

Fiber Optic Communication  
Couplers and Connectors  
Lecture 17



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# Couplers and connectors

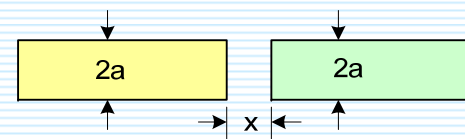
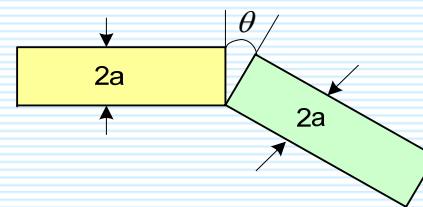
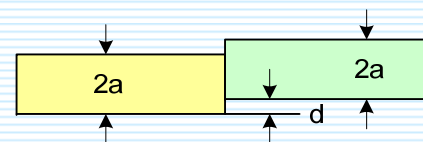
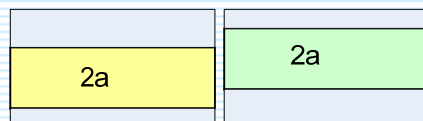
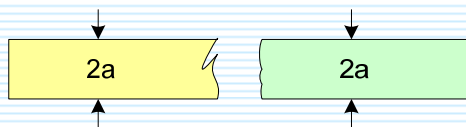
- Connectors:
  - Metallic system: Wire: Soldering: Lossless: Economical
  - Fiber system: fiber: Splicing: Loss: Economical
- Splicing is the permanent connection of two optical fiber.
- Two mechanism of splicing:
  - Fusion
  - Mechanical
- Splices are of two types:
  - Midspan: the connecting of two cables
  - Pigtail: assembly of a fiber that has been factory-installed into a connector in one end, with the other end free for splicing to a cable.
- The quality of splicing is measured by the insertion and reflection losses caused by the splice

# Couplers and connectors losses

- Connectors losses at any splice stem from the fact that not all light from one fiber is transmitted to another. The loss results from:
  - **Mismatch**: due to fiber's mechanical dimensions and numerical aperture. An improvement in splicing technique can not solve the problem. Also called **intrinsic connection losses**.
  - **Misalignment**: are caused by some imperfection in splicing, that theoretically can be eliminated. An improvement in splicing technique can solve the problem. Also called **extrinsic connection losses**.
- Misalignment Losses in fiber-to-fiber:
  - Core misalignment and imperfections.
  - Lateral (axial) misalignment
  - Angular misalignment
  - gap between ends contact
  - Non-flat ends
  - Cladding alignment

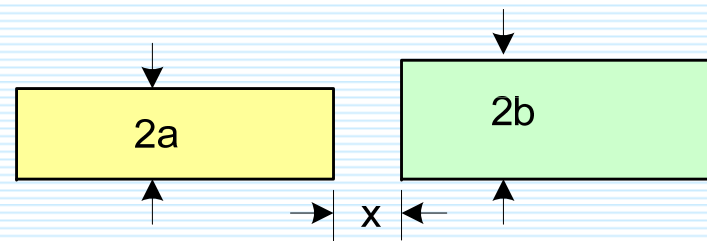
# Couplers and connectors losses

- Misalignment Losses in fiber-to-fiber due to some imperfection in splicing:
  - Core misalignment and imperfections.
  - Lateral (axial) misalignment
  - Angular misalignment
  - gap between ends contact
  - Non-flat ends due to cleaving
  - Cladding alignment



# Mismatch losses

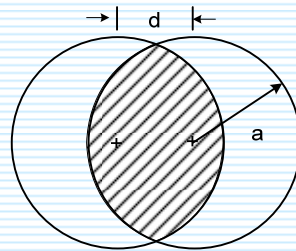
- Coupling efficiency reduction due to mismatch:
  - Different numerical aperture
  - Different core diameter
  - Elliptical cross sections (rather than Circular) with cross section are attached with their major axes unaligned.
  - The core is not centered in the cladding and the outside cladding is used as the reference for aligning the Joint.
  - The distance between the excitation point and the connector (due to unknown distribution of power across the fiber end face, excitation method)
  - Length of fiber following the Junctions.



- Reasonable loss of 0.1 dB for splices
- Reasonable loss of reusable connectors with losses less than 1 dB.

# Losses due to lateral misalignment

- Assumptions:
  - Uniform power distribution over the fiber core (suitable for multimode step index fiber).
  - The lateral misalignment loss is due only to the non-overlap of transmission and receiving cores.



- The coupling efficiency  $\eta$  is defined as the ratio of the overlapping area to the core area.

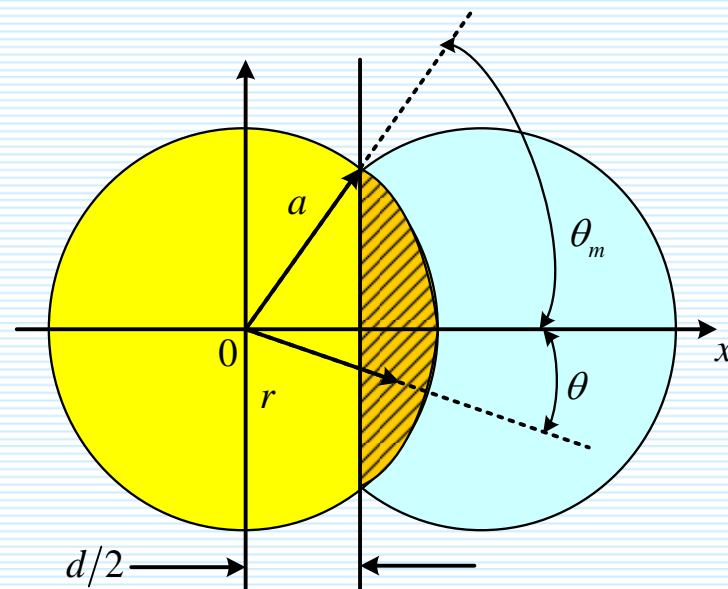
$$\eta = \frac{2}{\pi} \left\{ \cos^{-1} \frac{d}{2a} - \frac{d}{2a} \sqrt{1 - \left( \frac{d}{2a} \right)^2} \right\}$$

