county basis at five-year intervals, starting in 1982. Erosion rates for forested land uses are not available on a county basis from NRI; however, for the purpose of the CBP Phase 2 watershed model, NRI calculated average annual erosion rates for forested land use on a watershed basis. These rates are still being used as targets in the CBP P5 model.

The average value of the 1982 and 1987 surveys was used as the basis for EOF target loads. The erosion rates from this period do not reflect best management practices (BMPs) or other soil conservation policies introduced in the wake of the effort to restore the Chesapeake Bay. To compensate for this, a BMP factor was included in the loading estimates using best available "draft" information from the CBP. However, the effect of these factors was minimal, as most of the anticipated reductions are expected to result from land use changes (e.g. high till to low till). Rates for urban pervious, urban impervious, and barren land were based on a combination of best professional judgment, literature analysis, and regression analysis. Table 2 lists erosion rates specific to the Lower Monocacy River watershed.

Table 2: Summary of EOF Erosion Rate Calculations

Land Use	Data Source	Frederick County (tons/acre/year)	Montgomery County (tons/acre/year)
Forest	Phase 2 NRI	0.21	0.36
Harvested Forest[1]	Average Phase 2 NRI (x 10)	3	3
Natural Grass	Average NRI Pasture (1982-1987)	1.5	1.5
Pasture	Pasture NRI (1982-1987)	1.48	1.23
Trampled pasture[2]	Pasture NRI (x 9.5)	14.06	11.69
Animal Feeding Operations[2]	Pasture NRI (x 9.5)	14.06	11.69
Hay[2]	Crop NRI (1982-1987) (x 0.32)	2.46	2.8
High Till Without Manure[2]	Crop NRI (1982-1987) (x 1.25)	9.59	10.96
High Till With manure[2]	Crop NRI (1982-1987) (x 1.25)	9.59	10.96
Low till With Manure[2]	Crop NRI (1982-1987) (x 0.75)	5.76	6.57
Pervious Urban	Intercept Regression Analysis	0.74	0.74
Extractive	Best professional judgment	10	10
Barren	Literature survey	12.5	12.5
Impervious	100% Impervious Regression Analysis	5.18	5.18

Notes: [1] Based on an average of NRI values for the Chesapeake Bay Phase 5 segments.
[2] NRI score data adjusted based on land use.

Sediment Delivery Ratio: The base formula for calculating *sediment delivery ratio*s in the CBP P5 model is the same as the formula used by the NRCS (USDA 1983).

$$DF = 0.417762 * A^{-0.134958} - 0.127097 \qquad (2.1)$$

where
DF (delivery factor) = the sediment delivery ratio
A = drainage area in square miles

In order to account for the changes in sediment loads due to distance traveled to the stream, the CBP P5 model uses the *sediment delivery ratio*. Land use specific *sediment delivery ratios* were calculated for each river segment using the following procedure:

(1) mean distance of each land use from the river reach was calculated;

(2) *sediment delivery ratio*s for each land use were calculated (drainage area in Equation 2.1 was assumed to be equal to the area of a circle with radius equal to the mean distance between the land use and the river reach).

Edge-of-Stream Loads

Edge-of-stream loads are the loads that actually enter the river reaches (i.e., the mainstem of a watershed). Such loads represent not only the erosion from the land but all of the intervening processes of deposition on hillsides and sediment transport through smaller rivers and streams.

2.2.2 Point Source Assessment

A list of 73 active permitted point sources that contribute to the sediment load in the Lower Monocacy River watershed was compiled using MDE's Environmental Permit Service Center (EPSC) database. The types of permits identified include individual industrial, individual municipal, general mineral mining, general industrial stormwater, and general municipal separate storm sewer systems (MS4s). The permits can be grouped into two categories, process water and stormwater. The stormwater category includes all National Pollutant Discharge Elimination System (NPDES) regulated stormwater discharges. The process water category includes those loads generated by continuous discharge sources whose permits have total suspended solids (TSS) limits. Other permits that do not meet these conditions are considered *de minimis* in terms of the total sediment load.

The sediment loads for the 24 process water permits (Process Water BL_{LM}) are calculated based on their TSS limits and corresponding flow information. The 49 NPDES Phase I or Phase II stormwater permits identified throughout the Lower Monocacy River watershed are regulated based on BMPs and do not include TSS limits. In the absence of TSS limits, the NPDES regulated stormwater baseline load (NPDES Stormwater BL_{LM})

is calculated using methods described in Section 2.2.1 and watershed specific urban land use sediment delivery factors. A detailed list of the permits appears in Appendix B.

2.2.3 Upstream Loads Assessment

For the purpose of this analysis, two upstream watersheds have been identified: the Lake Linganore watershed and the Upper Monocacy River watershed. Subsequently, sediment baseline loads from these watersheds will be presented as a Lake Linganore Baseline Load (BL_{LL}) and an Upper Monocacy River Baseline Load (BL_{UM}). The BL_{LL} will be set equivalent to the total baseline sediment load identified in the Lake Linganore 2003 Sediment TMDL (MDE 2003). The BL_{UM} will be set equivalent to the total baseline sediment load identified in the TMDL analysis for the Upper Monocacy River watershed (MDE 2008a).

2.2.4 Summary of Baseline Loads

Table 3 summarizes the Lower Monocacy River Baseline Sediment Load, reported in tons per year (ton/yr) and presented in terms of Upstream Baseline Loads and Lower Monocacy River Watershed Baseline Load Contribution nonpoint and point source loadings.

Table 3: Lower Monocacy River Baseline Sediment Loads (ton/yr)

		Upstream Baseline Load[1]				Lower Monocacy River Watershed Baseline Load Contribution				
Total Baseline Load (ton/yr)	=	**BL_{LL}[2]**	+	**BL_{UM}[3]**	+	**Nonpoint Source BL_{LM}**	+	**NPDES Stormwater BL_{LM}**	+	**Process Water BL_{LM}**
146,420.0	=	11,585.0	+	98,725.7	+	27,073.4	+	8,312.5	+	723.4

Notes: [1] Although the upstream values are reported as a single value, they include point and nonpoint sources.
[2] For Lake Linganore watershed point and nonpoint source characterization, please refer to the "Total Maximum Daily Load of Phosphorus and Sediments for Lake Linganore, Frederick County, Maryland" (MDE 2003).
[3] For Upper Monocacy River watershed point and nonpoint source characterization, please refer to the "Total Maximum Daily Load of Sediment in the Upper Monocacy River Watershed, Frederick and Carroll Counties, Maryland" (MDE 2008a).

Table 4 presents a breakdown of baseline loads generated within the Lower Monocacy River watershed, detailing loads per land use. The majority of the sediment load is from crop land (59%). The next largest sediment sources are urban land (23%), pasture (11%), and forest (5%).

Table 4: Detailed Baseline Sediment Budget Loads Generated Within the Lower Monocacy River Watershed

General Land Use	Description	Load (ton/Yr)	Percent	Grouped Percent of Total
Crop	Animal Feeding Operations	101.4	0.3	
	Hay	3,544.8	9.8	
	High Till	9,934.0	27.5	
	Low Till	6,982.1	19.3	
	Nursery	844.7	2.3	59.3
Extractive	Extractive	261.6	0.7	0.7
Forest	Forest	1,478.3	4.1	
	Harvested Forest	137.4	0.4	4.5
Pasture	Natural Grass	742.7	2.1	
	Pasture	2,890.5	8.0	
	Trampled Pasture	155.9	0.4	10.5
Urban[1]	Urban: Barren	958.9	2.7	
	Urban: Imp	4,673.5	12.9	
	Urban: perv	2,680.1	7.4	23.0
N/A	Process Load	723.4	2.0	2.0
	Total[2]	36,109.3	100.0	100.0

Notes: [1] The Maryland urban land use load represents the permitted stormwater load.
[2] The Lower Monocacy River watershed receives loads from two direct upstream watersheds: Lake Linganore and the Upper Monocacy River watershed. These loads are presented in their respective TMDLs (MDE 2003 and 2008a).

2.3 Water Quality Characterization

The Lower Monocacy River watershed was originally listed on Maryland's 1996 303(d) List as impaired by elevated sediments from nonpoint sources, with supporting evidence cited in Maryland's 1996 305(b) report. The 1996 305(b) report did not directly state that elevated sediments were a concern, and it has been determined that the sediment listing was based on best professional judgment (MDE 2004; DNR 1996).

Currently in Maryland, there are no specific numeric criteria for suspended sediments. However, the Maryland 2004 303(d) report states that degraded stream water quality resulting in a sediment impairment is characterized by erosional impacts, depositional impacts, and decreased water clarity (MDE 2004). Therefore, the evaluation of suspended sediment loads will be based on how the sediment related impacts are influencing the designated use of supporting aquatic health, as defined by Maryland's biocriteria (Roth et al. 1998, 2000; Stribling et al. 1998).

Recently, MDE developed a stressor identification methodology entitled "Using MBSS Data to Identify Stressors for Streams that Fail Biocriteria in Maryland" (Southerland et al. 2007). This document proposes a conceptual model (see Figure 3) that establishes a link between sediment loads and aquatic health. Specifically, it identifies whether current sediment loads have a negative impact on a watershed's aquatic health based on the observed sediment impacts. This linkage between sediment loads, sediment impacts, and aquatic health is used to evaluate a sediment impairment.

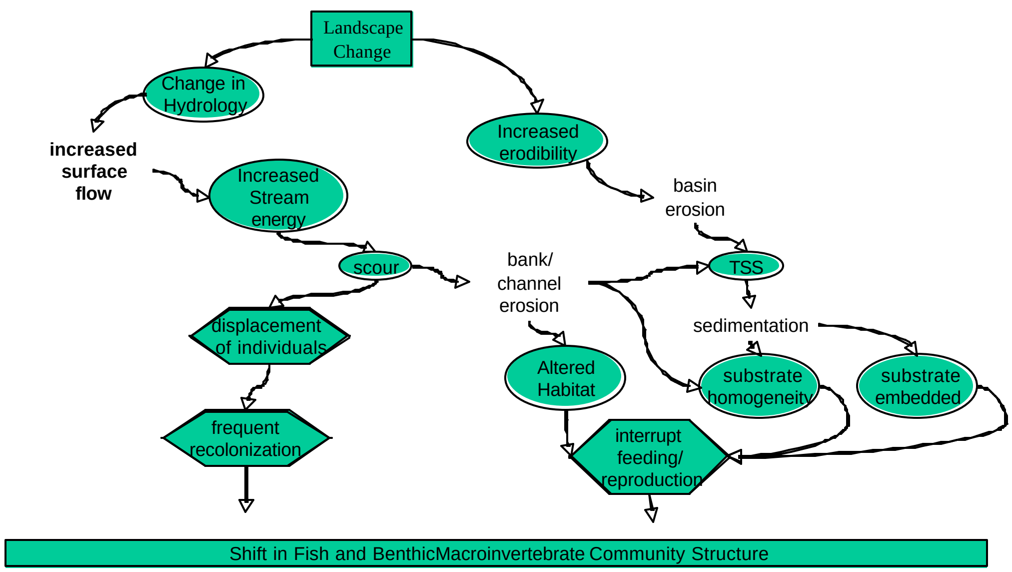


Figure 3: Sediment Stressor Conceptual Model

The sediment stressor conceptual model (adapted from Southerland et al. 2007) illustrates that changes in the landscape result in two possible paths, one triggered by changes in hydrology and the other triggered by increased land erodibility. Both paths ultimately result in changes in TSS and sediment loads, which, if increased, will result in a negative shift in the structure of the biological community.

Furthermore, the stressor conceptual model identifies water column TSS as the most direct measure of sediment loadings. Therefore, TSS was chosen as the most appropriate parameter for the sediment TMDL analysis. While an effective TSS concentration threshold would include both exposure duration and concentration magnitude, due to natural variations in geology, topography, and episodic flows, such a threshold would be extremely difficult to quantify (Rowe et al. 2003). In addition, the collection of sufficient instantaneous TSS concentration and flow data would be difficult due to high cost and limited site access during high flow events. Thus, MDE has not established a specific TSS water column concentration criteria. As a result, the water quality characterization of TSS impacts to aquatic life will be based on the cumulative impacts identified from observed streambed measures. Upon identification of sediment impacts, the TMDL will be estimated as a cumulative loading based on a comparison of the current watershed sediment loads with the acceptable levels derived from reference watersheds.

The streambed measures used to determine the water quality characterization were gathered from the Maryland Biological Stream Survey (MBSS) dataset. The MBSS uses a fixed length (75 m) randomly selected stream segment for collecting site level information within a primary sampling unit (PSU), also defined as a watershed. The randomly selected stream segments, from which field data are collected, are selected using either stratified random sampling with proportional allocation, or simple random sampling (Cochran 1977). This allocation ensures that all sites in a PSU stream network have the same probability of being selected. The random sample design allows for unbiased watershed estimates of mean conditions by averaging results at multiple stations. The average watershed estimates are then used to determine if streams within a watershed have a degraded biology (fish or benthic) and subsequently whether or not sediment is contributing to the observed degradation (Roth et al. 2005).

<u>Lower Monocacy River Watershed Monitoring Stations</u>

A total of 13 water quality monitoring stations were used to characterize the Lower Monocacy River watershed. There were 11 biological/physical habitat monitoring stations from the MBSS program and 2 biological monitoring stations from the Maryland Core/Trend monitoring network. The stations are presented in Figure 4 and listed in Table 5.

