Aquifer Thermal Energy Storage in Germany

Peter Seibt & Frank Kabus

Geothermie Neubrandenburg GmbH www.gtn-online.de

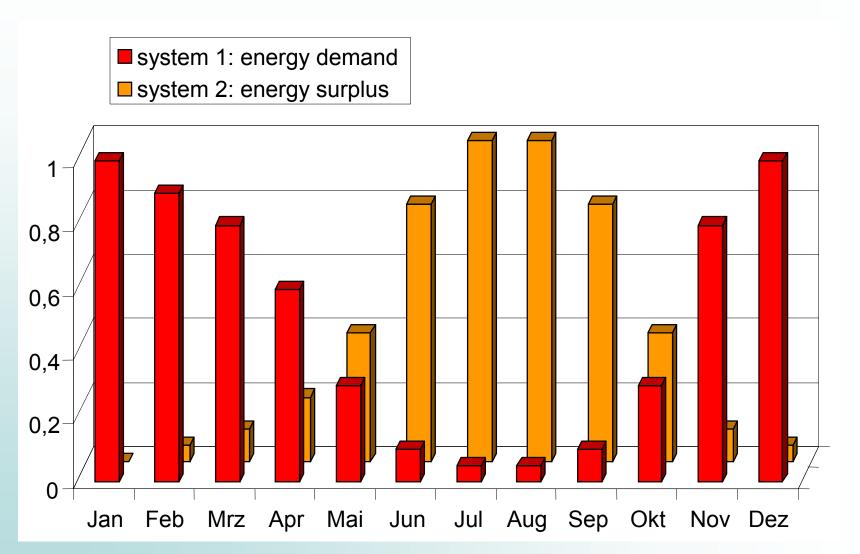


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 - Reichstag building / Berlin (seat of the German Parliament)