- The inversed cosine is calculated in radians. The loss in dB is:

$$L = -10 \log_{10} \eta$$

# Losses due to lateral misalignment

- Assumptions:
  - Uniform power distribution over the fiber core (suitable for multimode step index fiber).
  - The lateral misalignment loss is due only to the non-overlap of transmission and receiving cores.



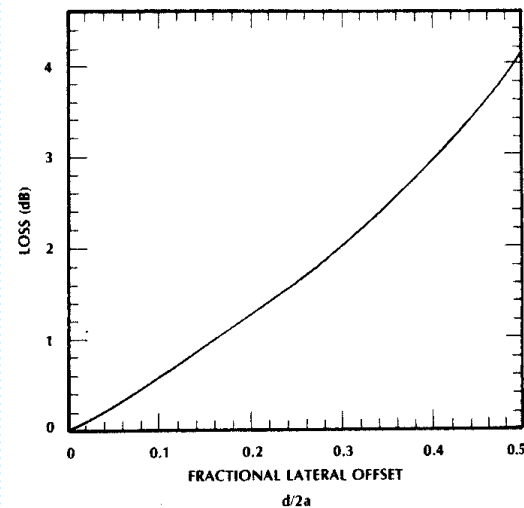
$$\cos \theta = \frac{d/2}{r}$$
$$\cos \theta_m = \frac{d/2}{a}$$
$$\theta_m = \cos^{-1} \frac{d/2}{a}$$

# Losses due to lateral misalignment

- The small displacements  $d/2a < 0.2$  the equation:

$$\eta = \frac{2}{\pi} \left\{ \cos^{-1} \frac{d}{2a} - \frac{d}{2a} \sqrt{1 - \left(\frac{d}{2a}\right)^2} \right\}$$

- Reduces to:  
$$\eta = 1 - \frac{2d}{\pi a}$$
- Lateral misalignment loss for a multimode SI fiber





# Axial displacement loss example

- A fiber has a core diameter of  $50\mu m$ .
  - 1) what is the allowable axial displacement if the coupling loss is to be less than 1 dB.
  - 2) Repeat for losses of 0.5 dB.
  - 3) Repeat for losses of 0.1 dB.

- Solution:

- The coupling efficiency

$$L = -10\log_{10}\eta \Rightarrow \eta = 10^{-\frac{L}{10}}$$

- The  $d/a$

$$\eta = \frac{2}{\pi} \left\{ \cos^{-1} \frac{d}{2a} - \frac{d}{2a} \sqrt{1 - \left(\frac{d}{2a}\right)^2} \right\}$$

- The displacement

# Axial displacement loss example

- A fiber has a core diameter of  $50\mu m$ .

$$L = -10\log_{10}\eta \Rightarrow \eta = 10^{-\frac{L}{10}}$$

- The displacement

$$\eta = \frac{2}{\pi} \left\{ \cos^{-1} \frac{d}{2a} - \frac{d}{2a} \sqrt{1 - \left(\frac{d}{2a}\right)^2} \right\}$$

Loss (dB)	$d / 2a$	$d (\mu m)$
1.0	0.16	8
0.5	0.09	4.5
0.1	0.02	1

# Losses due to lateral misalignment

- Higher-ordered modes are more heavily attenuated than lower modes.
- Higher-ordered modes contained more power near the core-cladding interface.
- The power density at the end of a long fiber will be lower at the edge of the core than at points near its center.
- For small axial displacements, only the edges of the transmitting core miss the receiving fiber but the edge contain less power than is assumed in

$$L = -10\log_{10} \eta$$

- The actual loss is less than that predicted by theory.

# Losses due to lateral misalignment

- Multimode Graded-index fiber (GRIN) numerical aperture varies across the face of the core.
- The numerical aperture has

$$NA = n_1 \sqrt{2\Delta} \sqrt{1 - \left(\frac{r}{a}\right)^2}$$

- The numerical apertures of transmitter and receiver match at every point within the core when the two fibers meet with no offset.
- With an offset, there is a NA mismatch at nearly every point.
- At those points where the receiver NA is larger than the transmitter NA, all the power is transferred.
- At those points where the receiver NA is less than the transmitter NA, some of the power is lost.