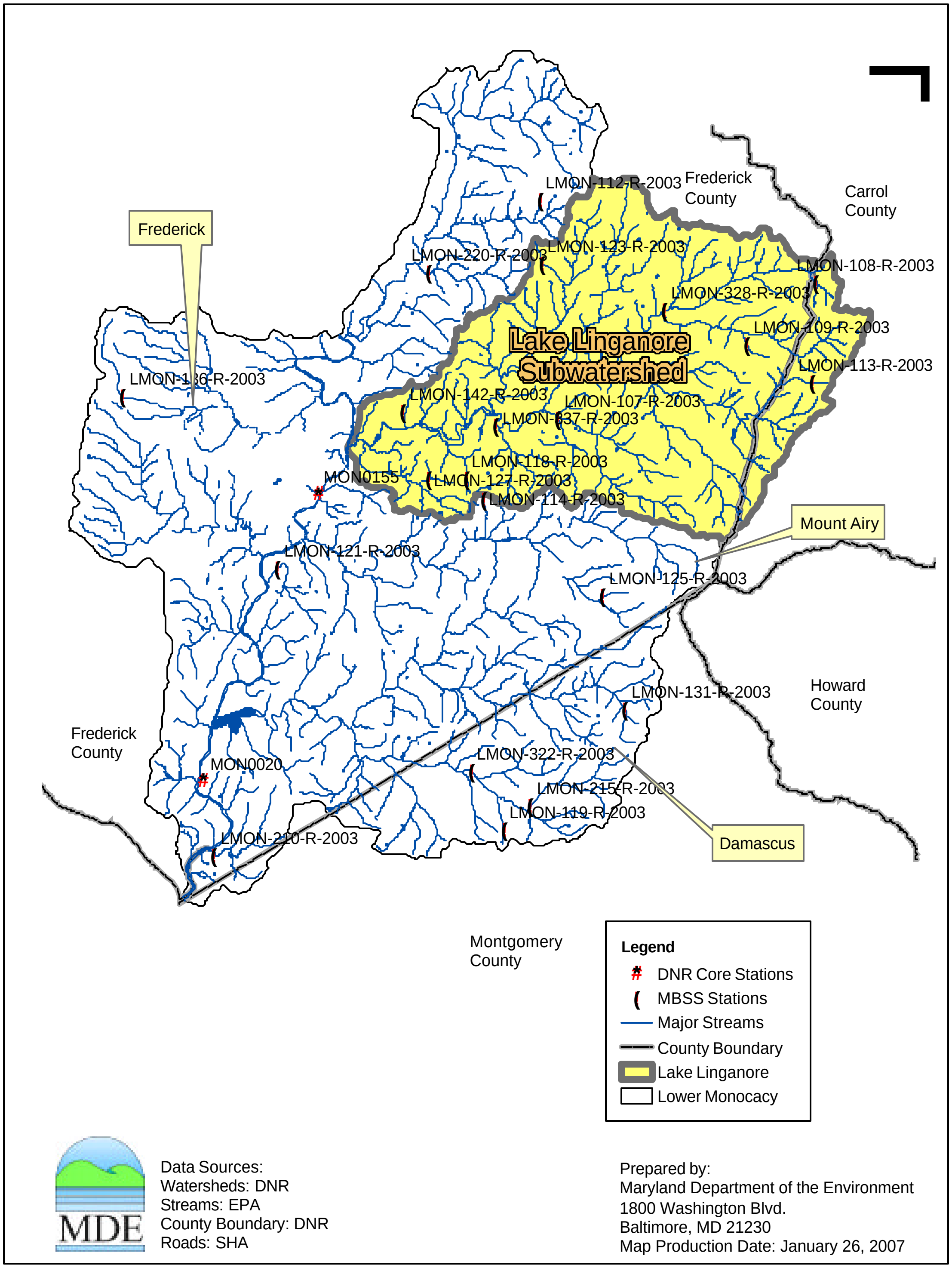


Figure 4: Monitoring Stations in the Lower Monocacy River Watershed

Table 5: Monitoring Stations in the Lower Monocacy River Watershed

Site Number	Sponsor	Site	Site Name	Latitude	Longitude
LMON-112-R-2003	MD DNR	MBSS	Cabbage Run, unnamed tributary 1	39.5075	-77.263
LMON-114-R-2003	MD DNR	MBSS	Bush Creek, unnamed tributary 2	39.3861	-77.293
LMON-119-R-2003	MD DNR	MBSS	Little Bennett Creek, unnamed tributary 1	39.2521	-77.281
LMON-121-R-2003	MD DNR	MBSS	Monocacy River, unnamed tributary 4	39.3575	-77.403
LMON-125-R-2003	MD DNR	MBSS	Church Branch of Bush Creek, unnamed tributary	39.347	-77.229
LMON-131-R-2003	MD DNR	MBSS	Bennett Creek	39.3011	-77.217
LMON-136-R-2003	MD DNR	MBSS	Rock Creek (MP)	39.4268	-77.486
LMON-210-R-2003	MD DNR	MBSS	Furnace Branch	39.2415	-77.436
LMON-215-R-2003	MD DNR	MBSS	Little Bennett Creek	39.262	-77.267
LMON-220-R-2003	MD DNR	MBSS	Israel Creek, unnamed tributary 1	39.4781	-77.322
LMON-322-R-2003	MD DNR	MBSS	Little Bennett Creek	39.2759	-77.299
MONO0020	MD DNR	CORE	Route 28	39.2717	-77.442
MONO0155	MD DNR	CORE	Reichs Ford Rd	39.3878	-77.381

Lower Monocacy River Watershed MBSS Monitoring Stations

The MBSS program monitored 11 locations in the Lower Monocacy River watershed in 2003 (see Figure 4). The MBSS parameters recommended from the stressor identification model for determining a sediment stressor were: percent embeddedness, epifaunal substrate score, instream habitat score, bank stability, and number of benthic tolerant species. These specific parameters were chosen based on their ecological and statistical significance (Southerland et al. 2007) as well as their linkage to increased terrestrial and/or instream erosion. High percent embeddedness indicates that fine particulates are filling the spaces between cobbles, thus covering habitat and limiting food supply. Low epifaunal substrate is an indication of either stream erosion or excess deposition limiting the quality of the streambed to support a benthic community. Decreased instream habitat is an indication of potential erosion removing woody debris and is primarily linked with the Fish Index of Biotic Integrity (FIBI). The bank stability index is a composite score that indicates the lack of channel erosion, based on the presence or absence of riparian vegetation and other stabilizing bank materials. The number of benthic tolerant species is an indicator of frequent stream scouring, which prevents more sensitive species from colonizing the streambed.

Observed values of the above parameters, along with Benthic Index of Biotic Integrity (BIBI) and FIBI scores, are presented in Table 6.

Table 6: Lower Monocacy River MBSS Data

Site	FIBI	BIBI	Epifaunal Substrate	Percent Embeddedness	Instream Habitat	Bank Stability	Benthic Tolerant Species
LMON-112-R-2003	1.33	2.5	11	40	10	13.8	4.79
LMON-114-R-2003	1.33	2.00	14	25	9	17.4	3.27
LMON-119-R-2003	1.00	3.00	12	40	14	18.53	5.47
LMON-121-R-2003	2.67	1.75	15	25	13	11.7	6.23
LMON-125-R-2003	3.67	2.75	12	40	13	17.6	4.35
LMON-131-R-2003	3.67	3.25	13	35	8	13.1	4.64
LMON-136-R-2003	2.00	1.5	12	25	10	20	4.09
LMON-210-R-2003	4.33	2.25	10	35	12	19	5.27
LMON-215-R-2003	3.67	2.75	17	20	17	15.6	4.27
LMON-220-R-2003	4.33	3.25	9	40	15	17.2	4.87
LMON-322-R-2003	4.33	3.25	16	20	16	11.7	4.92

Lower Monocacy River Core Stations

Additional data for the Lower Monocacy River was obtained from the Maryland Department of Natural Resources (DNR) Core/Trend program. The program collected benthic macroinvertebrate data between 1978 and 2006. This data was used to calculate four benthic community measures: total number of taxa, Shannon-Weiner diversity index, modified Hilsenhoff biotic index, and percent Ephemeroptera, Plecoptera, and Trichoptera (EPT). DNR has monitoring information for two stations in the mainstem of the Lower Monocacy River through the Core/Trend program. The stations are Route 28 (MONO0020) and Reichs Ford Road (MONO0155). The Route 28 station has 27 years of data between 1977 and 2006. The Reichs Ford Road station has 27 years of data between 1978 and 2006. Overall results for the stations appear in Table 7 (DNR 2007a).

Table 7: Lower Monocacy River DNR Core Data

Site Number	Current Water Quality Status	Trend Since 1970's
MONO0020	Good	Moderate improvement
MONO0155	Good	Strong improvement

2.4 Water Quality Impairment

The Maryland water quality standards surface water use designation for the Lower Monocacy River upstream of US Route 40, and its tributary Israel Creek is Use IV-P (Recreational Trout Waters and Public Water Supply); Downstream of US Route 40, the Lower Monocacy River is designated as a Use I-P waterbody (Water Contact Recreation, protection of Aquatic Life, and Public Water Supply). Additional tributaries of the Lower Monocacy River – Ballenger Creek, Bear Branch, Carroll Creek, Furnace Branch, Little Bennett Creek, and Rocky Fountain Run – are designated as Use III-P waterbodies (Non-tidal Cold Water and Public Water Supply) (COMAR 2007a,b,c,d).

To determine whether aquatic health is impacted by elevated sediment loads, a weight-of-evidence stressor identification approach was used. This approach applies a composite stressor indicator, defined as the *sediment stream disturbance index*. Similar to the Index of Biotic Integrity , the SSDI is based on a comparison of specific watershed parameters with those from streams with a healthy aquatic community (i.e., reference watersheds) and is scored separately for the benthic and fish communities. The benthic SSDI includes benthic tolerant species, embeddedness, bank stability, and epifaunal substrate condition. The fish SSDI includes embeddedness, epifaunal substrate, and instream habitat condition. Watershed specific SSDI values indicate whether sediment is one of the stressors affecting the biological community.

The SSDI is developed by scoring each parameter result (see Section 2.3) and then calculating the average of the scores to form an index value. Each parameter result is scored a value of 1, 3, or 5, depending on whether its original parameter value at a site approximates (5), deviates slightly from (3), or deviates greatly from (1) conditions at reference sites (Karr et al. 1986). This discrete scoring approach was based on Maryland's IBI methodology, so that a direct comparison could be made between the SSDI and the IBI thresholds. Per Maryland's biocriteria, FIBI and BIBI scores less than 3 are indicative of water quality conditions that are not protective of aquatic life (Roth et al. 1998, 2000; Stribling et al. 1998). Similarly, an SSDI score less than 3 provides evidence of a sediment stressor or sediment impact to the aquatic community. An SSDI score significantly greater than 3 indicates that there is no evidence of an adverse sediment impact to the aquatic community.

The threshold values for each selected parameter were established based on how they compared to the values observed at the reference sites (i.e., sites with FIBI & BIBI>3.0). For parameters expected to decrease with degradation, values below the 10th percentile were scored as 1. Values between the 10th and 50th percentiles were scored as 3. Values above the 50th percentile were scored as 5. Scoring was reversed for metrics expected to increase with degradation (i.e., values below the 50th percentile were scored as 5, and values above the 90th percentile were scored as 1). In this method, both the upper and lower thresholds are independently derived from the distribution of reference site values. This approach is based on the assumption that in Maryland, and most other states, even reference sites are expected to have some degree of anthropogenic impact (Southerland et al. 2005). Thresholds used for scoring the SSDI are summarized in Table 8.

Table 8: Sediment Stream Disturbance Index Scoring

Parameter	Score		
	1	3	5
Benthic Tolerant Species Limits	x ≥ 5.3	5.3 > x ≥ 4.2	x <4.2
Bank Stability	x < 12	12 = x < 19	x ≥ 19
Embeddedness Limits	x > 40	40 ≥ x > 25	x = 25
Epifaunal Substrate Limits	x < 10	10 = x < 15	x ≥ 15
Instream Habitat Condition Limits	x < 10	10 = x < 16	x ≥ 16

The Lower Monocacy River watershed average BIBIs, FIBIs, and corresponding SSDIs are listed in Table 9. The BIBIs and FIBIs indicate that the watershed is exhibiting a negative deviation from reference conditions. Both the benthic and fish based SSDIs indicate that sediment is a stressor to the aquatic community. Therefore, it is concluded that a sediment TMDL is required.

Table 9: Lower Monocacy River IBI and SSDI Values

Site	BIBI	Benthic SSDI	FIBI	Fish SSDI
LMON-112-R-2003	2.50	3.00	1.33	3.00
LMON-114-R-2003	2.00	4.00	1.33	3.00
LMON-119-R-2003	3.00	3.00	1.00	3.00
LMON-121-R-2003	1.75	2.50	2.67	3.67
LMON-125-R-2003	2.75	3.00	3.67	3.00
LMON-131-R-2003	3.25	3.00	3.67	2.33
LMON-136-R-2003	1.50	4.50	2.00	3.67
LMON-210-R-2003	2.25	3.00	4.33	3.00
LMON-215-R-2003	2.75	4.00	3.67	5.00
LMON-220-R-2003	3.25	2.50	4.33	2.33
LMON-322-R-2003	3.25	3.50	4.33	5.00
Average	**2.57 ± 0.31**	**3.27 ± 0.32**	**2.94 ± 0.65**	**3.36 ± 0.45**

3.0 TARGETED WATER QUALITY GOAL

The objective of the sediment TMDL established herein is to reduce sediment loads, and subsequent effects on aquatic health, in the Lower Monocacy River watershed to levels that support the Use I-P/IV-P/III-P designations (Water Contact Recreation, Protection of Aquatic Life, and Public Water Supply/Recreational Trout Waters and Public Water Supply/Non-tidal Cold Water and Public Water Supply) (COMAR 2007a,b,c,d). Assessment of aquatic health is based on Maryland's biocriteria protocol, which evaluates both the amount and diversity of the benthic and fish community through the use of the IBI (Roth et al. 1998, 2000; Stribling et al. 1998).

Reductions of sediment loads are expected to result from decreased watershed and streambed erosion, which will then lead to improved benthic and fish habitat conditions. Specifically, sediment load reductions are expected to result in an increase in the number of benthic sensitive species present, an increase in the available and suitable habitat for a benthic community, a possible decrease in fine sediment (fines), and improved stream habitat diversity, all of which will result in improved water quality.

4.0 TOTAL MAXIMUM DAILY LOADS AND SOURCE ALLOCATION

4.1 Overview

This section describes how the sediment TMDL and corresponding allocations were developed for the Lower Monocacy River. Section 4.2 describes the analysis framework for estimating sediment loading rates and the assimilative capacity of the watershed stream system. Section 4.3 summarizes the scenarios that were used in the analysis and presents results. Section 4.4 discusses critical conditions and seasonality. Section 4.5 discusses the consideration of other related TMDLs within the assessment unit. Section 4.6 explains the calculations of TMDL loading caps. Section 4.7 details the load allocations, and Section 4.8 explains the rationale for the margin of safety. Finally, Section 4.9 summarizes the TMDL.

4.2 Analysis Framework

The stressor identification methodology (see Section 2.3) identifies the most direct measure of sediment pollutant loading as water column TSS concentrations. Elevated TSS loads are linked with negative sediment impacts to stream geomorphology and aquatic health. Since TSS numeric criterion is not available, a reference watershed approach will be used to establish the TMDL.