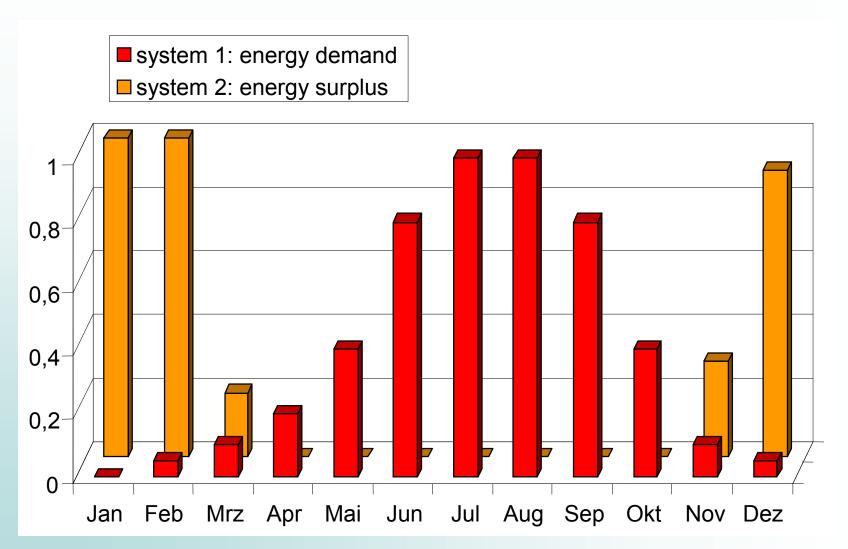


Demand / surplus scenarios



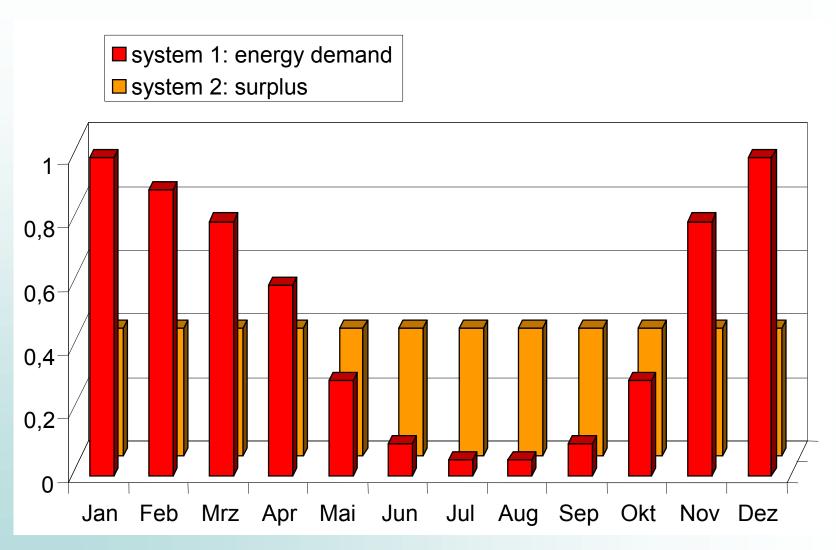


Demand / surplus scenarios





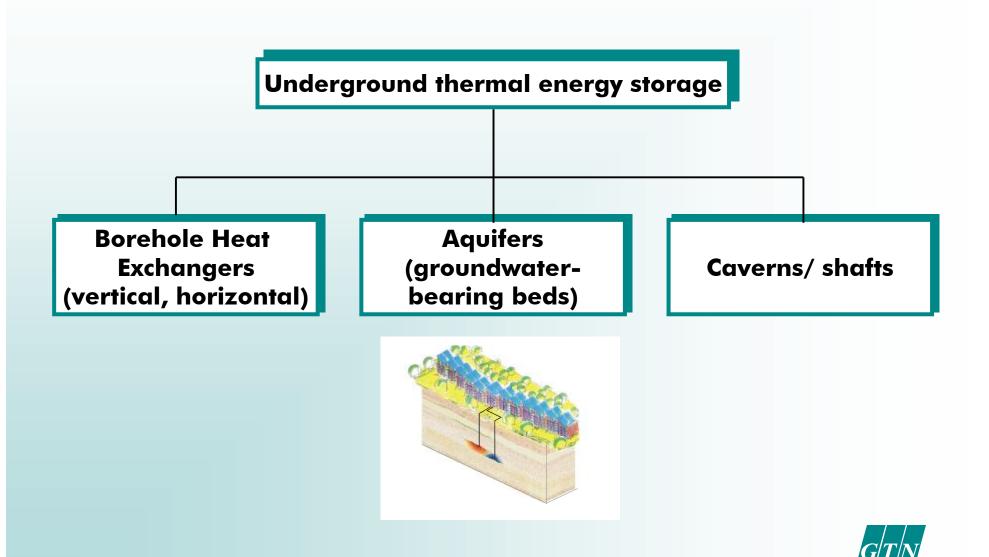
Demand / surplus scenarios



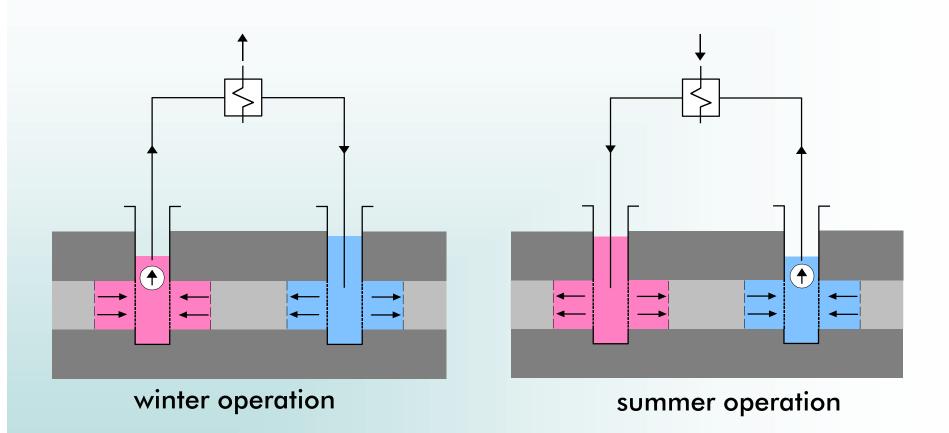
Heating / waste heat from power generation