# Losses due to lateral misalignment

- The fractional efficiency at those points is equal to the ratio of square of the local numerical aperture.
- The coupling efficiency is the average of the local efficiencies weighted according to power distribution across the end face.
- The power distribution across the face is not generally known. This fact discourages comprehensive analysis.
- For both step index (SI) and parabolic-index fibers with the nearly Gaussian beam. The loss between identical fibers:

$$L = -10 \log_{10} e^{-\left(\frac{d}{w}\right)^2}$$

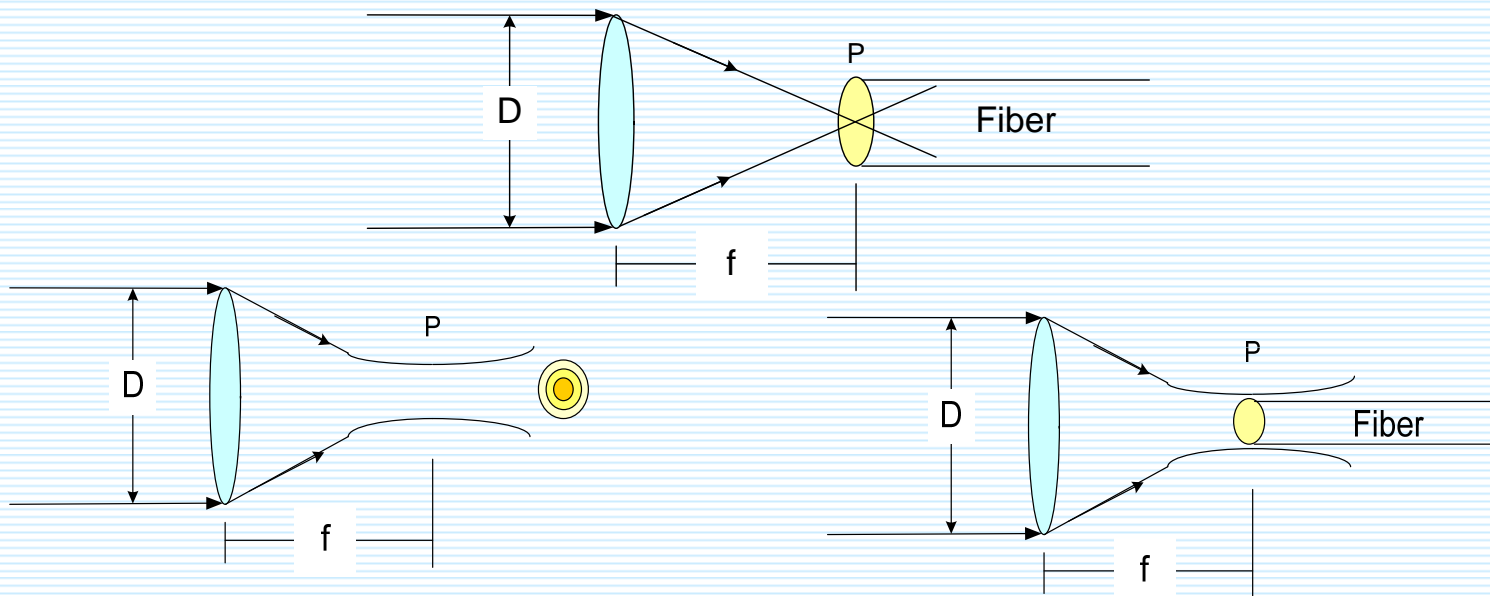
- Where  $W$  is the spot size.
- The spot size in the focal plane

$$W_0 = \frac{\lambda f}{\pi W}$$

# Physical optics (Diffraction theory) review

- Collimated uniform light beam does not converge to a point but instead reduces to a central spot of light surrounded by rings of a steadily diminishing intensity. The central spot has diameter.

$$d = 2.44\lambda f / D$$



# Diffraction theory review

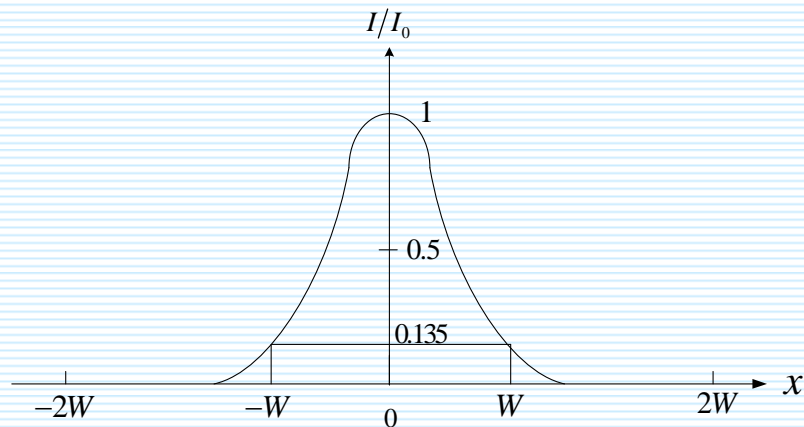
- Very small fibers (having diameters of a few micrometers) and actual light sources produces non-uniform beams. The intensities vary across the transverse plane. A transverse pattern is the Gaussian distribution.

- A Gaussian intensity distribution:

$$I = I_0 e^{-\frac{2x^2}{W^2}}$$

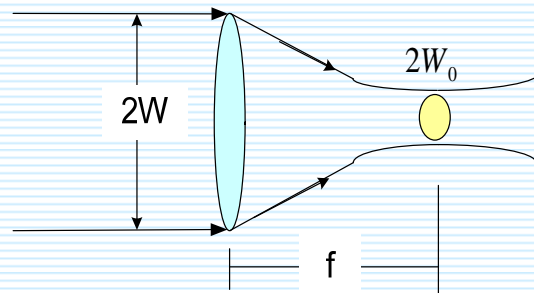
$$W_0 = \frac{\lambda f}{\pi W}$$

- A normalized Gaussian intensity distribution:



# Diffraction theory review

- The Gaussian beam spot pattern appears to be a circle of light. The edges of the circle are not sharp. The light intensity drops gradually from  $I_0$ , the maximum at the center.
- The radius of the spot is the distance at which the beam intensity has dropped to  $1/e^2 = 0.135$  times its peak value  $I_0$ . This radius is called the **spot size**.
- Focusing a Gaussian light with a lens yields distribution of light in the focal plane that is also Gaussian shaped. There are no surrounding rings like those that appear when focusing a uniform beam. The spot size in the focal plane is:

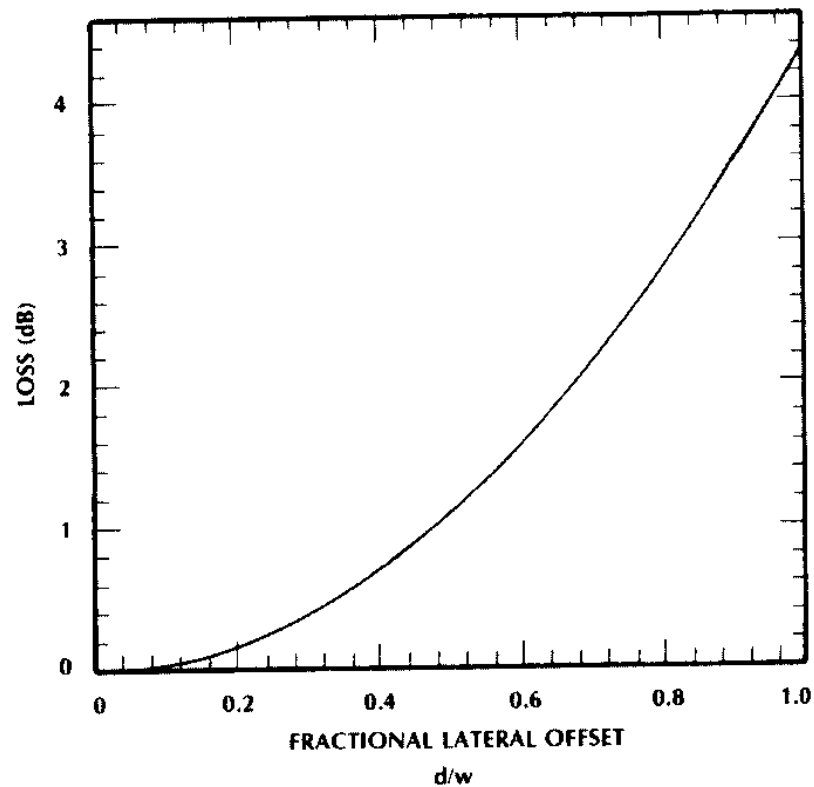


$$W_0 = \frac{\lambda f}{\pi W}$$



# Losses due to lateral misalignment

- The small displacements  $d/2a < 0.2$  the equation:



# Lateral misalignment loss example

- Consider the single-mode fiber core diameter of  $50\mu m$ . Plot the coupling loss as a function of lateral misalignment at the wavelengths  $1.3\mu m$  and  $1.55\mu m$ , Do this for offset from 0 to  $5\mu m$ .
- Solution: The  $V$  parameters must be calculated at two wavelengths of interest.

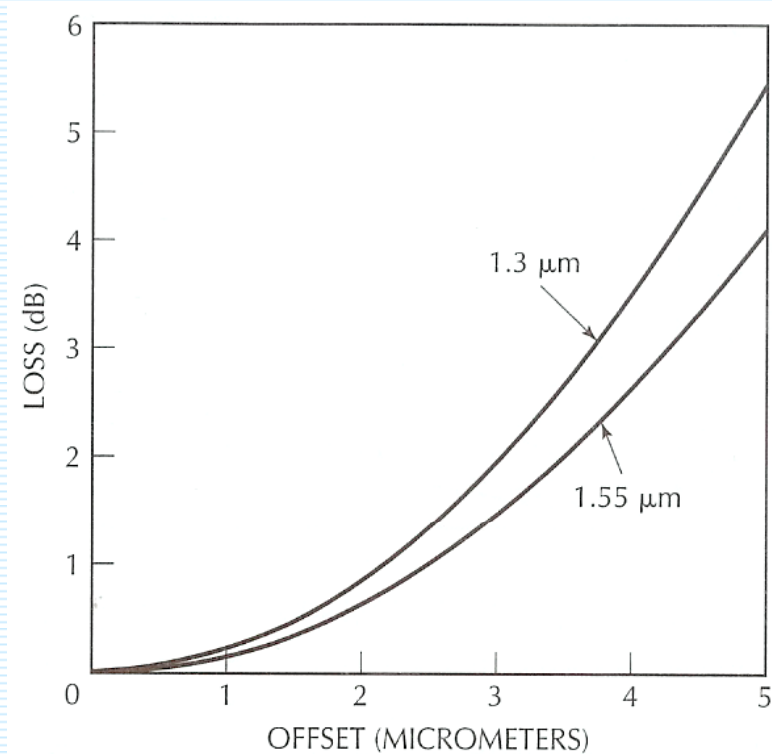
$$V = \frac{2\pi a}{\lambda} \sqrt{n_1^2 - n_2^2}$$

$$\frac{W}{a} = 0.65 + 1.619V^{-\frac{3}{2}} + 2.879V^{-6}$$

$\lambda(\mu m)$	$V$	$W/a$	$W(\mu m)$
1.3	2.31	1.13	4.47
1.55	1.94	1.3	5.16

# Lateral misalignment loss plot example

- Plot of the coupling loss as a function of lateral misalignment at the wavelengths  $1.3\mu m$  and  $1.55\mu m$