Watershed Model

The watershed model framework chosen for the Lower Monocacy River TMDL was the CBP P5 long-term average annual watershed model EOS loading rates. The spatial domain of the CBP P5 watershed model segmentation aggregates to the Maryland 8-digit watersheds, which is consistent with the impairment listing. The EOS loading rates were used because actual time variable CBP P5 calibration and scenario runs are currently being developed and are not yet available. These target-loading rates are used to calibrate the land use EOS loads within the CBP P5 model and thus should be consistent with future CBP modeling efforts.

The nonpoint source and NPDES stormwater baseline sediment loads generated within the Lower Monocacy River watershed are calculated as the sum of corresponding land use EOS loads within the watershed and represent a long-term average loading rate. Individual land use EOS loads are calculated as a product of the land use area, land use target loading rate, and loss from the EOF to the main channel. The loss from the EOF to the main channel is the *sediment delivery ratio* and is defined as the ratio of the sediment load reaching a basin outlet to the total erosion within the basin. A *sediment delivery ratio* is estimated for each land use type based on the proximity of the land use to the main channel. Thus, as the distance to the main channel increases, more sediment is stored within the channels (i.e., *sediment delivery ratio* decreases). Details of the data sources for the unit loading rates can be found in Section 2.2 of this report.

The Lower Monocacy River watershed was evaluated using one TMDL segment (see Figure 5).

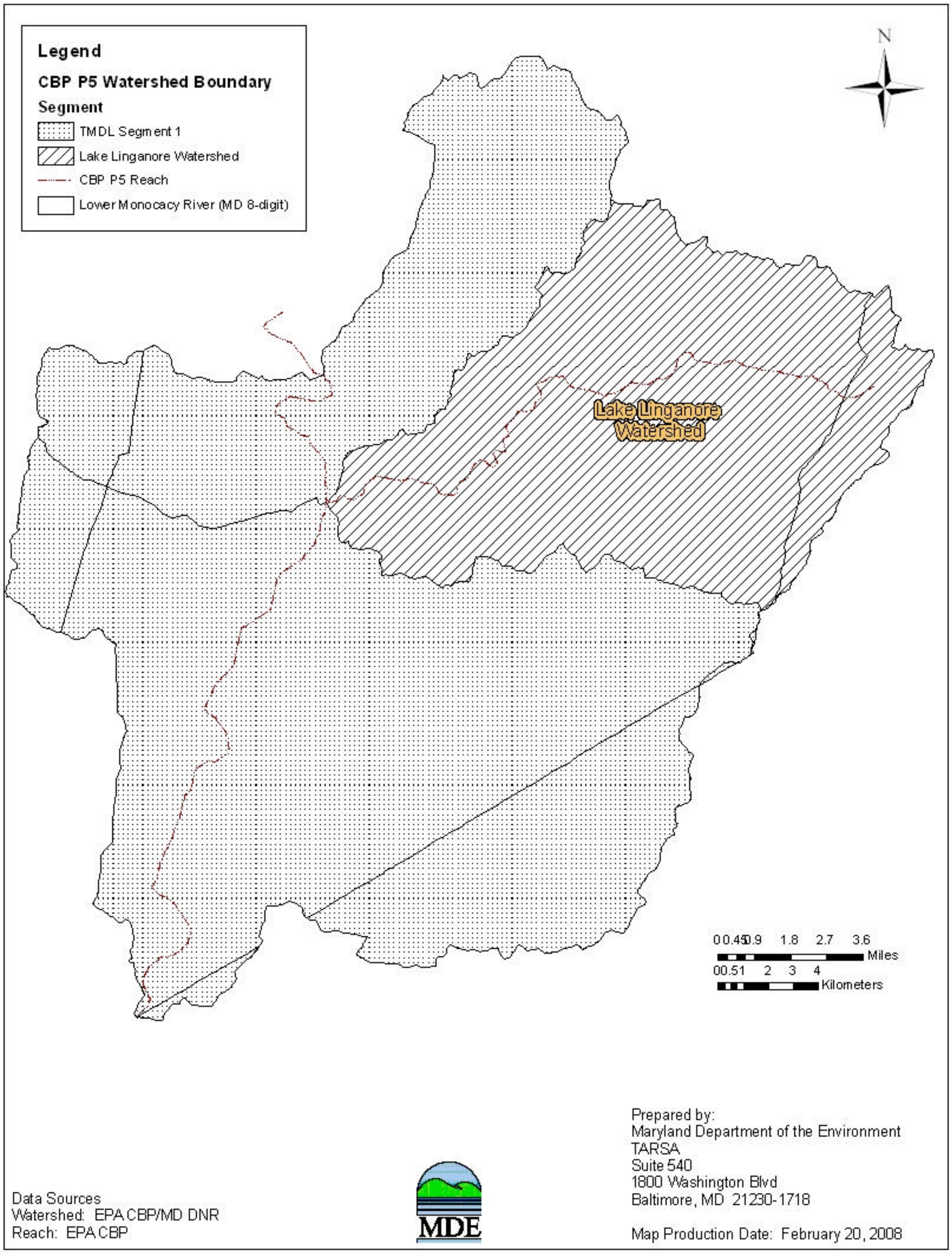


Figure 5: Lower Monocacy River Watershed Segmentation

Reference Watershed Approach

Currently in Maryland, there are no specific numeric criteria that quantify the impact of sediment on the aquatic health of non-tidal stream systems. Therefore, in order to quantify the impact of sediment on the aquatic health of non-tidal stream systems, a reference watershed TMDL approach was used and resulted in the establishment of a *sediment loading threshold* for watersheds within the Highland and Piedmont physiographic regions (Currey et al. 2006). In summary, reference watersheds were determined based on the BIBI/FIBI average watershed scores significantly greater than 3.0 (based on a scale of 1 – poor to 5 – good). A threshold of 3.0 was selected because this is the level indicative of satisfactory water quality per Maryland's biocriteria (Roth et al. 1998, 2000; Stribling et al. 1998). In determining if the average watershed score is significantly greater than 3.0, a 90% confidence interval was calculated for each watershed based on the individual MBSS sampling results.

Comparison of watershed sediment loads to loads from reference watersheds requires that the watersheds be similar in physical and hydrological characteristics. To satisfy this requirement, Currey et al. (2006) selected reference watersheds only from the Highland and Piedmont physiographic regions (see appendix A for the list of reference watersheds). This region is consistent with the non-coastal region that was identified in the 1998 development of FIBI and subsequently used in the development of BIBI (Roth et al. 1998; Stribling et al. 1998).

To reduce the effect of the variability within the Highland and Piedmont physiographic regions, the watershed sediment loads were then normalized by a constant background condition, the all forested watershed condition. This new normalized term, defined as the *forest normalized sediment load* (Y_n), represents how many times greater the current watershed sediment load is than the *all forested sediment load*. A similar approach was used by EPA Region 9 for sediment TMDLs in California (e.g., Navarro River or Trinity River TMDLs), where the loading capacity was based on an analysis of the amount of human-caused sediment delivery that can occur in addition to natural sediment delivery, without causing adverse impacts to aquatic life. The *forest normalized sediment load* for this TMDL is calculated as the current watershed sediment load divided by the *all forested sediment load*. The equation for the *forest normalized sediment load* is as follows:

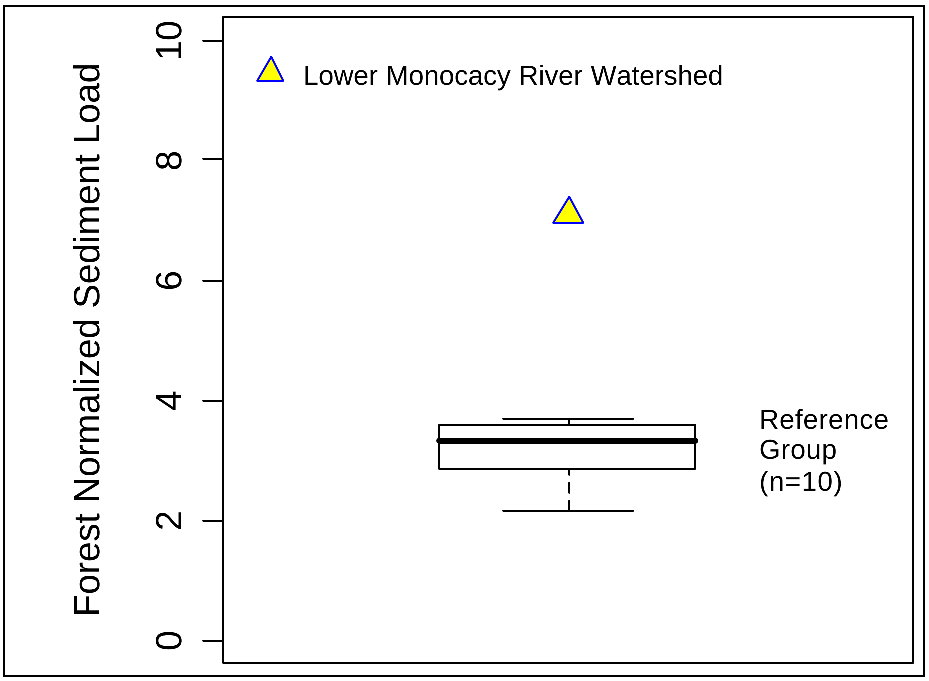
$$Y_n = \frac{y_{ws}}{y_{for}} \qquad (4.1)$$

where:

Y_n = forest normalized sediment load
y_{ws} = current watershed sediment load (ton/yr)
y_{for} = all forested sediment load (ton/yr)

An average *sediment loading threshold* of approximately 3.6 was established by Currey et al. (2006) with an 80% confidence interval ranging from 3.3 to 4.1. The lower confidence interval of 3.3 was chosen as an environmentally conservative approach to develop this TMDL (see Appendix A for more details).

A comparison of the Lower Monocacy River watershed *forest normalized sediment load* to the *forest normalized reference sediment load* (also referred to as the *sediment loading threshold*) is shown in Figure 6. The *forest normalized sediment load* exceeds the *sediment loading threshold*, indicating that the Lower Monocacy River is receiving loads that are above the maximum allowable load that the watershed can sustain and still meet water quality standards.



Note: The *forest normalized sediment load* is unitless and represents how many times greater the current watershed sediment load is than the *all forested sediment load.*

Figure 6: Lower Monocacy River Forest Normalized Sediment Load Compared to Reference Watershed Group

4.3 Scenario Descriptions and Results

The following analyses allow a comparison of baseline conditions (under which water quality problems exist) with future conditions, which project the water quality response to various simulated sediment load reductions. The analyses are grouped according to baseline conditions and future conditions associated with TMDLs.

Baseline Conditions

The baseline conditions are intended to provide a point of reference by which to compare the future scenario that simulates conditions of a TMDL. The baseline conditions typically reflect an approximation of nonpoint source and upstream loads during the monitoring time frame, as well as estimated point source loads based on discharge data for the same period.

The Lower Monocacy River watershed baseline sediment loads are estimated using the CBP P5 target EOS land use sediment loading rates with the CBP P5 2000 land use. Watershed loading calculations, based on the CBP P5 segmentation scheme, are represented by multiple CBP P5 model segments within the TMDL analysis segment. The TSS loads from these segments are combined to represent the baseline condition. The point source sediment loads are estimated based on the existing permit information. Details of these loading source estimates can be found in Section 2.2, Section 4.6, and Appendix B of this report.

Future (TMDL) Conditions

This scenario represents the future conditions of maximum allowable sediment loads that will support a healthy biological community. In the TMDL calculation, the allowable load for the impaired watershed is calculated as the product of the *sediment loading threshold* (determined from watersheds with a healthy benthic community) and the Lower Monocacy River *all forested sediment load* (see Section 4.3). The resulting load is considered the maximum allowable load the watershed can receive and still meet water quality standards.

The TMDL loading and associated reductions are averaged at the Maryland 8-digit watershed scale, which is consistent with the original listing scale. It is important to recognize that some subwatersheds may require higher reductions than others, depending on the distribution of the land use.

The formula for estimating the TMDL is as follows:

$$TMDL = \sum_{i=1}^{n} Yn_{ref} \cdot y_{forest_i} \qquad (4.2)$$

where

TMDL = allowable load for impaired watershed (ton/yr)
Yn_{ref} = sediment loading threshold = forest normalized reference sediment load (3.3)
y_{forest_i} = all forested sediment load for segment i (ton /yr)
i = CBP P5 model segment
n = number of CBP P5 model segments in watershed

The Lower Monocacy River TMDL is estimated using equation 4.2.

4.4 Critical Condition and Seasonality

EPA's regulations require TMDLs to take into account seasonality and critical conditions for stream flow, loading, and water quality parameters (CFR 2007b). The intent of this requirement is to ensure that the water quality of the waterbody is protected during times when it is most vulnerable. The biological monitoring data used to determine the reference watersheds integrates the stress effects over the course of time and thus inherently addresses critical conditions. Seasonality is captured in two components. First, it is implicitly included in biological sampling. Second, the MBSS dataset included benthic sampling in the spring and fish sampling in the summer.

4.5 TMDL Loading Caps

This section presents the average annual TMDL of TSS for the Lower Monocacy River watershed. This load is considered the maximum allowable long-term average annual load the watershed can receive and still meet water quality standards.
The TMDL was based on equation 4.2 and set at a load 3.3 times the all forested condition. A constant reduction was estimated for the predominant controllable sources (i.e., significant contributors of sediment to the stream system) in the TMDL analysis segment. If only these predominant (generally the largest) sources are controlled, water quality standards can be achieved in the most effective, efficient, and equitable manner. Predominant sources typically include urban land, high till crops, low till crops, hay, pasture, and harvested forest, but additional sources might need to be controlled in order to ensure that the water quality standards are attained.

The Lower Monocacy River Baseline Load and TMDL are shown in Table 10.

Table 10: Lower Monocacy River Baseline Load and TMDL

Baseline Load (ton/yr)	TMDL (ton/yr)	Reduction (%)
146,420.0	90,158.0	38.4

Note:[1]The load summary includes upstream loads from the Lake Linganore and Upper Monocacy River watersheds.

4.6 Load Allocations Between Point and Nonpoint Sources

The allocations described in this section summarize a TMDL of TSS established to meet the water quality criteria in the Lower Monocacy River watershed. Per EPA regulation, all TMDLs need to be presented as a sum of waste load allocations (WLAs) for point sources and load allocations (LAs) for nonpoint source loads generated within the assessment unit, as well as natural background, tributary, and adjacent segment loads (CFR 2007a). Consequently, the Lower Monocacy River TMDL allocations are presented in terms of WLAs (i.e., point source loads identified within the assessment unit) and LAs (i.e., the assessment unit's nonpoint source loads and loads entering the watershed from outside the assessment unit). The State reserves the right to revise these allocations provided the revisions are consistent with achieving water quality standards.