Classification

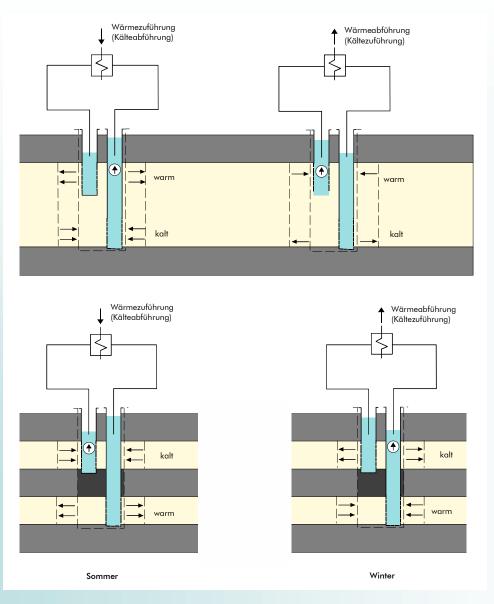


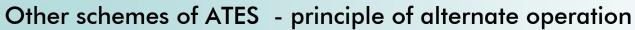
Introduction





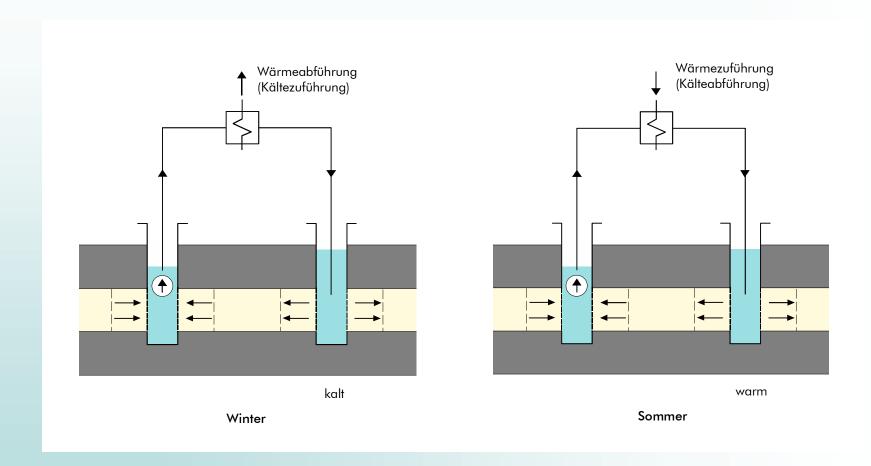
Introduction







Introduction





Principally, aquifers (groundwater-bearing beds) which are intended for thermal energy storage should come up to the following requirements:

- Max. depth of 1000 m:
 At present, a depth of up to 200 m represents the most favourable variant for the installation of low-enthalpy stores in terms of cost.
- Covered (confined) groundwater-bearing bed:
 On condition that adequate technological storage
 parameters are selected, even phreatic aquifers can be used
 according to most recent studies.



- Max. effective reservoir thickness approx. 30 m:
 If thicker, special production techniques would be required due to the horizontal propagation of the thermal front.
- Homogeneous aquifer structure:
 Strong interstratification may result in a smaller coefficient of recovery.



- Geometrical aquifer structure:
 Major differences in level relative to the aquifer top may lead to problems when re-producing the fluid accumulating in the top sections.
- Low regional base flow or detailed knowledge on the regional groundwater flow parameters:
 Appropriate siting of the wells can influence the propagation of the thermal front which is important for long-term operation.