# Angular misalignment

- The coupling efficiency due to small angular misalignment of multimode SI fibers is:

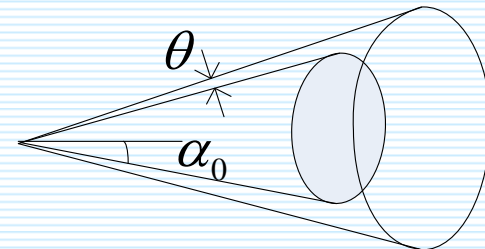
$$\eta = 1 - \frac{n_0 \theta}{\pi NA}$$

- Where  $n_0$  is the refractive index of the material filling the groove formed by the two fibers and  $\theta$  is the misalignment angle in radian. The loss is:

$$L = -10 \log_{10} \left( 1 - \frac{n_0 \theta}{\pi NA} \right)$$

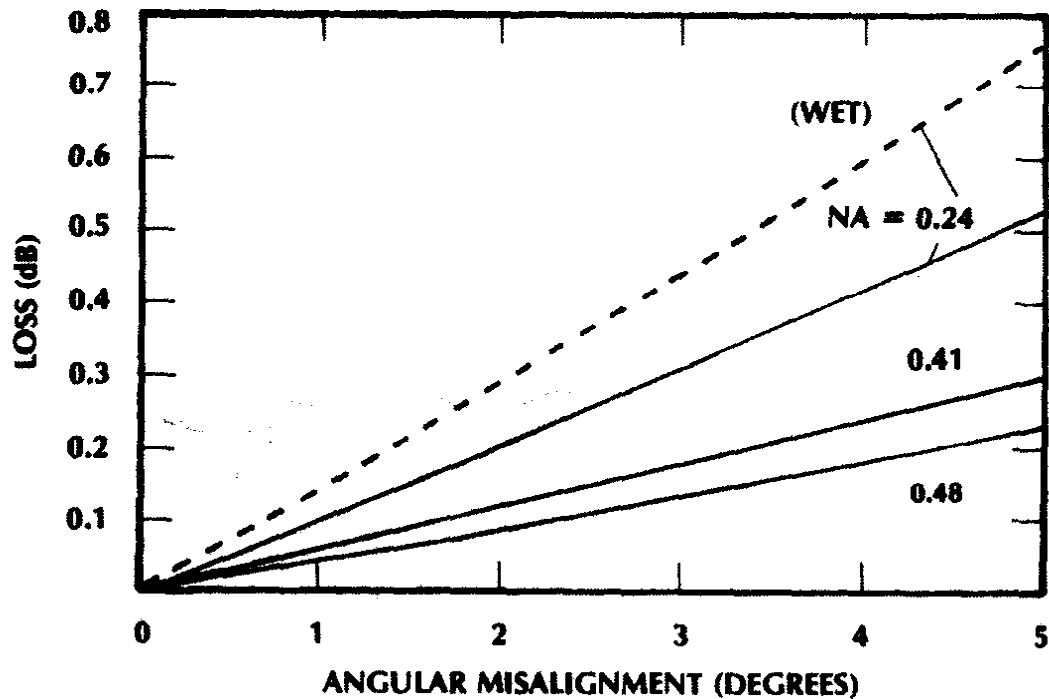
- The efficiency was found by computing the overlap of the transmitting and receiving cones, assuming uniform power distribution.

- Where  $\theta$  is tilt angle and  $NA = n_0 \sin \alpha_0$



# Angular misalignment plot

- Plot of the coupling efficiency due to small angular misalignment of **multimode SI fibers** per degree is:

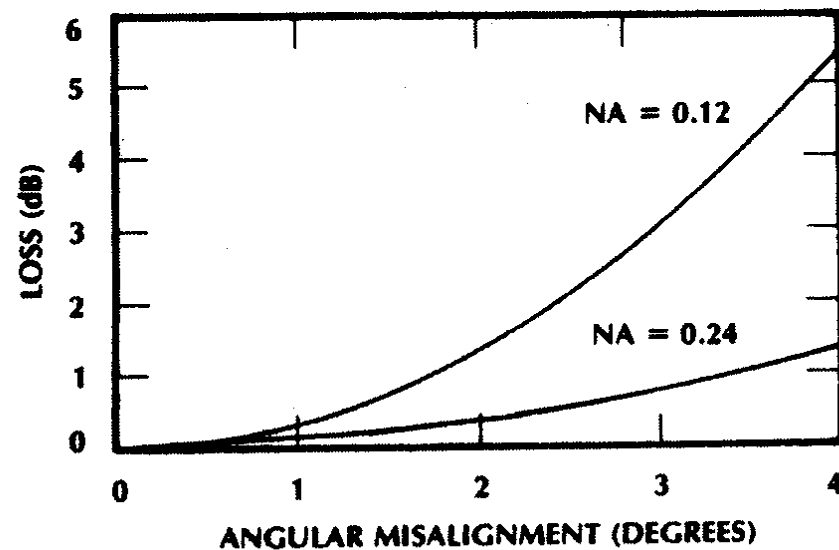


# Angular misalignment

- Angular misalignment losses for **single-mode fiber**:

$$L = -10 \log_{10} e^{-\left(\frac{\pi n_2 w \theta}{\lambda}\right)^2}$$

- The coupling efficiency due to small angular misalignment of single SI fibers is:



# example

- A SI fiber  $n_1 = 1.465, n_2 = 1.46$  and normalized frequency 2.4.
  - 1) Compute its numerical aperture and core radius at  $0.8\mu m$ .
  - 2) The spot size at  $0.8\mu m$ .