As described in Section 4.5, a constant reduction was applied to the predominant controllable sources in the assessment unit. In this watershed, crop, pasture, and urban land were identified as the predominant controllable sources. Forest is the only non-controllable source, as it represents the most natural condition in the watershed. No reductions were applied to permitted process load sources because at 0.5% of the total load, such controls would produce no discernable water quality benefit.

Table 11 summarizes the TMDL results for the entire watershed derived by applying the reductions equally to the predominant controllable sediment sources. The source categories in the table represent aggregates of multiple sources (e.g. crop source is an aggregate of high till, low till, hay, animal feeding operations, and nursery sources). The TMDL results in a 54.6% reduction for the Lower Monocacy River Watershed Contribution and an overall reduction of 38.4%.

Table 11: Lower Monocacy River Watershed TMDL Reductions by Source Category

	Baseline Load Source Categories		Baseline Load (ton/yr)	TMDL Components	TMDL (ton/yr)	Reduction (%)
Lower Monocacy River Watershed Contribution	Nonpoint Source	Crop	21,406.9	LA	8,567.2	60.0%
		Extractive	261.6		261.6	0.0%
		Forest	1,615.7		1,615.7	0.0%
		Pasture	3,789.2		1,952.9	48.5%
	Point Source	Urban	8,312.5	WLA	3,256.8	60.8%
		Permits	723.4		723.4	0.0%
Sub-total			36,109.3		16,377.6	54.6%
Upstream	Lake Linganore[1]		11,585.0	Upstream LA	7,073.0	38.9%
	Upper Monocacy River Watershed[2]		98,725.7	Upstream LA	66,707.3	32.4%
Total			**146,420.0**		**90,158.0**	**38.4%**

Notes:[1] Background relating to the Lake Linganore upstream baseline load and TMDL are presented in the Lake Linganore TMDL document (MDE 2003).
[2] Background relating to the Upper Monocacy River watershed upstream baseline load and TMDL are presented in the Upper Monocacy River watershed TMDL document (MDE 2008a).

The WLA of the Lower Monocacy River watershed is allocated to two permitted source categories, Process Water WLA and Stormwater WLA. The categories are described below.

Process Water WLA

Process Water permits with specific TSS limits and corresponding flow information are assigned to the WLA. In this case, detailed information is available to accurately estimate the WLA. If specific TSS limits are not explicitly stated in the process water permit, then TSS loads are expected to be *de minimis.* If loads are *de minimis*, then they pose little or no risk to the aquatic environment and are not a significant source.

Process Water permits with specific TSS limits include:

- Individual industrial facilities
- Individual municipal facilities
- General mineral mining facilities

There are 24 process water sources with explicit TSS limits (see Appendix B), which include 2 industrial sources, 17 municipal sources, and 5 mineral mines. The total estimated TSS load from all of the process water sources is based on current permit limits and is equal to 723.4 ton/yr. As mentioned above, no reductions were applied to this source because at 0.5% of the total load, such controls would produce no discernable water quality benefit.

NPDES Stormwater WLA

Per EPA requirements, "stormwater discharges that are regulated under Phase I or Phase II of the NPDES stormwater program are point sources that must be included in the WLA portion of a TMDL" (US EPA 2002). Phase I and II permits can include the following types of discharges:

- Small, medium, and large MS4s – these can be owned by local jurisdictions, municipalities, and state and federal entities e.g., departments of transportation, hospitals, military bases),
- General industrial stormwater permitted facilities, and
- Small and large construction sites.

EPA recognizes that available data and information are usually not detailed enough to determine WLAs for NPDES regulated stormwater discharges on an outfall-specific basis (US EPA 2002). Therefore, NPDES regulated stormwater loads within the Lower Monocacy River watershed will be expressed as a single NPDES stormwater WLA. Upon approval of the TMDL, "NPDES-regulated municipal stormwater and small construction storm water discharges effluent limits should be expressed as BMPs or other similar requirements, rather than as numeric effluent limits" (US EPA 2002).

The Lower Monocacy River NPDES stormwater WLA is based on reductions applied to the sediment load from the urban land use of the watershed and may include legacy or other sediment sources. Some of these sources may also be subject to controls from other management programs. The Lower Monocacy River NPDES stormwater WLA requires an overall reduction of 60.8% (see Table 11). The NPDES stormwater WLA distribution between Frederick County and Montgomery County is presented in Appendix B. It constitutes a proportional allocation of the stormwater load to the entire urban land area of each county and may include any or all of the NPDES stormwater discharges listed above.

As stormwater assessment and/or other program monitoring efforts result in a more refined source assessment, MDE reserves the right to revise the current NPDES stormwater WLA provided the revisions are consistent with achieving water quality standards.

For more information on methods used to calculate the baseline urban sediment load see Section 2.2.2. Additionally, Appendix B provides a detailed summary of all point source allocations.

4.7 Margin of Safety

All TMDLs must include a margin of safety to account for any lack of knowledge and uncertainty concerning the relationship between loads and water quality (CFR 2007b). It is proposed that the estimated variability around the reference watershed group used in this analysis already accounts for such uncertainty. Analysis of the reference group *forest normalized sediment loads* indicates that approximately 75% of the reference watersheds have a value of less than 3.6, consistent with the recommended value reported by Currey et al. (2006). Also, 50% of the reference watersheds have a value less than 3.3, consistent with the lower confidence interval value reported in Currey et al. (2006). Based on this analysis the *forest normalized reference sediment load* (also referred to as the *sediment loading threshold*) was set at the median value of 3.3. This is considered an environmentally conservative estimate, since 50% of the reference watersheds have a load above this value, which when compared to the 75% value, results in an implicit margin of safety of approximately 8%.

4.8 Summary of Total Maximum Daily Loads

The average annual Lower Monocacy River TMDL is summarized in Table 12. The TMDL is the sum of the LAs, NPDES Stormwater WLA, Process Water WLA, and MOS. The LAs include nonpoint source loads generated within the Lower Monocacy River watershed and loads from upstream sources. The Maximum Daily Load (MDL) is summarized in Table 13 (see Appendix C for more details).

Table 12: Average Annual Lower Monocacy River TMDL of Sediment/TSS (ton/yr)

TMDL (ton/yr)	=	**LA**					+	**WLA**			+	**MOS**
		LA_{LL}[1]	+	**LA_{UM}[2]**	+	**LA_{LM}**		**NPDES Stormwater WLA_{LM}**	+	**Process Water WLA_{LM}**		
90,158.0	=	7,073.0	+	66,707.3	+	12,397.5	+	3,256.8	+	723.4	+	Implicit
		Upstream Load Allocations[3,4]				Lower Monocacy River TMDL Contribution						

Notes:[1] For Lake Linganore watershed WLA and LA characterization, please refer to the "Total Maximum Daily Loads of Phosphorus and Sediments for Lake Linganore, Frederick County, MD" (MDE 2003).

[2] For Upper Monocacy River watershed WLA and LA characterization, please refer to the "Total Maximum Daily Load of Sediment in the Upper Monocacy River Watershed, Frederick and Carroll Counties, Maryland" (MDE 2008a).

[3] Although for the purpose of this analysis the upstream load is referred to as an LA, it could include loads from point and nonpoint sources.

[4] A delivery factor of 1 was used for all of the Upstream Load Allocations**.**

Table 13: Lower Monocacy River Maximum Daily Loads of Sediment/TSS (ton/day)

MDL (ton/day)	=	LA					+	WLA			+	MOS
		LA_{LL}[1]	+	LA_{UM}[2]	+	LA_{LM}		NPDES Stormwater WLA_{LM}	+	Process Water WLA_{LM}		
2,416.7		268.8		1,547.4		471.1		123.8		5.7	+	Implicit
		Upstream Load Allocations[3,4]				Lower Monocacy River Watershed MDL Contribution						

Notes: [1] An MDL is not calculated within the 2003 Lake Linganore Sediment TMDL. Thus, this MDL was established based off the average annual TMDL specified in the 2003 Lake Linganore Sediment TMDL document via the methods described in Appendix C.

[2] For Upper Monocacy River watershed MDL WLA and LA characterization, please refer to the "Total Maximum Daily Load of Sediment in the Upper Monocacy River Watershed, Frederick and Carroll Counties, Maryland" (MDE 2008a).

[3] Although for the purpose of this analysis the upstream loads are referred to as an LA, they could include loads from point and nonpoint sources.

[4] A delivery factor of 1 was used for all of the Upstream Load Allocations.

5.0 ASSURANCE OF IMPLEMENTATION

This section provides the basis for reasonable assurances that the sediment TMDL will be achieved and maintained. Section 303(d) of the Clean Water Act and current EPA regulations require reasonable assurance that the TMDL load and wasteload allocations can and will be implemented (CFR 2007b). Maryland has several well-established programs to draw upon, including the Water Quality Improvement Act of 1998 (WQIA) and the Federal Nonpoint Source Management Program (§ 319 of the Clean Water Act).

Potential funding sources for implementation include the Buffer Incentive Program (BIP) and the Maryland Agriculture water quality cost share program (MACS). Other funding available for local governments includes the State Water Quality Revolving Loan Fund and the Stormwater Pollution Cost Share Program. Details of these programs and additional funding sources can be found at http://www.dnr.state.md.us/bay/services/summaries.html.

Potential best management practices for reducing sediment loads and resulting impacts can be grouped into three general categories. The first is directed toward agricultural lands, the second to urban (developed) land, and the third applies to all land uses.

In agricultural areas comprehensive soil conservation plans can be developed that meet criteria of the USDA-NRCS Field Office Technical Guide (USDA 1983). Soil conservation plans help control erosion by modifying cultural practices or structural practices. Cultural practices may change from year to year and include changes to crop rotations, tillage practices, or use of cover crops. Structural practices are long-term measures that include, but are not limited to, the installation of grass waterways (in areas with concentrated flow), terraces, diversions, sediment basins, or drop structures. The reduction percentage attributed to cultural practices is determined based on changes in land use, while structural practices have a reduction percentage up to 25%. In addition, livestock can be controlled via stream fencing and rotational grazing. Sediment reduction efficiencies of methods applicable to pasture land use range from 40% to 75% (US EPA 2004).

Sediment from urban areas can be reduced by stormwater retrofits, impervious surface reduction, and stream restoration. Stormwater retrofits include modification of existing stormwater structural practices to address water quality. Reductions range from as low as 10% for dry detention to approximately 80% for wet ponds, wetlands, infiltration practices, and filtering practices. Impervious surface reduction results in a change in hydrology that could reduce stream erosion (US EPA 2003).

All non-forested land uses can benefit from improved riparian buffer systems. A riparian buffer reduces the effects of upland sediment sources through trapping and filtering. Riparian buffer efficiencies vary depending on type (grass or forested), land use (urban or agriculture), and physiographic region. The CBP estimates riparian buffer sediment reduction efficiencies in the Lower Monocacy River region to be approximately 50% (US EPA 2006).

In summary, through the use of the aforementioned funding mechanisms and best management practices, there is reasonable assurance that this TMDL can be implemented.

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APPENDIX A – Watershed Characterization Data

Table A-1: Reference Watersheds

MD 8-digit Name[1]	MD 8-digit	FIBI n	BIBI n	FIBI[4]	BIBI	Forest Normalized[2] Sediment Load
Deer Creek	02120202	28	28	Ind.	Pass	3.63
Broad Creek	02120205	10	10	Ind.	Pass	3.67
Little Gunpowder Falls	02130804	19	20	Ind.	Pass	3.26
Prettyboy Reservoir	02130806	11	11	Pass	Pass	2.87
Liberty Reservoir	02130907	31	31	Pass	Pass	3.28
S Branch Patapsco	02130908	10	10	Pass	Pass	3.57
Rocky Gorge Dam	02131107	10	10	Pass	Pass	3.43
Brighton Dam	02131108	11	11	Ind.	Pass	3.61
Town Creek	02140512	16	20	Ind.	Pass	2.17
Savage River	02141006	13	14	Pass	Pass	2.48
Median[3]						3.3
75th Percentile						3.6

Notes: 1 Potomac River Lower North Branch determined to be an outlier through statistical analysis and best professional judgment; Fifteen Mile Creek watershed was removed because the majority of the watershed is in Pennsylvania.

2 Forest normalized sediment loads based on Maryland watershed area only (Consistent with MBSS random monitoring data).

3 Median rounded down (3.36 to 3.3) as conservative estimate

4 Ind.= Indeterminate.

Table A-2: Benthic SSDI Calculation

Site	Epifaunal Substrate	Percent embeddedness	Benthic Tolerant Species	Bank Stability Index	Benthic SSDI
LMON-112-R-2003	3	3	3	3	3.0
LMON-114-R-2003	3	5	5	3	4.0
LMON-119-R-2003	3	3	1	3	2.5
LMON-121-R-2003	5	5	1	1	3.0
LMON-125-R-2003	3	3	3	3	3.0
LMON-131-R-2003	3	3	3	3	3.0
LMON-136-R-2003	3	5	5	5	4.5
LMON-210-R-2003	3	3	1	5	3.0
LMON-215-R-2003	5	5	3	3	4.0
LMON-220-R-2003	1	3	3	3	2.5
LMON-322-R-2003	5	5	3	1	3.5
Average	**3.36**	**3.91**	**2.82**	**3.00**	**3.27 ± 0.32**

Table A-3: Fish SSDI Calculation

Site	Percent embeddedness	Instream Habitat	Epifaunal Substrate	Fish SSDI
LMON-112-R-2003	3	3	3	3.00
LMON-114-R-2003	5	1	3	3.00
LMON-119-R-2003	3	3	3	3.00
LMON-121-R-2003	5	3	3	3.67
LMON-125-R-2003	3	3	3	3.00
LMON-131-R-2003	3	1	3	2.33
LMON-136-R-2003	5	3	3	3.67
LMON-210-R-2003	3	3	3	3.00
LMON-215-R-2003	5	5	5	5.00
LMON-220-R-2003	3	3	1	2.33
LMON-322-R-2003	5	5	5	5.00
Average	**3.91**	**3.00**	**3.18**	**3.36±0.45**