- Appropriate chemical composition of reservoir fluid (heat transfer medium) and matrix:
 Changes of the state in the working section of the reservoir must not affect reinjection.
- Store installation out of groundwater catchment areas: Interference and quality impairment must be avoided.



Ne ubran den burg regional vorhande ne Aquifere (sehr gute Speichereigenschaften) regional vorhandene Aquifere (gut e\$ peicher eigenschaft en) nur ör tlich vorhanden e Aquif er e (gut e - siehr gut e. Speicherei gensich aften) Speicherung nur in Ausnahmefällen möglich

Geological conditions

Geological potentials of aquifer thermal energy storage



- Depending on the state of the geological knowledge, at least two exploratory wells should be drilled down on the site, followed by geophysical logging giving evidence on:
 - * depth and thickness of the aquifers
 - existence of aquicludes in the under- and overlying sections of the aquifer intended for thermal energy storage
 - * non-homogeneities in the aquifer
- Pump and injection tests duly recording the changes of the water level in the water and oberservation wells - are to determine the productivity and injectivity of the water well.



- Objectives of the laboratory analysis of matrix and fluid:
 - * Mineralogical investigations of the matrix to describe potential damages to the reservoir caused by precipitation or intrastratal solution caused by temperature changes
 - * Determination of the grain size distribution to characterise the reservoir



- * Geochemical investigation of the groundwater to identify the water components with regard to their reaction behaviour in changed temperature conditions
- * Determination of the actual microbiological state of the groundwater to identify the sensitivity of the reservoir to temperature increases

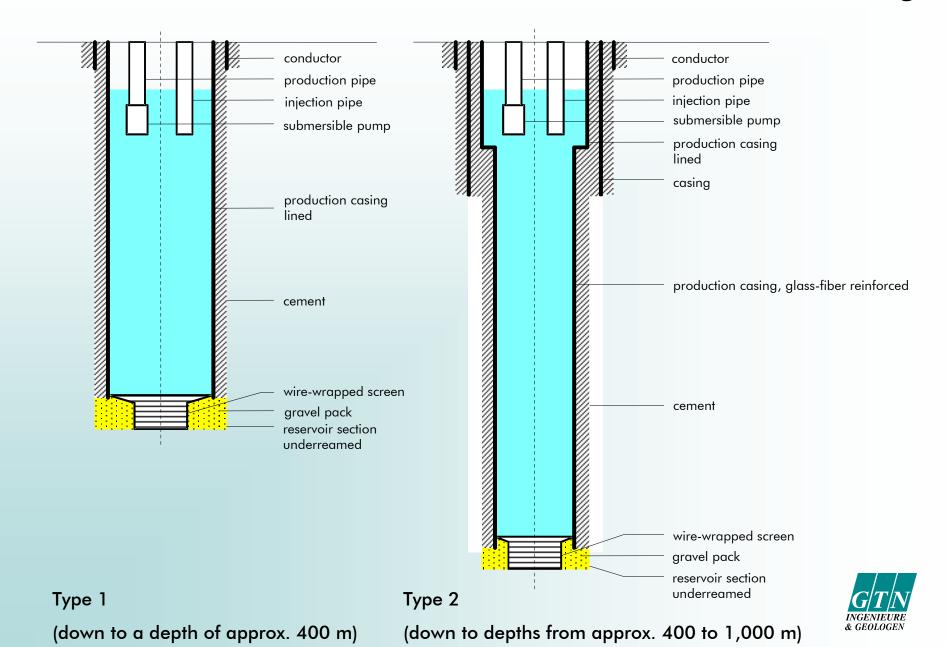


- * Isotope-hydrogeological analysis to determine the hold-up time of the groundwater and to derive a potential geohydraulic communication among neighbouring wells
- As the geometrical aquifer structure is especially important, shallow seismics proved to be an efficient method to enhance the state of hydrogeological knowledge



Comparing	Water well	ATES well
Water temperature	constant	cold/warm
Injection	no	yes
Mode of operation	continuous throughout the year	seasonal
Flow	continuous	discontinuous
Direction of flow	one direction	two directions