□ Solution:

- 1) the numerical aperture

$$NA = \sqrt{n_1^2 - n_2^2} = \sqrt{(1.465)^2 - (1.46)^2} = 0.12$$

$$V = \frac{2\pi a}{\lambda} \sqrt{n_1^2 - n_2^2} \Rightarrow a = \frac{\lambda V}{2\pi \sqrt{n_1^2 - n_2^2}} = \frac{0.8(2.4)}{2\pi(0.12)} = 2.53\mu m$$

- 2) The spot size at  $0.8\mu m$ .

$$\frac{w}{a} = 0.65 + 1.619V^{-\frac{3}{2}} + 2.879V^{-6} = 0.65 + 1.619(2.4)^{-\frac{3}{2}} + 2.879(2.4)^{-6} = 1.1$$

$$w = 1.1(2.53) = 2.78\mu m$$

# End separation loss

- Losses due to gap between the fibers being joined has two components:

- 1) Two boundaries between the fiber medium and air:

$$R = \left( \frac{n_1 - n_2}{n_1 + n_2} \right)^2 = \left( \frac{1 - 1.5}{1 + 1.5} \right)^2 = 0.04$$

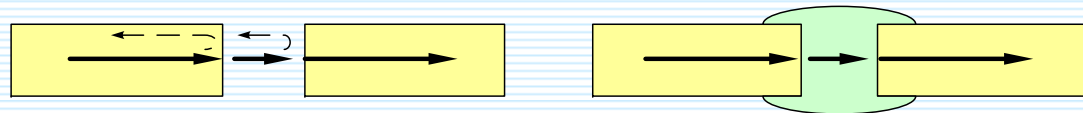
- 4% of light reflected. 96% transmitted. Loss in dB.

$$L = -10 \log_{10} 0.96 = 0.177 \text{ dB}$$

- The total loss

$$L = 2 \times 0.177 \text{ dB} = 0.35$$

- To improve the loss: fill the gap by the index-matching fluid.



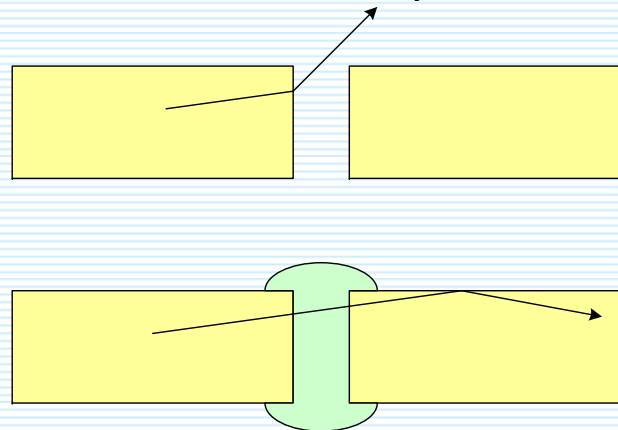


# End separation loss

- Losses due to gap between the fibers being joined has two components:
  - 2) some transmitted ray are not intercepted by receiving fiber:

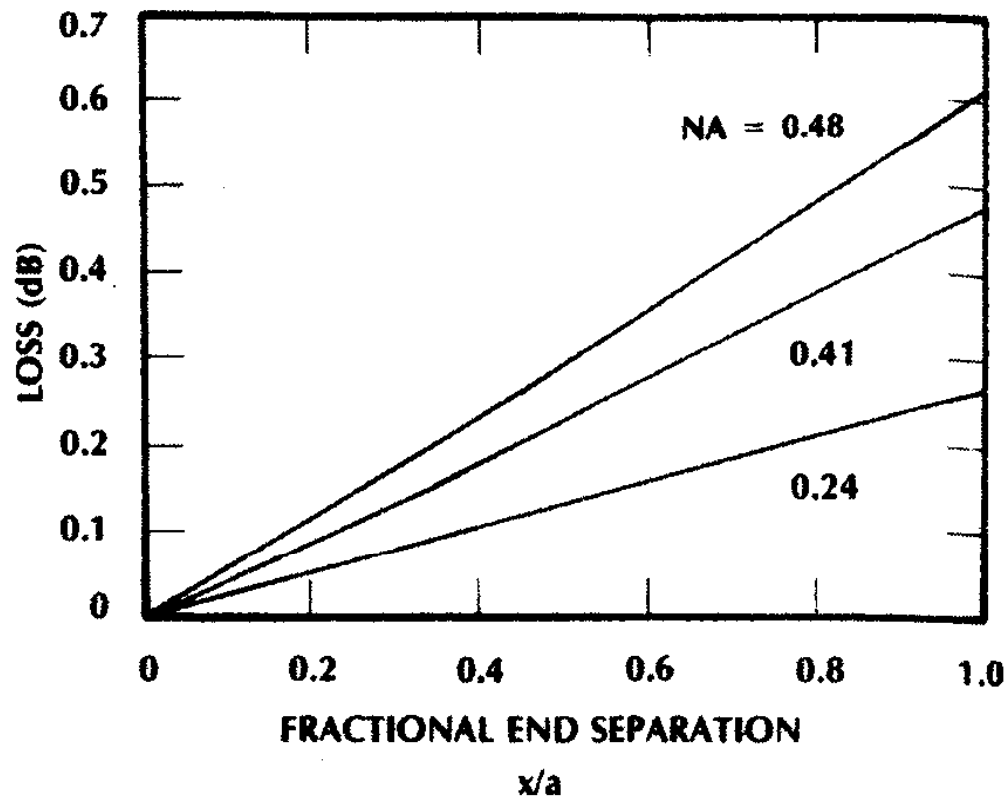
$$L = -10 \log_{10} \left( 1 - \frac{xNA}{4an_0} \right)$$