APPENDIX B – MDE Permit Information for the Lower Monocacy River Watershed

Table B-1: Permit Summary for the Lower Monocacy River Watershed

Permit #	NPDES	Facility	County	City	Type	TMDL
00DP0967	MD0002038	ESSROC CEMENT CORPORATION - FREDERICK PLANT	FREDERICK	FREDERICK	WMA1	Process Water WLA
92DP2191	MD0061093	REICHS FORD SANITARY LANDFILL	FREDERICK	FREDERICK	WMA1	Process Water WLA
00DP0278	MD0025089	WHITE ROCK WWTP	FREDERICK	FREDERICK	WMA2	Process Water WLA
00DP0784	MD0023060	CONCORD TRAILER PARK	FREDERICK	JEFFERSON	WMA2	Process Water WLA
00DP1574	MD0056481	KEMPTOWN SCHOOL WWTP	FREDERICK	MONROVIA	WMA2	Process Water WLA
00DP1633	MD0057100	NEW LIFE FOURSQUARE CHURCH AND SCHOOL	FREDERICK	FREDERICK	WMA2	Process Water WLA
00DP1990	MD0059609	MONROVIA WWTP	FREDERICK	MONROVIA	WMA2	Process Water WLA
01DP0672	MD0022683	CRESTVIEW ESTATES WWTP	FREDERICK	FREDERICK	WMA2	Process Water WLA
01DP3200	MD0067768	HYATTSTOWN WWTP	MONTGOMERY	CLARKSBURG	WMA2	Process Water WLA
02DP0478	MD0020729	NEW MARKET WWTP	FREDERICK	FREDERICK	WMA2	Process Water WLA
02DP0607A	MD0023710	DAN-DEE MOTEL & COUNTRY INN	FREDERICK	FREDERICK	WMA2	Process Water WLA
02DP1024	MD0024244	CRACKED CLAW WWTP	FREDERICK	IJAMSVILLE	WMA2	Process Water WLA
02DP2814	MD0065269	PLEASANT BRANCH WWTP	FREDERICK	PLEASANT GROVE	WMA2	Process Water WLA
02DP2841	MD0065439	MILL BOTTOM WWTP	FREDERICK	MT. AIRY	WMA2	Process Water WLA
03DP1036	MD0022870	SPRINGVIEW MOBILE HOME PARK	FREDERICK	FREDERICK	WMA2	Process Water WLA

Permit #	NPDES	Facility	County	City	Type	TMDL
99DP1855	MD0058661	WOODSBORO WWTP	FREDERICK	WOODSBORO	WMA2	Process Water WLA
01DP0801	MD0021610	FREDERICK CITY WWTP	FREDERICK	FREDERICK	WMA2M	Process Water WLA
03DP0809	MD0021822	BALLENGER CREEK WWTP	FREDERICK	FREDERICK	WMA2M	Process Water WLA
03DP2527	MD0020877	FORT DETRICK - AREA C	FREDERICK	FREDERICK	WMA2M	Process Water WLA
00MM0621	MDG490621	LAFARGE- FREDERICK QUARRY	FREDERICK	FREDERICK	WMA5	Process Water WLA
00MM2695	MDG492695	SUPERIOR PLUS, LLC	FREDERICK	FREDERICK	WMA5	Process Water WLA
00MM9704	MDG499704	ELLIE MAY, LLC - BUCKEYSTOWN MINE	FREDERICK	BUCKEYSTOWN	WMA5	Process Water WLA
00MM9818	MDG499818	FREDERICK CONCRETE PLANT	FREDERICK	KEYMAR	WMA5	Process Water WLA
00MM9893	MDG499893	DANIEL G. SCHUSTER, INC. - FREDERICK PLANT	FREDERICK	FREDERICK	WMA5	Process Water WLA
02SW0124	N/A	FORT DETRICK - AREA A	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW0212	N/A	ALLIED WASTE SERVICES OF FREDERICK	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW0285	N/A	MORNINGSTAR FOODS, INC.	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW0336	N/A	M-NCPPC - LITTLE BENNETT MAINTENANCE YARD	MONTGOMERY	CLARKSBURG	WMA5SW	Stormwater WLA
02SW0518	N/A	ACCUBID EXCAVATION, INC.	FREDERICK	MOUNT AIRY	WMA5SW	Stormwater WLA
02SW0547	N/A	PRECISION AUTOBODY, INC.	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW0674	N/A	FREDERICK ASPHALT CO., L.C. AT ESSROC	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW0696	N/A	RICHARD B. RUDY, INC.	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW0699	N/A	FREDERICK CITY WWTP	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA

Permit #	NPDES	Facility	County	City	Type	TMDL
02SW0726	N/A	D.M. BOWMAN, INC. - FREDERICK	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW0850	N/A	UNITED PARCEL SERVICE - FREDERICK	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW0987	N/A	ENTENMANN'S, INC.	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1066	N/A	RICHARD F. KLINE, INC. - FREDERICK	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1067	N/A	MCCORMICK PAINT WORKS COMPANY - FREDERICK	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1099	N/A	HAHN TRANSPORTATION INC.	FREDERICK	NEW MARKET	WMA5SW	Stormwater WLA
02SW1100	N/A	FREDERICK MUNICIPAL AIRPORT	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1162	N/A	RELIABLE JUNK COMPANY INC.	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1163	N/A	FREDERICK AUTO PARTS, INC.	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1199	N/A	BP SOLAR INTERNATIONAL, LLC	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1226	N/A	FORT DETRICK - AREA B	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1227	N/A	FORT DETRICK - AREA C	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1343	N/A	SHA - FREDERICK SHOP	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1349	N/A	RINKER MATERIALS HYDRO CONDUIT-FREDERICK	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1564	N/A	YORK BUILDING PRODUCTS - FREDERICK	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1571	N/A	MTA - TRAIN STORAGE YARD	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1654	N/A	PLEASANTS CONSTRUCTION INC.	MONTGOMERY	CLARKSBURG	WMA5SW	Stormwater WLA
02SW1707	N/A	WASTE MANAGEMENT OF MARYLAND - FREDERICK COUNTY	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA

Permit #	NPDES	Facility	County	City	Type	TMDL
02SW1767	N/A	INVITROGEN CORPORATION	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1773	N/A	DAIRY MAID DAIRY, INC.	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1775	N/A	SCHWERMAN TRUCKING COMPANY - FREDERICK TERMINAL	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1780	N/A	GRIMES PROPERTIES, LLC	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1799	N/A	ALTEC INDUSTRIES, INC.	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1851	N/A	COUNTRY SIDE USED AUTO PARTS	FREDERICK	MT. AIRY	WMA5SW	Stormwater WLA
02SW1866	N/A	ROLLING FRITO-LAY SALES - FREDERICK DC	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1878	N/A	BALLENGER CREEK WWTP	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1887	N/A	FREDERICK COUNTY PUBLIC SCHOOLS - HAYWARD BUS LOT	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1888	N/A	FREDERICK COUNTY TRANSIT	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1890	N/A	FREDERICK COUNTY HIGHWAYS - FREDERICK HQ	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1891	N/A	FREDERICK COUNTY HIGHWAYS - JOHNSVILLE	FREDERICK	UNION BRIDGE	WMA5SW	Stormwater WLA
02SW1893	N/A	FREDERICK COUNTY HIGHWAYS - URBANA	FREDERICK	IJAMSVILLE	WMA5SW	Stormwater WLA
02SW1942	N/A	FREDERICK COUNTY LAW ENFORCEMENT COMPLEX	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1950	N/A	TAMKO BUILDING PRODUCTS, INC.	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1975	N/A	MEDIMMUNE, INC.	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
02SW1994	N/A	SFA DEFENSE PRODUCTS DIVISION	FREDERICK	FREDERICK	WMA5SW	Stormwater WLA
00DP3320	MD0068349	MONTGOMERY COUNTY MS4	MONTGOMERY	ALL CITIES	WMA6	Stormwater WLA

Permit #	NPDES	Facility	County	City	Type	TMDL
02DP3321	MD0068357	FREDERICK COUNTY MS4	FREDERICK	ALL CITIES	WMA6	Stormwater WLA
MS4-FR-003	N/A	FREDERICK CITY MS4	FREDERICK	FREDERICK	WMA6G	Stormwater WLA
05SS5501	MD0055501	STATE HIGHWAY ADMINISTRATION MS4	ALL	ALL	WMA6	Stormwater WLA
		MDE GENERAL PERMIT TO CONSTRUCT	ALL	ALL		Stormwater WLA

Notes: [1]TMDL column identifies how the permit was considered in the TMDL allocation.
[2]WTP = Water Treatment Plant
[3]WWTP = Wastewater Treatment Plant

Table B-2: Industrial Permit Data for the Lower Monocacy River Watershed

Facility name	Permit #	NPDES #	Flow (MGD)	Permit Avg Monthly Conc. (mg/l)	Permit Daily Max Conc. (mg/l)	WLA (tons/yr)
ESSROC CEMENT CORPORATION - FREDERICK PLANT	00DP0967	MD0002038	0.025	50	50	1.90
REICHS FORD SANITARY LANDFILL	92DP2191	MD0061093	0.045	35	70	2.394

Notes:[1] MGD = Millions of gallons per day
[2] mg/l = Milligram per liter

Table B-3: Municipal Permit Data for the Lower Monocacy River Watershed

Facility name	MDE Permit #	NPDES #	Flow (MGD)	Permit Avg Monthly Conc. (mg/l)	Permit Weekly Max Conc. (mg/l)	WLA (tons/yr)
CONCORD TRAILER PARK	00DP0784	MD0023060	0.015	30	45	0.684
CRACKED CLAW WWTP	02DP1024	MD0024244	0.03	30	45	1.368
CRESTVIEW ESTATES WWTP	01DP0672	MD0022683	0.04	30	45	0.912
CRESTVIEW ESTATES WWTP	01DP0672	MD0022683	0.04	12	18	0.365
DAN-DEE MOTEL & COUNTRY INN	02DP0607A	MD0023710	0.012	30	45	0.5472
HYATTSTOWN WWTP	01DP3200	MD0067768	0.02	30	45	0.912
KEMPTOWN SCHOOL WWTP	00DP1574	MD0056481	0.005	30	45	0.228
MILL BOTTOM WWTP	02DP2841	MD0065439	0.1	30	45	4.56
MONROVIA WWTP	00DP1990	MD0059609	0.2	30	45	9.12
NEW LIFE FOURSQUARE CHURCH AND SCHOOL	00DP1633	MD0057100	0.005	30	45	0.228
NEW MARKET WWTP	02DP0478	MD0020729	0.24	30	45	10.944
PLEASANT BRANCH WWTP	02DP2814	MD0065269	0.1	30	45	4.56
SPRINGVIEW MOBILE HOME PARK	03DP1036	MD0022870	0.007	30	45	0.3192
WHITE ROCK WWTP	00DP0278	MD0025089	0.05	30	45	2.28
WOODSBORO WWTP	99DP1855	MD0058661	0.1	30	45	4.56
BALLENGER CREEK WWTP	03DP0809	MD0021822	6	30	45	273.6
FORT DETRICK - AREA C	03DP2527	MD0020877	2	10	15	30.4
FREDERICK CITY WWTP	01DP0801	MD0021610	8	26	39	316.16

Table B-4: General Mine Permit Data for the Lower Monocacy River Watershed

Facility name	MDE Permit #	NPDES #	Flow (MGD)	Permit Avg Quarterly Conc. (mg/l)	Permit Daily Max Conc. (mg/l)	WLA (tons/yr)
DANIEL G. SCHUSTER, INC. - FREDERICK PLANT	00MM9893	MDG499893	0.001	30	60	0.046
ELLIE MAY, LLC - BUCKEYSTOWN MINE	00MM9704	MDG499704	0.001	30	66	0.046
FREDERICK CONCRETE PLANT	00MM9818	MDG499818	0.0008	30	60	0.036
LAFARGE- FREDERICK QUARRY	00MM0621	MDG490621	2.5	15	31	57.0
SUPERIOR PLUS, LLC	00MM2695	MDG492695	0.005	30	60	0.228

Table B-5: Stormwater Permit Data for the Lower Monocacy River Watershed[1]

Permit #	Facility	NPDES group
02SW0124	FORT DETRICK - AREA A	Phase-I
02SW0212	ALLIED WASTE SERVICES OF FREDERICK	Phase-I
02SW0285	MORNINGSTAR FOODS, INC.	Phase-I
02SW0336	M-NCPPC - LITTLE BENNETT MAINTENANCE YARD	Phase-I
02SW0518	ACCUBID EXCAVATION, INC.	Phase-I
02SW0547	PRECISION AUTOBODY, INC.	Phase-I
02SW0674	FREDERICK ASPHALT CO., L.C. AT ESSROC	Phase-I
02SW0696	RICHARD B. RUDY, INC.	Phase-I
02SW0699	FREDERICK CITY WWTP	Phase-I
02SW0726	D.M. BOWMAN, INC. - FREDERICK	Phase-I
02SW0850	UNITED PARCEL SERVICE - FREDERICK	Phase-I
02SW0987	ENTENMANN'S, INC.	Phase-I
02SW1066	RICHARD F. KLINE, INC. - FREDERICK	Phase-I
02SW1067	MCCORMICK PAINT WORKS COMPANY - FREDERICK	Phase-I
02SW1099	HAHN TRANSPORTATION INC.	Phase-I
02SW1100	FREDERICK MUNICIPAL AIRPORT	Phase-I
02SW1162	RELIABLE JUNK COMPANY INC.	Phase-I
02SW1163	FREDERICK AUTO PARTS, INC.	Phase-I
02SW1199	BP SOLAR INTERNATIONAL, LLC	Phase-I
02SW1226	FORT DETRICK - AREA B	Phase-I
02SW1227	FORT DETRICK - AREA C	Phase-I
02SW1343	SHA - FREDERICK SHOP	Phase-I
02SW1349	RINKER MATERIALS HYDRO CONDUIT- FREDERICK	Phase-I
02SW1564	YORK BUILDING PRODUCTS - FREDERICK	Phase-I
02SW1571	MTA - TRAIN STORAGE YARD	Phase-I
02SW1654	PLEASANTS CONSTRUCTION INC.	Phase-I
02SW1707	WASTE MANAGEMENT OF MARYLAND - FREDERICK COUNTY	Phase-I

Permit #	Facility	NPDES group
02SW1767	INVITROGEN CORPORATION	Phase-I
02SW1773	DAIRY MAID DAIRY, INC.	Phase-I
02SW1775	SCHWERMAN TRUCKING COMPANY - FREDERICK TERMINAL	Phase-I
02SW1780	GRIMES PROPERTIES, LLC	Phase-I
02SW1799	ALTEC INDUSTRIES, INC.	Phase-I
02SW1851	COUNTRY SIDE USED AUTO PARTS	Phase-I
02SW1866	ROLLING FRITO-LAY SALES - FREDERICK DC	Phase-I
02SW1878	BALLENGER CREEK WWTP	Phase-I
02SW1887	FREDERICK COUNTY PUBLIC SCHOOLS - HAYWARD BUS LOT	Phase-I
02SW1888	FREDERICK COUNTY TRANSIT	Phase-I
02SW1890	FREDERICK COUNTY HIGHWAYS - FREDERICK HQ	Phase-I
02SW1891	FREDERICK COUNTY HIGHWAYS - JOHNSVILLE	Phase-I
02SW1893	FREDERICK COUNTY HIGHWAYS - URBANA	Phase-I
02SW1942	FREDERICK COUNTY LAW ENFORCEMENT COMPLEX	Phase-I
02SW1950	TAMKO BUILDING PRODUCTS, INC.	Phase-I
02SW1975	MEDIMMUNE, INC.	Phase-I
02SW1994	SFA DEFENSE PRODUCTS DIVISION	Phase-I
00DP3320	MONTGOMERY COUNTY MS4	Phase-I
02DP3321	FREDERICK COUNTY MS4	Phase-I
05SS5501	STATE HIGHWAY ADMINISTRATION MS4	Phase-I
	MDE GENERAL PERMIT TO CONSTRUCT	Phase-I/II
MS4-FR-003	FREDERICK CITY MS4	Phase-II

Notes: [1] Although not listed in this table, some individual permits from Tables B-2 through B-4 incorporate stormwater requirements and are accounted for within the NPDES Stormwater WLA.