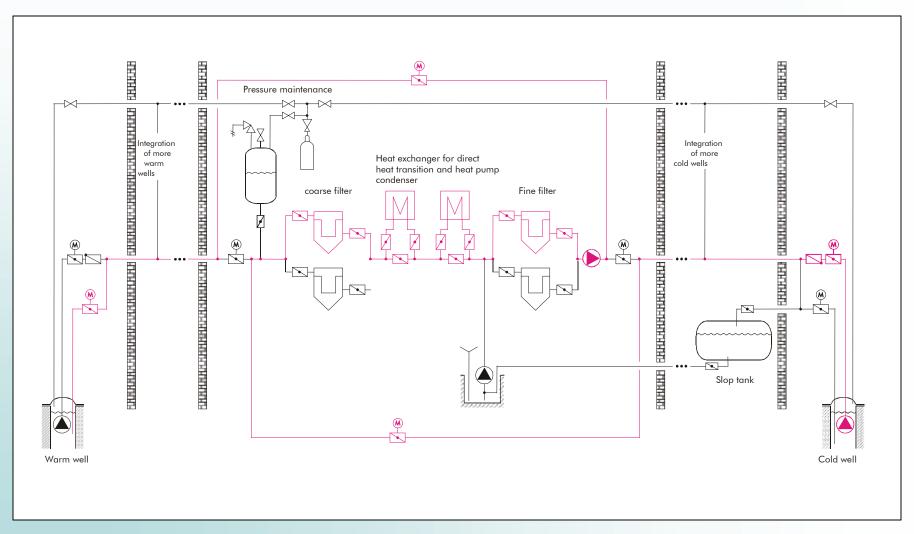


- The most important parameter is the well diameter which depends on several criteria to be observed:
 - * laminar flow in order to prevent the precipitation of ochre and incrustations in the screen section
 - * non-overspeeding of the critical flow velocity against the screen

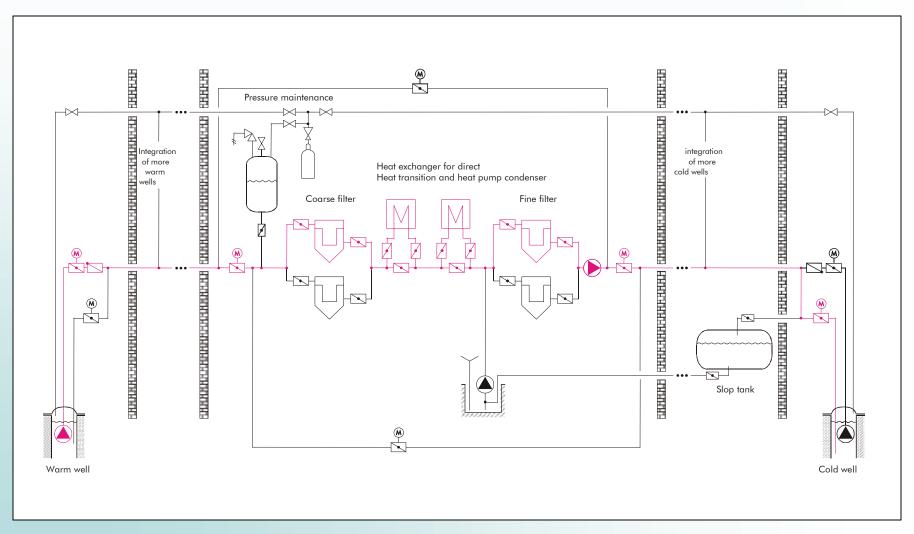


- the diameter required for installation of the submersible pump
- resistance of the equipment to thermal shocks and corrosion