- Where  $n_0$  is the refractive index of matching fluid. An index-matching fluid decreases fiber-separation loss by reducing beam divergence



# End separation loss for multimode fiber

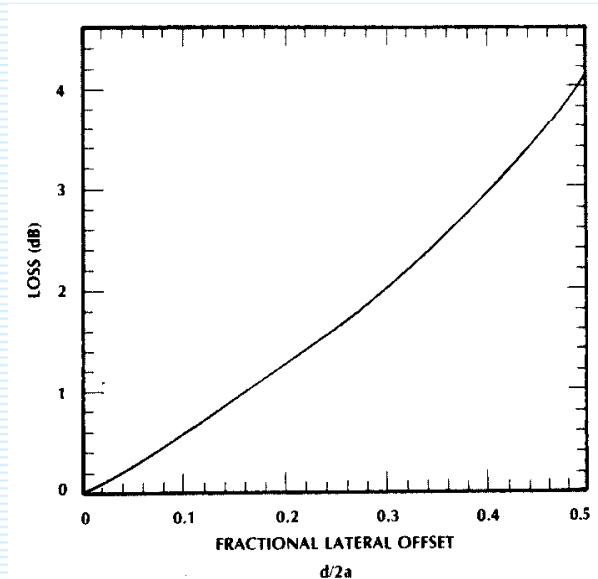
- End separation for a **multimode SI fiber**:  $L = -10 \log_{10} \left( 1 - \frac{xNA}{4an_0} \right)$



# Example

- Estimate the allowed misalignment for a multimode SI fiber if each type of error is allowed to contribute 0.25 dB of loss. The core radius is  $50\mu m$  and  $NA = 0.24$ 
  - 1) lateral offset:  $L=0.25$  from the figure  $d/2a=0.045$ .

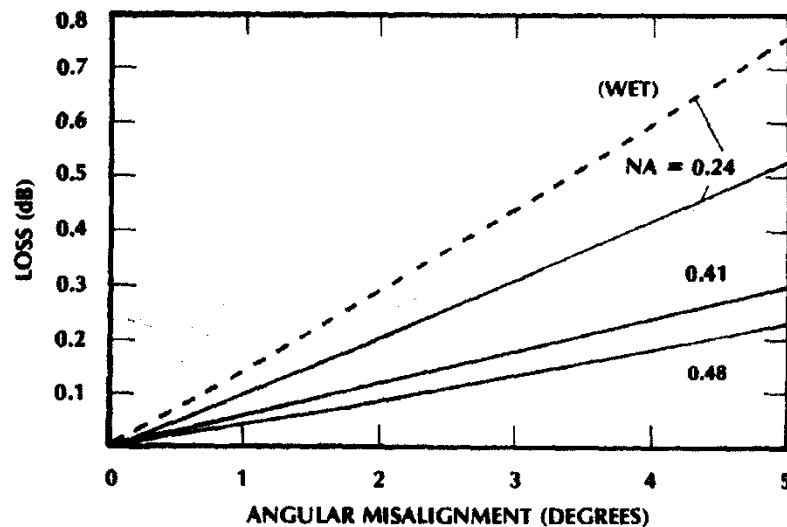
$$L = 0.045(2 \times 50\mu m) = 4.5\mu m$$



# Example

- Estimate the allowed misalignment for a multimode SI fiber if each type of error is allowed to contribute 0.25 dB of loss. The core radius is  $50\mu\text{m}$  and  $NA = 0.24$ 
  - 2) angular misalignment: from the figure, the angle is 2.4 degrees.

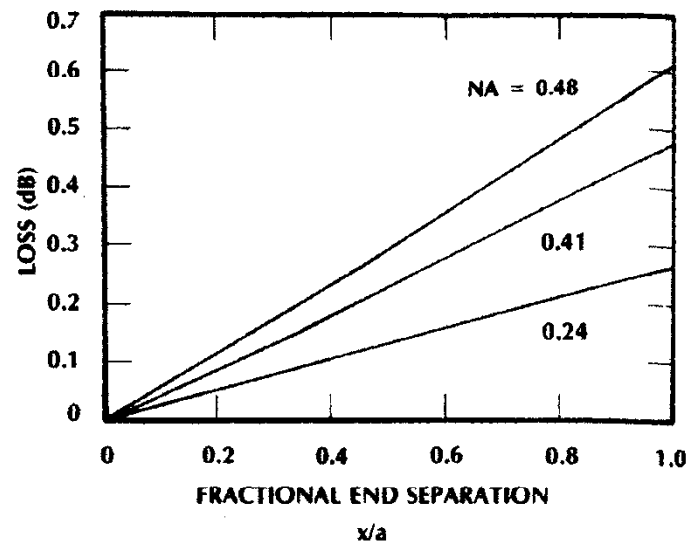
$$L = 0.045(2 \times 50\mu\text{m}) = 4.5\mu\text{m}$$