Table B-6: NPDES Stormwater Baseline Loads and Wasteload Allocations per County

County	NPDES Stormwater BL_{LM} (tons/year)	NPDES Stormwater WLA_{LM} (tons/year)
Montgomery County	252.5	99.0
Frederick County	8,060.0	3,157.9
TOTAL	**8,312.5**	**3,256.8**

APPENDIX C – Technical Approach Used to Generate Maximum Daily Loads

Summary

This appendix documents the technical approach used to define maximum daily loads of TSS consistent with the average annual TMDL, which is protective of water quality standards in the Lower Monocacy River Watershed. The approach builds upon the modeling analysis that was conducted to determine the loadings of TSS and can be summarized as follows.

- The approach defines maximum daily loads for each of the source categories.
- The approach builds upon the TMDL modeling analysis that was conducted to ensure that average annual loading targets result in compliance with water quality standards.
- The approach converts daily time-series loadings into TMDL values in a manner that is consistent with available EPA guidance on generating daily loads for TMDLs.
- The approach considers a daily load level of a resolution based on the specific data that exists for each source category.

Introduction

The appendix documents the development and application of the approach used to define total maximum daily loads on a daily basis. It is divided into sections discussing:

- Basis for approach
- Options considered
- Selected approach
- Results of approach

Basis for approach

The overall approach for the development of daily loads was based upon the following factors:

- **Average Annual TMDL:** The basis of the average annual sediment TMDL is that cumulative high sediment loading rates have negative impacts on the biological community. Thus, the average annual sediment load was calculated to be protective of the aquatic life designated use.
- **CBP P5 Watershed Model Sediment Loads:** There are two spatial calibration points for sediment within the CBP P5 watershed model framework. First, EOS loads are calibrated to long term EOS target loads. These target loads are the loads used to determine an average annual TMDL. Furthermore, the target loads were used in the TMDL because, as calibration targets, they are expected to remain relatively unchanged during the final calibration stages of the CBP P5 model, and therefore will be the most consistent with the final CBP P5 watershed model TSS loading estimates. Currently, the CBP P5 model river segments are being calibrated to daily monitoring information for watersheds with a flow greater than 100 cfs, or an approximate area of 100 square miles.

- **Draft EPA guidance document entitled "Developing Daily Loads for Load-based TMDLs"** This guidance provides options for defining maximum daily loads when using TMDL approaches that generate daily output.

The rationale for developing TMDLs expressed as *daily* loads was to accept the existing average annual TMDL, but then develop a method for converting this number to a maximum *daily* load – in a manner consistent with EPA guidance and available information.

Options considered

The draft EPA guidance document for developing daily loads does not specify a single approach that must be adhered to, but rather it contains a range of acceptable options. The selection of a specific method for translating a time-series of allowable loads into the expression of a TMDL requires decisions regarding both the level of resolution (e.g., single daily load for all conditions vs. loads that vary with environmental conditions) and level of probability associated with the TMDL.

This section describes the range of options that were considered when developing methods to calculate the Lower Monocacy River Maximum Daily Loads.

Level of Resolution

The level of resolution pertains to the amount of detail used in specifying the maximum daily load. The draft EPA guidance on daily loads provides three categories of options for level of resolution, all of which are potentially applicable for the Lower Monocacy River watershed:

1. **Representative daily load:** In this option, a single daily load (or multiple representative daily loads) is specified that covers all time periods and environmental conditions.
2. **Flow-variable daily load:** This option allows the maximum daily load to vary based upon the observed flow condition.
3. **Temporally-variable daily load:** This option allows the maximum daily load to vary based upon seasons or times of varying source or water body behavior.

Probability Level

All TMDLs have some probability of being exceeded, with the specific probability being explicitly specified or implicitly assumed. This level of probability directly or indirectly reflects two separate phenomena:

1. Water quality criteria consist of components describing acceptable magnitude, duration, and frequency. The frequency component addresses how often conditions can allowably surpass the combined magnitude and duration components.

2. Pollutant loads, especially from wet weather sources, typically exhibit a large degree of variability over time. It is rarely practical to specify a "never to be exceeded value" for a daily load, as essentially any loading value has some finite probability of being exceeded.

The draft daily load guidance document states that the probability component of the maximum daily load should be "based on a representative statistical measure" that is dependent upon the specific TMDL and best professional judgment of the developers. This statistical measure represents how often the maximum daily load is expected/allowed to be exceeded. The primary options for selecting this level of protection would be:

1. **The maximum daily load reflects some central tendency:** In this option, the maximum daily load is based upon the mean or median value of the range of loads expected to occur. The variability in the actual loads is not addressed.
2. **The maximum daily load reflects a level of protection implicitly provided by the selection of some "critical" period**: In this option, the maximum daily load is based upon the allowable load that is predicted to occur during some critical period examined during the analysis. The developer does not explicitly specify the probability of occurrence.
3. **The maximum daily load is a value that will be exceeded with a pre-defined probability:** In this option, a "reasonable" upper bound percentile is selected for the maximum daily load based upon a characterization of the variability of daily loads. For example, selection of the 95th percentile value would result in a maximum daily load that would be exceeded 5% of the time.

Selected Approach

The approach selected for defining a Lower Monocacy River Maximum Daily Load was based upon the specific data that exists for each source category. The approach consists of unique methods for each of the following categories of sources:

- Approach for Nonpoint Sources and Stormwater Point Sources within the Lower Monocacy River watershed
- Approach for Process Water Point Sources within the Lower Monocacy River watershed
- Approach for upstream sources.

<u>Approach for Nonpoint Sources and Stormwater Point Sources within the Lower Monocacy River watershed</u>

The level of resolution selected for defining a Lower Monocacy River Maximum Daily Load was a representative daily load, expressed as a single daily load for each source. This approach was chosen based upon the specific data that exists for nonpoint sources and stormwater point sources within the Lower Monocacy River watershed. Currently, the best available data is the CBP P5 model daily time series calibrated to long-term average annual loads (per land use). The CBP reach simulation results are calibrated to daily monitoring information for watershed segments with a flow typically greater than 100 cfs, but they have not been through appropriate peer review. Therefore, it was concluded that it would not be appropriate to apply the absolute values of the reach simulation model results to the TMDL, and the annual loads were used instead. However, it was assumed that the distribution of the daily values was correct, in order to calculate a normalized statistical parameter to estimate the maximum daily loads.

The maximum daily load was estimated based on three factors: a specified probability level, the average annual sediment TMDL, and the coefficient of variation (CV) of the CBP P5 Lower Monocacy River reach simulation daily loads. The probability level (or exceedance frequency) is based upon guidance from EPA (US EPA 1991) where examples suggest that when converting from a long-term average to a daily value, the z-score corresponding to the 99th percentile of the log-normal probability distribution should be used.

The CBP P5 Lower Monocacy River reach simulation consisted of a daily time series beginning in 1985 and extending to the year 2005. The CV was estimated by first converting the daily sediment load values to a log distribution and then verifying that the results approximated the normal distribution (see Figure B-1). Next the CV was calculated using the arithmetic mean and standard deviation results from the log transformation. The log-transformed values were used to reduce the possible influence of outliers. The resulting CV of 6.47 was calculated using the following equation:

$$CV = \frac{b}{a} \qquad \text{(Equation C.1)}$$

where:
CV = coefficient of variation
$b = a\sqrt{e^{s^2} - 1}$
$a = e^{(m+0.5*s^2)}$
a = mean (arithmetic)
ß = standard deviation (arithmetic)
µ= mean of logarithms
s=standard deviation of logarithms

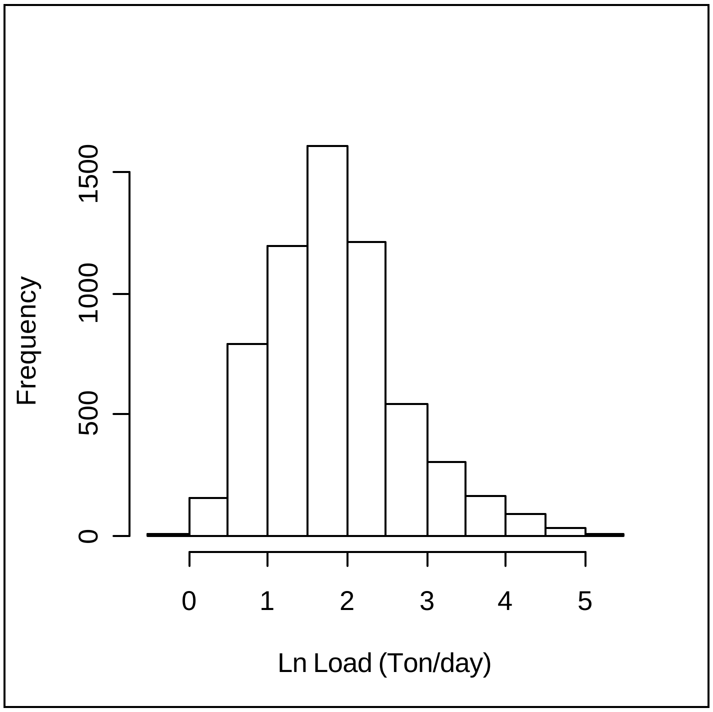


Figure C-1: Histogram of CBP river segment daily simulation results for the Lower Monocacy River Watershed

The maximum "daily" load for each contributing source is estimated as the long-term average annual load multiplied by a factor that accounts for expected variability of daily loading values. The equation is as follows:

$$MDL = LTA * e^{(zs - 0.5s^2)} \qquad \text{(Equation C.2)}$$

where:
MDL = Maximum daily load
LTA = Long term average (average annual load)
Z = z-score associated with target probability level
s = $\ln(CV^2+1)$
CV = Coefficient of variation based on arithmetic mean and standard deviation

Using a z-score associated with the 99th percent probability, a CV of 6.47, and consistent units, the resulting dimensionless conversion factor from long term average loads to a maximum daily value is 13.88. The average annual Lower Monocacy River TMDL of sediment/TSS is reported in ton/year and the conversion from tons/year to a maximum daily load in tons/day is 0.038 (e.g. 13.88/365).

<u>Approach for Process Water Point Sources within the Lower Monocacy River watershed</u>

The TMDL also considers contributions from other point sources (i.e., sources other than stormwater point sources) in the watershed that have NPDES permits with sediment limits. As these sources are generally minor contributors to the overall sediment load, the TMDL analysis that defined the average annual TMDL did not propose any reductions for these sources and held each of them constant at their existing technology-based NPDES permit monthly (or daily if monthly was not specified) limit for the entire year.

The approach used to determine maximum daily loads for these sources was dependent upon whether a maximum daily load was specified within the permit. If a maximum daily limit was specified, then the reported average flow was multiplied by the daily maximum limit to obtain a maximum daily load. If a maximum daily limit was not specified, the maximum daily loads were calculated based on the guidance provided in the Technical Support Document (TSD) for Water Quality-based Toxics Control (US EPA 1991). The long-term average annual TMDL was converted to maximum daily limits using Table 5-2 of the TSD assuming a coefficient of variation of 0.6 and a 99th percentile probability. This results in a dimensionless multiplication factor of 3.11. The average annual Lower Monocacy River TMDL of sediment/TSS is reported in ton/yr, and the conversion from ton/yr to a maximum daily load in ton/day is 0.0085 (e.g. 3.11/365).

<u>Approach for Upstream Sources</u>

For the purpose of this analysis two direct upstream watersheds have been identified: the Upper Monocay River watershed and the Lake Linganore watershed. The Upper Monocacy River Maximum Daily Load is presented in a separate TMDL document and subsequently applied in this analysis (MDE 2008a). As the Lake Linganore 2003 Sediment TMDL does not specify an MDL, the Lake Linganore Upstream Maximum Daily Load included in this analysis is calculated based on 1) the same approach that is used for nonpoint sources and NPDES regulated stormwater point sources within the Lower Monocacy River watershed and 2) the 2003 average annual Lake Linganore Sediment TMDL.

Results of Approach

This section lists the results of the selected approach to define the Lower Monocacy River Maximum Daily Loads.

- Calculation Approach for Nonpoint Sources and Stormwater Point Sources within the Lower Monocacy River watershed

LA_{LM} (ton/day) = Average Annual TMDL LA_{LM} (ton/yr) * .038

NPDES Stormwater WLA_{LM} (ton/day) = Average Annual TMDL NPDES Stormwater WLA_{LM} (ton/yr) * .038

- Calculation Approach for Process Water Point Sources within the Lower Monocacy River watershed

    - For permits with a daily maximum limit:

Process Water WLA_{LM} (ton/day) = Permit flow (mgd) * Daily maximum permit limit(mg/l) * 0.0042

    - For permits without a daily maximum limit:

Process Water WLA_{LM} (ton/day) = Average Annual TMDL WLA Process Water WLA_{LM} (ton/yr)* 0.0085

- Calculation Approach for Upstream Sources
    - For Lake Linganore Upstream Sources

      LA_{LL} (ton/day) = Average Annual TMDL LA_{LL} (ton/yr) * .038
    - For Upper Monocacy River Upstream Sources

      For Upper Monocacy River watershed MDL calculation please refer to the "Total Maximum Daily Load of Sediment in the Upper Monocacy River Watershed, Frederick and Carroll Counties, Maryland" (MDE 2008a).