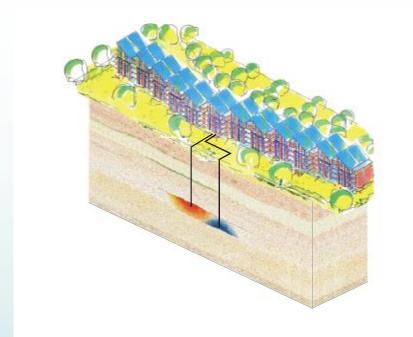








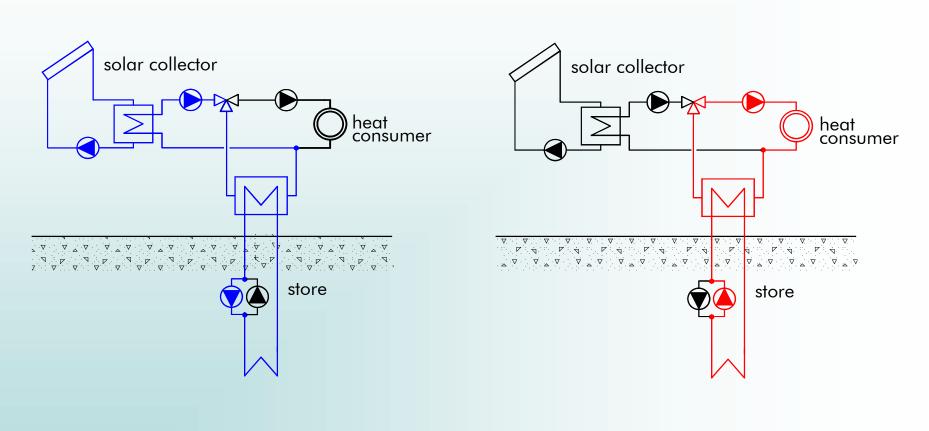




Design and present view



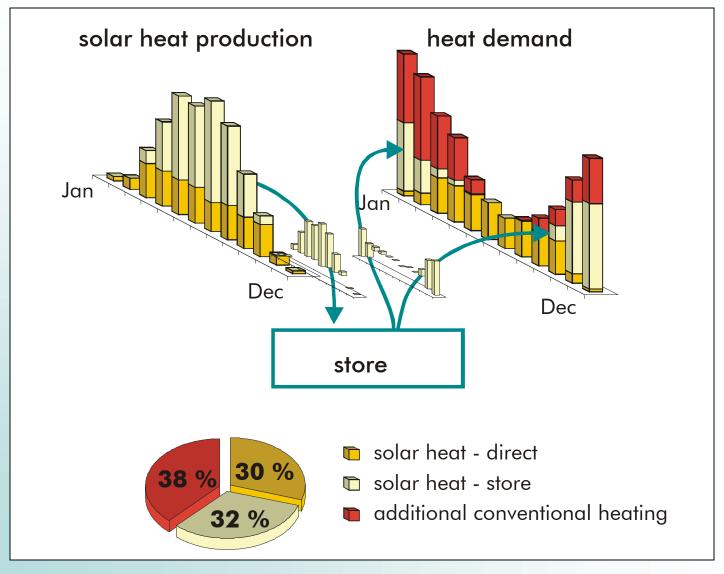




summer winter



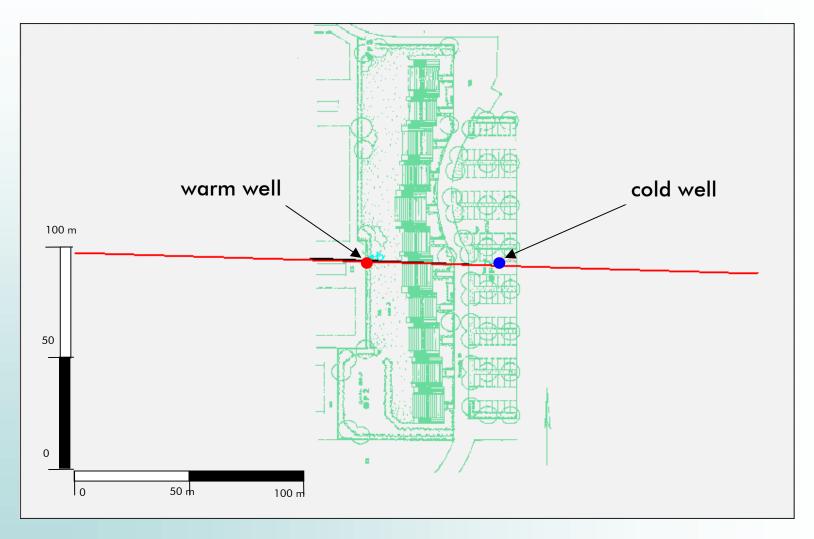
Technical concept of solar energy storage