# Example

- Estimate the allowed misalignment for a multimode SI fiber if each type of error is allowed to contribute 0.25 dB of loss. The core radius is  $50\mu\text{m}$  and  $NA = 0.24$ 
  - 3) the end separation: from the figure, the  $x/a = 0.94$

$$x = 0.94a = 0.94(50\mu\text{m}) = 47\mu\text{m}$$



# The gap loss for single mode fibers

- The gap loss for single mode fibers:

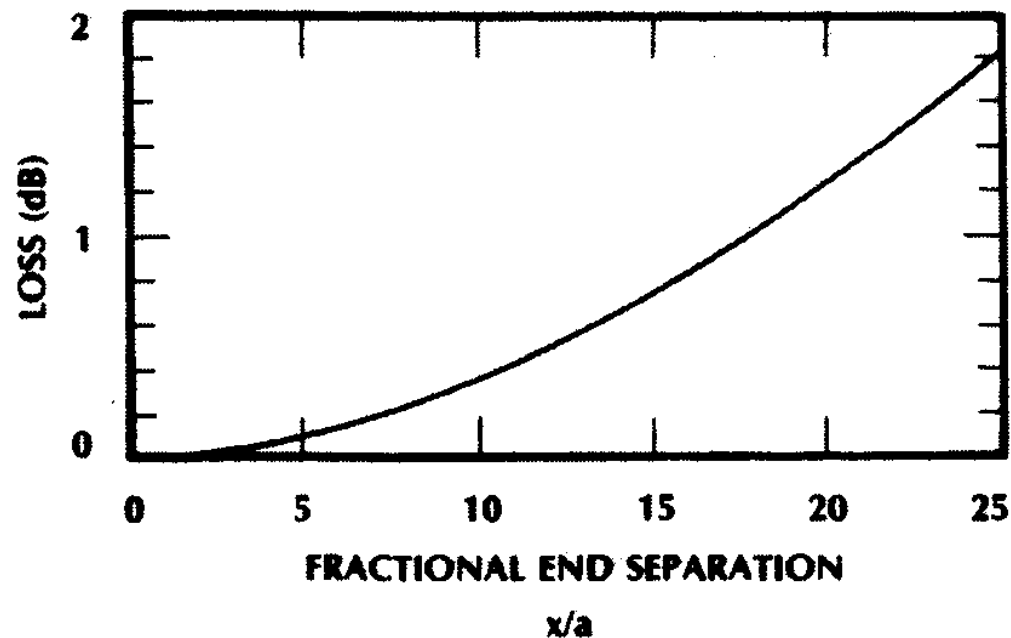
$$L = -10 \log_{10} \frac{4(4z^2 + 1)}{(4z^2 + 2) + 4z^2}$$

- Where  $z = \frac{x\lambda}{2\pi n_2 w^2}$

- From the next page figure the gap of 10 times of the core radius produces a loss than 0.4 dB.
- Axial misalignment is potentially the most serious problem in multimode SI fiber.

# Gap loss for single-mode fiber

- The gap loss for single-mode fiber is:



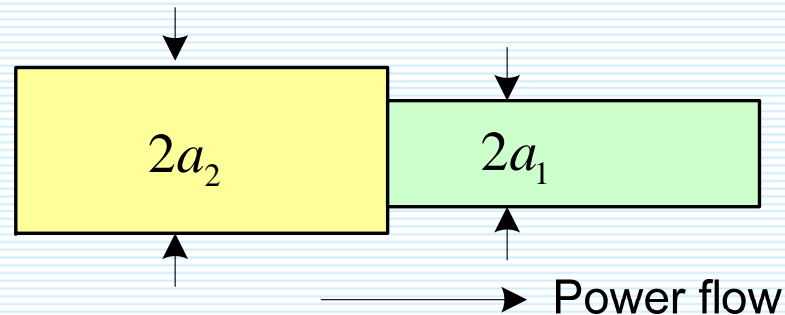
- End- separation loss for single mode SI fiber  $V=2.4$ ,  $w/a=1.1$ ,  $NA=0.12$  and  $\lambda = 0.8\mu m$

# Loss due to fiber core radius difference

- The loss transmitting from a fiber of core radius  $a_1$  to one having core radius  $a_2$  is:

$$L = -10 \log_{10} \left( \frac{a_2}{a_1} \right)^2$$

- Applicable for both SI and GRIN fibers. If all the allowed modes are equally excited
- If the receiving fiber core is larger than the transmitting one  $a_1 > a_2$  there is no loss.



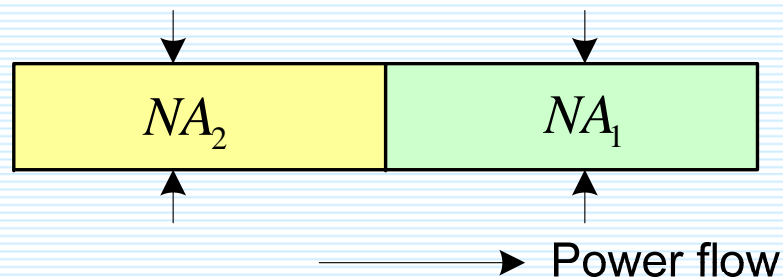


# Loss due to fiber core radius difference

- The loss transmitting from a fiber with a higher numerical aperture to lower one is:

$$L = -10 \log_{10} \left( \frac{NA_2}{NA_1} \right)^2$$

- Applicable for both multimode SI and GRIN fibers. If all the allowed modes are equally excited
- If the receiving fiber NA is larger than the transmitting one  $NA_1 > NA_2$  there is no loss.



# Reference

- Joseph C. Palais, *Fiber optic communication*. fifth edition, Pearson, Prentice Hall. 2005.