Table C-1: Lower Monocacy River Maximum Daily Load of Sediment/TSS (ton/day)

MDL (ton/day)	=	LA					+	WLA			+	MOS
		LA_{LL}[1]	+	LA_{UM}[2]	+	LA_{LM}		NPDES Stormwater WLA_{LM}	+	Process Water WLA_{LM}		
2,416.7		268.8		1,547.4		471.1		123.8		5.7	+	Implicit
		Upstream Load Allocations[3,4]				Lower Monocacy River Watershed TMDL Contribution						

Notes: [1] An MDL is not calculated within the 2003 Lake Linganore Sediment TMDL. Thus, this MDL was established based off the average annual TMDL specified in the 2003 Lake Linganore Sediment TMDL document via the methods described in Appendix C.

[2] For Upper Monocacy River watershed MDL WLA and LA characterization, please refer to the "Total Maximum Daily Load of Sediment in the Upper Monocacy River Watershed, Frederick and Carroll Counties, Maryland" (MDE 2008a).

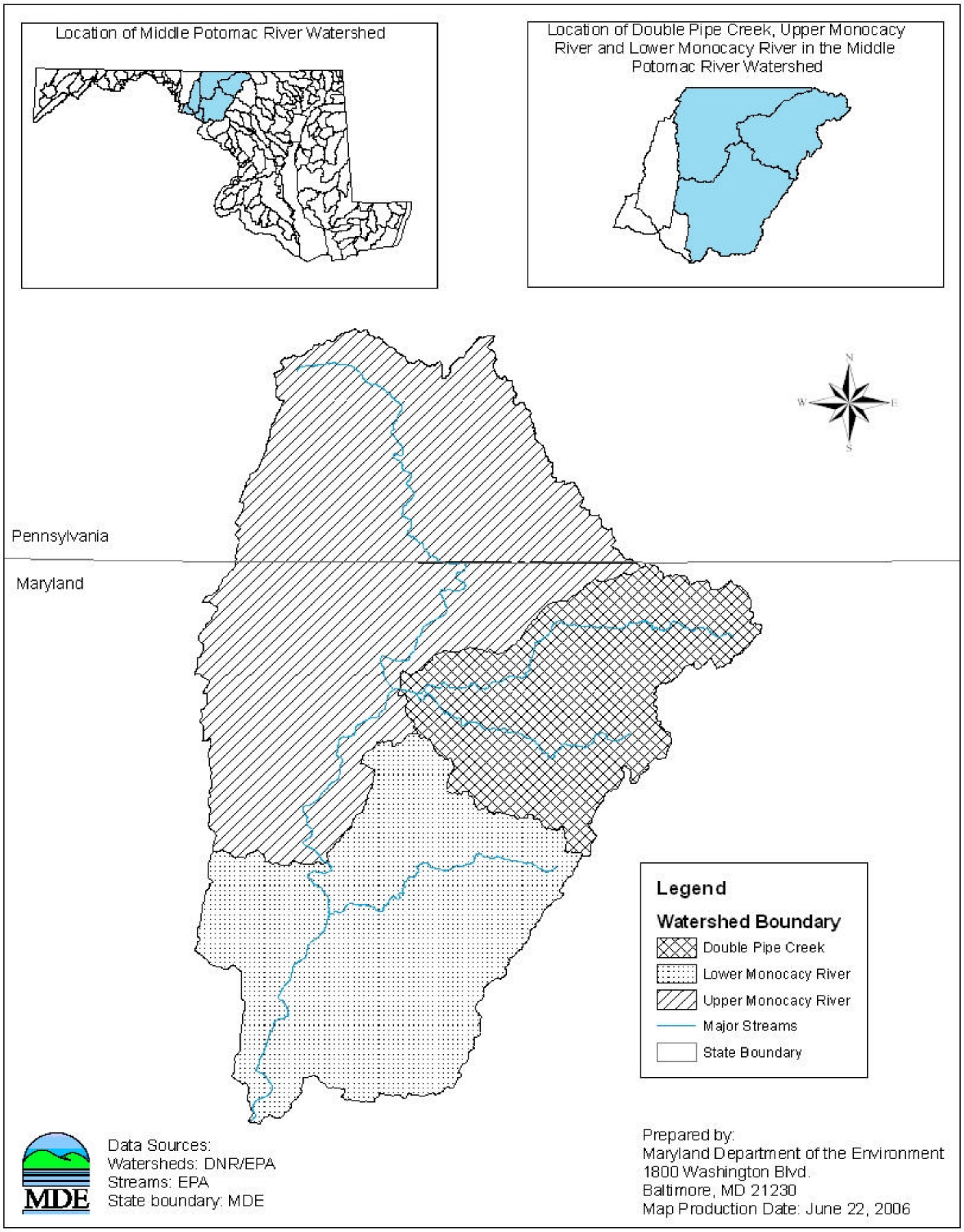
[3] Although for the purpose of this analysis the upstream loads are referred to as an LA, they could include loads from point and nonpoint sources.

[4] A delivery factor of 1 was used for all of the Upstream Load Allocations.

APPENDIX D – Sediment TMDLs for the Double Pipe Creek, MD 8-Digit Upper Monocacy River, and Lower Monocacy River Watersheds

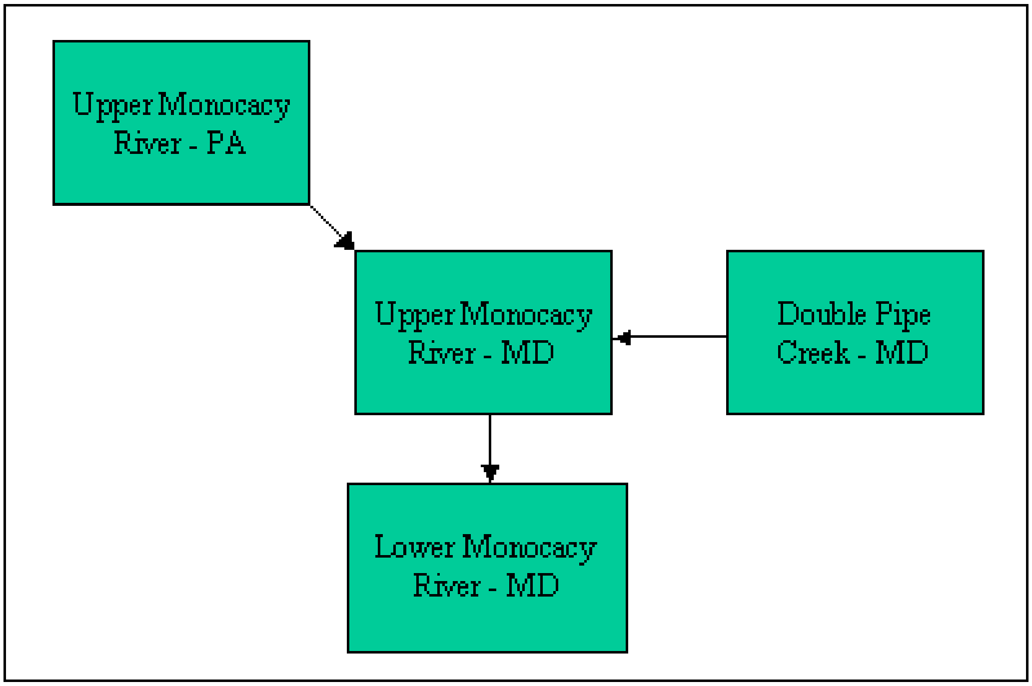
The purpose of this appendix is to explain the hydrologic relationship between the Double Pipe Creek, Upper Monocacy River, and Lower Monocacy River watersheds and how this affects the sediment TMDLs for each of the respective watersheds. As illustrated in Figure D-1, the three watersheds are hydrologically connected, beginning with the Double Pipe Creek watershed to the east. The Double Pipe Creek watershed flows into the Upper Monocacy River watershed, near the town of Rocky Ridge. It is also shown in Figure D-1 that the Upper Monocacy River watershed includes land in Pennsylvania and Maryland. The combined flow from the Upper Monocacy River and the Double Pipe Creek flows into the Lower Monocacy River. The hydrologic connectivity of the watersheds is illustrated in Figure D-2.

The baseline sediment loads for the watersheds are shown in Table D-1 through D-4. The TMDL calculations are shown in Tables D-4 through D-6. Further information can be found in the individual TMDL documents for each watershed (MDE 2008a,b).



Note: A separate sediment TMDL has been developed for Lake Linganore, a subwatershed within Lower Monaocay River watershed (MDE 2003), and is presented as an upstream load within the Lower Monocacy River TMDL.

Figure D-1: Location of the Double Pipe Creek, Upper Monocacy River, and Lower Monocacy River Watersheds



Note: A separate sediment TMDL has been developed for Lake Linganore, a subwatershed within the Lower Monaocay River watershed (MDE 2003), and is presented as an upstream load within the Lower Monocacy River TMDL.

Figure D-2: Flow Schematic of the Double Pipe Creek, Upper Monocacy River, and Lower Monocacy River Watersheds

Table D-1: Double Pipe Creek Baseline Sediment Loads (ton/yr)

Total Baseline Load (ton/yr)	=	Nonpoint Source BL_{DP}	+	NPDES Stormwater BL_{DP}	+	Process Water BL_{DP}
35,224.3	=	29,674.5	+	5,189.8	+	360.0

Table D-2: MD 8-digit Upper Monocacy River Baseline Sediment Loads (ton/yr)

		Upstream Baseline Load[1]				MD 8-digit Upper Monocacy River Watershed Baseline Load Contribution				
Total Baseline Load (ton/yr)	=	BL_{PA}	+	BL_{DP}[2]	+	Nonpoint Source BL_{UM}	+	NPDES Stormwater BL_{UM}	+	Process Water BL_{UM}
98,725.7	=	20,511.9	+	35,224.3	+	38,679.3	+	4,129.1	+	181.1

Notes:[1] Although the upstream values are reported as single values, they could include point and nonpoint sources.

[2] For Double Pipe Creek watershed point and nonpoint source characterization please refer to "Total Maximum Daily Load of Sediment in the Double Pipe Creek Watershed, Frederick and Carroll Counties, Maryland" (MDE 2008b).

Table D-3: Lower Monocacy River Baseline Sediment Loads (ton/yr)

		Upstream Baseline Load[1]				Lower Monocacy River Watershed Baseline Load Contribution				
Total Baseline Load (ton/yr)	=	BL_{LL}[2]	+	BL_{UM}[3]	+	Nonpoint Source BL_{LM}	+	NPDES Stormwater BL_{LM}	+	Process Water BL_{LM}
146,420.0	=	11,585.0	+	98,725.7	+	27,073.4	+	8,312.5	+	723.4

Notes: [1] Although the upstream values are reported as a single value, they include point and nonpoint sources.

[2] For the Lake Linganore watershed point and nonpoint source characterization, please refer to the "Total Maximum Daily Load of Phosphorus and Sediments for Lake Linganore, Frederick County, Maryland" (MDE 2003).

[3] For the Upper Monocacy River watershed point and nonpoint source characterization, please refer to the "Total Maximum Daily Load of Sediment in the Upper Monocacy River Watershed, Frederick and Carroll Counties, Maryland" (MDE 2008a).

Table D-4: Double Pipe Creek Average Annual TMDL (ton/yr)

TMDL (ton/yr) =	LA_{DP} +	NPDES Stormwater WLA_{DP} +	Process Water WLA_{DP} +	MOS
24,199.1	20,461.1	3,377.9	360.0	Implicit

Table D-5: Upper Monocacy River Average Annual TMDL (ton/yr)

TMDL (ton/yr)	=	LA					+	WLA			+	MOS
		LA_{PA}[1]	+	LA_{DP}[2]	+	LA_{UM}		NPDES Stormwater WLA_{UM}	+	Process Water WLA_{UM}		
66,707.3	=	19,362.2	+	24,199.1	+	20,823.1	+	2,141.8	+	181.1	+	Implicit
		Upstream Load Allocation[3, 4]				MD 8-digit Upper Monocacy Watershed River TMDL Contribution						

Notes:[1] LA_{PA} was determined to be necessary in order to meet Maryland water quality standards within the Upper Monocacy River watershed.
[2] For Double Pipe Creek watershed WLA and LA characterization please refer to "Total Maximum Daily Load of Sediment in the Double Pipe Creek Watershed, Frederick and Carroll Counties, Maryland" (MDE 2008b).
[3] A delivery factor of 1 was used.
[4] Although for the purpose of this analysis upstream loads are referred to as LAs, they could include point and nonpoint sources.

Table D-6: Lower Monocacy River Average Annual TMDL (ton/yr)

TMDL (ton/yr)	=	LA					+	WLA			+	MOS
		LA_{LL}[1]	+	LA_{UM}[2]	+	LA_{LM}		NPDES Stormwater WLA_{LM}	+	Process Water WLA_{LM}		
90,158.0	=	7,073.0	+	66,707.3	+	12,397.5	+	3,256.8	+	723.4	+	Implicit
		Upstream Load Allocations[3,4]				Lower Monocacy River Watershed TMDL Contribution						

Notes:[1] For Lake Linganore watershed WLA and LA characterization, please refer to the "Total Maximum Daily Loads of Phosphorus and Sediments for Lake Linganore, Frederick County, MD" (MDE 2003).
[2] For Upper Monocacy River watershed WLA and LA characterization, please refer to the "Total Maximum Daily Load of Sediment in the Upper Monocacy River Watershed, Frederick and Carroll Counties, Maryland" (MDE 2008a).
[3] Although for the purpose of this analysis the upstream load is referred to as an LA, it could include loads from point and nonpoint sources.
[4] A delivery factor of 1 was used for all of the Upstream Load Allocations**.**

APPENDIX E – Summary and Evaluation of the Alternative Lake Linganore Sediment TMDL

INTRODUCTION

In 2003, the EPA approved the document *Total Maximum Daily Loads of Phosphorus and Sediments for Lake Linganore, Frederick County, MD.* Lake Linganore is located in the northeastern portion of the Lower Monocacy River watershed. It is an impoundment within the Eagle Head development, near the city of Frederick in Frederick County, Maryland. The impoundment is part of the Linganore Creek subwatershed, a tributary of the Lower Monocacy River (MDE 2003).

In 1996 Lake Linganore was identified as impaired by both phosphorus and sediments. The phosphorus listing was based on water quality data, whereas the basis for the sediment listing was not explicitly stated. It has been determined that the sediment listing was a best professional judgment determination based on land use analysis.

Maryland does not have a numeric standard that could serve as a TMDL endpoint for sediment TMDLs in impoundments. In the absence of an applicable numeric criterion, Maryland has adopted a pragmatic approach for developing TMDLs for sediment in impoundments. Given the propensity of phosphorus to bind to sediments, reductions in phosphorous loads are expected to result in sediment load reductions (i.e., 0.5:1 sediment to phosphorous ratio). Consequently, whenever a phosphorus TMDL is developed for an impoundment/reservoir with a sediment listing, the Department evaluates whether the TMDL will also result in sediment conditions that preserve impoundment/reservoir capacity, thereby meeting the sediment requirement for the waterbody's specific designated use.

The Lake Linganore TMDL for phosphorus was based on two widely accepted empirical methods: the Vollenweider Relationship and Carlson's Trophic State Index. The results of this analysis required a 90% reduction in phosphorus loads in order to attain water quality standards within the impoundment. The sediment TMDL for this report was calculated based on a 0.5:1 ratio of sediment reduction to phosphorus reduction. Therefore, the net sediment reduction associated with a 90% phosphorus reduction is equivalent to a 45% reduction (0.9*0.5 = 0.45). This reduction was determined to significantly extend the impoundment's capacity, thus meeting the sediment conditions protective of Lake Linganore's designated use (Use IV-P: Recreational Trout Waters and Public Water Supply).

The Lower Monocacy River watershed 1996 sediment listing refers to the entire MD 8-digit watershed, which inherently includes the Lake Linganore drainage basin. In order to maintain consistency with the 2003 Lake Linganore Sediment TMDL and to ensure that the 2003 Lake Linganore sediment TMDL is also protective of the tributary streams draining to the impoundment, the Lake Linganore watershed was analyzed separately applying the same analytical approach as was used to develop a TMDL protective of aquatic health within the remainder of the Lower Monocacy River watershed. Since this analysis indicated that the 2003 Lake Linganore sediment TMDL is more environmentally conservative than the alternative TMDL estimated within this appendix, the 2003 Lake Linganore sediment TMDL will be applied in the Lower Monocacy River TMDL analysis and will be presented as an upstream load.

SETTING AND WATER QUALITY DESCRIPTION

General Setting

Location

Lake Linganore is an impoundment located near the city of Frederick in Frederick County, Maryland (See Figure 1 of main report). The impoundment, which is owned by the Lake Linganore Association, lies on Linganore Creek, a tributary of the Lower Monocacy River. An earthen dam was installed in 1972 to create the lake for the purpose of water supply and for recreational use.

Geology/Soils

The watershed lies in the Piedmont physiographic province, and the soils immediately surrounding the lake are of the Manor-Linganore-Montalto association. The Montalto soils are deep, well drained, and fine textured while the Manor and Linganore soils are generally shallow to very shallow, excessively drained, immature, or skeletal. They form in material weathered from schistose, schist or phyllite, and igneous rocks. The outer watershed area is comprised of soils of the Duffield-Hagerstown association. These soils are well drained and developed from limestone (USDA 1960).

Land Use

Land Use Methodology

For a detailed description of the methodology used to assess the Lake Linganore watershed land use, please see Section 2.1.1 of the main report.

Lake Linganore Land Use Distribution

The land use distribution in the Lake Linganore watershed consists of nearly equal amounts of crop (31%), forest (31%), and urban (27%) land uses. Pasture (11%) makes up the remainder of the land use distribution. A land use map is provided in Figure 2 of the main report and a summary of the watershed land use areas is presented in Table E-1.

Table E-1: Land Use Percentage Distribution for the Lake Linganore Watershed

General Land Use	Detailed Land Use	Area (Acres)	Percent	Grouped Percent of Total
Crop	Animal Feeding Operations	26.4	N/A[1]	
	Hay	6,485.9	12.0	
	High Till	5,013.0	9.3	
	Low Till	5,138.5	9.5	
	Nursery	229.6	0.4	31.3
Extractive	Extractive	1.2	N/A[1]	N/A[1]
Forest	Forest	16,545.9	30.7	
	Harvested Forest	167.1	0.3	31.0
Pasture	Natural Grass	153.9	0.3	
	Pasture	5,803.9	10.8	
	Trampled Pasture	30.4	0.1	11.1
Urban	Urban: Barren	171.4	0.3	
	Urban: Imp	1,286.8	2.4	
	Urban: perv	12,872.8	23.9	26.6
	Total	53,926.8	100.0	100.0

Note: [1] Percentage of total land area is minimal.

Source Assessment

For a detailed description of the methodology used to estimate the current nonpoint and point source baseline loadings within the Lake Linganore watershed, please see Sections 2.2.1-2.2.3 of the main report.

Summary of Baseline Loads

Table E-2 summarizes the Lake Linganore baseline sediment loads, which are reported in ton/yr and presented in terms of nonpoint and point source loadings.

Table E-2: Lake Linganore Baseline Sediment Loads (ton/yr)

Total Baseline Load (ton/yr)	=	Nonpoint Source BL_{LL}	+	NPDES Stormwater BL_{LL}	+	Process Water BL_{LL}
21,767.9	=	18,776.0	+	2,989.6	+	2.3

Table E-3 presents a breakdown of baseline loads generated within the Lake Linganore watershed, detailing loads per land use. The majority of the sediment load is from crop land (74.9%). The next largest sediment sources are urban land (13.7%), pasture (6.2%), and forest (5.1%).

Table E-3: Detailed Baseline Sediment Budget Loads Generated Within the Lake Linganore Watershed

General Land Use	Description	Load (Ton/Yr)	Percent	Grouped Percent of Total
Crop	Animal Feeding Operations	64.7	0.3	
	Hay	2,706.1	12.4	
	High Till	8,024.7	36.9	
	Low Till	4,954.6	22.8	
	Nursery	563.1	2.6	74.9
Extractive	Extractive	2.6	N/A[1]	N/A[1]
Forest	Forest	1,020.1	4.7	
	Harvested Forest	96.0	0.4	5.1
Pasture	Natural Grass	37.1	0.2	
	Pasture	1,240.1	5.7	
	Trampled Pasture	66.9	0.3	6.2
Urban	Urban: Barren	393.0	1.8	
	Urban: Imp	1,070.1	4.9	
	Urban: perv	1,526.5	7.0	13.7
N/A	Process Load	2.3	N/A	N/A
	Total	21,767.9	100.0	100.0

Note: [1] Percentage of total sediment load is minimal.

Water Quality Characterization

For a detailed description of the MBSS data (i.e., the individual MBSS parameters used in this analysis and how these data were collected) used to assess the Lake Linganore watershed, please see Section 2.3 of the main report.

Lake Linganore Watershed MBSS Monitoring Stations

A total of 10 water quality monitoring stations were used to characterize the Lake Linganore watershed, all of which were biological/physical habitat monitoring stations from the MBSS program. The stations are presented in Figure 4 of the main report and listed in Table E-4. Observed values of the SSDI selected MBSS parameters along with total BIBI and FIBI scores for each monitoring station are presented in Table E-5.

Table E-4: Monitoring Stations in the Lake Linganore Watershed

Site Number	Sponsor	Site Type	Site Name	Latitude	Longitude
LMON-107-R-2003	MD DNR	MBSS	Bens Branch, unnamed tributary 1	39.419	-77.253
LMON-108-R-2003	MD DNR	MBSS	Weldon Creek	39.4742	-77.115
LMON-109-R-2003	MD DNR	MBSS	Talbot Branch, unnamed tributary 1	39.449	-77.152
LMON-113-R-2003	MD DNR	MBSS	South Fork Linganore Creek, unnamed tributary 1	39.4338	-77.117
LMON-118-R-2003	MD DNR	MBSS	Lake Linganore, unnamed tributary 1	39.3942	-77.302
LMON-123-R-2003	MD DNR	MBSS	Town Branch, unnamed tributary 1	39.4817	-77.262
LMON-127-R-2003	MD DNR	MBSS	Long Branch, unnamed tributary 1	39.394	-77.322
LMON-142-R-2003	MD DNR	MBSS	Linganore Lake, unnamed tributary	39.4212	-77.336
LMON-328-R-2003	MD DNR	MBSS	North Fork Linganore Creek	39.4627	-77.196
LMON-337-R-2003	MD DNR	MBSS	Bens Branch	39.4163	-77.286

Table E-5: Lake Linganore MBSS Data

Site	FIBI	BIBI	Epifaunal Substrate	Percent Embeddedness	Instream Habitat	Bank Stability	Benthic Tolerant Species
LMON-107-R-2003	3.67	2.5	16	30	16	14.5	5.29
LMON-108-R-2003	3.33	3.25	10	35	15	20	4.85
LMON-109-R-2003	4	2.5	17	25	16	17.67	5.46
LMON-113-R-2003	3.67	2.25	8	40	6	12.2	5.07
LMON-118-R-2003	3	2	5	55	7	14	5.88
LMON-123-R-2003	2	2.25	11	40	9	14.8	5
LMON-127-R-2003	NS	3.5	NS	NS	NS	NS	5.19
LMON-142-R-2003	1	2.5	6	20	6	16.2	2.83
LMON-328-R-2003	4.33	2.75	6	60	16	14.53	5.75
LMON-337-R-2003	4.67	2.75	13	35	16	8.8	5.32

Note: NS = No Sample

Water Quality Impairment

For a detailed description of the SSDI methodology used to determine whether or not aquatic health within the Lake Linagnore watershed is impacted by elevated sediment loads, please see Section 2.4 of the main report. This section thoroughly describes the MBSS parameters used to calculate the SSDI, why these parameters were chosen, and how they were combined/analyzed to calculate the SSDI.

The Lake Linganore watershed average BIBIs, FIBIs, and corresponding SSDIs are listed in Table E-6. The BIBIs and FIBIs indicate that the watershed is exhibiting a negative deviation from reference conditions. Both the benthic and fish based SSDIs indicate that sediment is a stressor to the aquatic community.

Table E-6: Lake Linganore IBI and SSDI Values

Site	BIBI	Benthic SSDI	FIBI	Fish SSDI
LMON-107-R-2003	2.5	3.5	3.67	4.33
LMON-108-R-2003	3.25	3.5	3.33	3.0
LMON-109-R-2003	2.5	3.5	4.0	5.0
LMON-113-R-2003	2.25	2.5	3.67	1.67
LMON-118-R-2003	2.0	1.5	3.0	1.0
LMON-123-R-2003	2.25	3.0	2.0	2.33
LMON-127-R-2003	3.5	3.0	NS	NS
LMON-142-R-2003	2.5	3.5	1.0	2.33
LMON-328-R-2003	2.75	1.5	4.33	2.33
LMON-337-R-2003	2.75	2.0	4.67	3.67
Average	**2.63 ± 0.24**	**2.70 ± 0.41**	**3.30 ± 0.64**	**2.85 ± 0.70**

Note: NS = No Sample

TOTAL MAXIMUM DAILY LOADS AND SOURCE ALLOCATION

For a detailed description regarding the general methodology used to calculate the alternative Lake Linganore sediment TMDL, please refer to Sections 4.1-4.4 and Section 4.7 within the main report. These sections thoroughly describe the following components of the alternative Lake Linganore sediment TMDL analysis: the CBP PV watershed model, the reference watershed approach, the forest normalized sediment load, the sediment loading threshold and its calculation, the formula for calculating the TMDL, and the incorporation of critical conditions, seasonality, and a margin of safety.

TMDL Loading Caps

The average annual alternative Lake Linganore TMDL of TSS is considered the maximum allowable long-term average annual load the watershed can receive and still meet water quality standards. The alternative Lake Linganore sediment TMDL was set at a load 3.3 times the all forested condition. In order to arrive at the TMDL, equal reductions were applied to the predominant controllable sources (i.e., significant contributors of sediment to the stream system) in the TMDL analysis segment. This approach aims to achieve water quality standards in the most effective, efficient, and equitable manner. Predominant sources typically include urban land, high till crops, low till crops, hay, pasture, and harvested forest, but additional sources might need to be controlled in order to ensure that the water quality standards are attained. The Lake Linganore watershed baseline load and alternative Lake Linganore sediment TMDL are presented in Table E-7.

Table E-7: Lake Linganore Watershed Sediment Baseline Load and Alternative Lake Linganore Sediment TMDL

Baseline Load (ton/yr)	Alternative TMDL (ton/yr)	Reduction (%)
21,767.9	11,133.6	48.8

Load Allocations Between Point and Nonpoint Sources

Table E-8 summarizes the alternative Lake Linganore sediment TMDL results derived by applying the reductions equally to the predominant controllable sediment sources. The source categories in the table represent aggregates of multiple sources (e.g. crop source is an aggregate of high till, low till, hay, animal feeding operations, and nursery sources). The alternative Lake Linganore sediment TMDL of 11,133.6 ton/year is equivalent to a 48.8% overall reduction.

Table E-8: Alternative Lake Linganore Sediment TMDL Reductions by Source Category

Baseline Load Source Categories		Baseline Load (ton/yr)	TMDL Components	TMDL (ton/yr)	Reduction (%)
Nonpoint Source	Crop	16,313.2	LA	7,875.4	51.7
	Extractive	2.6		2.6	0.0
	Forest	1,116.1		1,116.1	0.0
	Pasture	1,344.1		700.1	47.9
Point Source	Urban	2,989.6	WLA	1,437.1	51.9
	Permits	2.3		2.3	0.0
Total		**21,767.9**		**11,133.6**	**48.8**

Summary of Alternative Lake Linganore Sediment Total Maximum Daily Loads

The average annual alternative Lake Linganore sediment TMDL is summarized in Table E-9. The TMDL is the sum of the LA, NPDES Stormwater WLA, Process Water WLA, and MOS.

Table E-9: Average Annual Alternative Lake Linganore TMDL of Sediment/TSS Summary (ton/yr)

Alternative TMDL (ton/yr)	=	Nonpoint Source BL_{LL}	+	NPDES Stormwater BL_{LL}	+	Process Water BL_{LL}	+	MOS
11,133.6	=	9,694.2	+	1,437.7	+	2.3	+	Implicit

COMPARISON

The analysis presented in this appendix indicates that the 2003 Lake Linganore sediment TMDL is more environmentally conservative than the alternative Lake Linganore sediment TMDL and is thus not only preserving the impoundment's capacity, but is also protective of the aquatic health within the tributary streams draining to the impoundment. Therefore, the 2003 Lake Linganore sediment TMDL will be applied in the Lower Monocacy River TMDL analysis and will be presented as an upstream load.

Table E-11 compares the 2003 Lake Linganore sediment TMDL to the alternative Lake Linganore sediment TMDL estimated in this appendix.

Table E-11: Comparison of the 2003 Lake Linganore Sediment TMDL to the Alternative Lake Linganore Sediment TMDL

2003 Lake Linganore Sediment TMDL (ton/yr)	Alternative Lake Linganore TMDL (ton/yr)
7,073.0	11,133.6