m u. GOK (NN 0.00) _S, Mu, h 0.0 0.01_/ mS, fs, u' 0.58_ 1.0 Lg, U, fs 0 mS, fs, gs' 1.00_/_ 2.0 (kve) 1.50_ ∖mS, fs, u' 2.00_/ 3.0 4.0 5.0 6.0 _Lg, s 7.0 7.00_ Lg, U, ms, fs 8.0 8.00_ _mS, gs, fs 8.40_ Lg, Ŭ, s , g 8.80___ 9.0 9.00_/ 10.0 11.0 12.0 _Mg, u, s mS, fs 12.60_ 13.0 13.00_ 14.0 15.00_ Mg, U, s, t, g 15.0 16.0 16.72 ___(kve) 17.0 17.00 mS, fs 17.90 18.00 18.40 19.00 19.20 17.90_ 18.0 ⊤fG, mg, gs √ fS, u, ms' 19.0 fG, gs, ms (kve) 20.0 fS, u, ms' 20.60_ 20.80 fS, u 21.0 (kve) 21.10_ 22.0 _fS, u, ms' 22.50___ mS, fs 23.0 23.00_ 24.0 25.0 25.50_ 26.0 fS, u 26.10__ (kve) 26.40__ 27.0 fS, u 27.10_ 28.0 _Mg, U, s' 28.60_ 29.0 __mS, u _, fs _Mg, U, s' _fS, u 29.20_ 29.50_ mS, fs 30.0 ET 30.00_ ET 30.00_







geological formation: Quaternary

• depth: 13 m - 27 m

• store temperature: 11 °C

• porosity: ~20 %

• permeability: $0.25-0.5 \,\mu\text{m}^2$

number of wells:

• internal distance: 55 m

production and injection

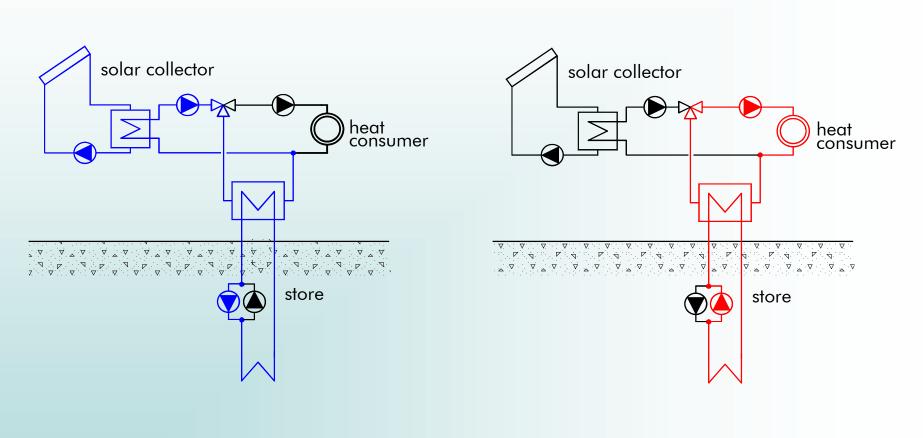
flowrate: 20 m³/h

injection temperature: 50 °C

charging heat: 234 MWh/a

discharging heat: 222 MWh/a

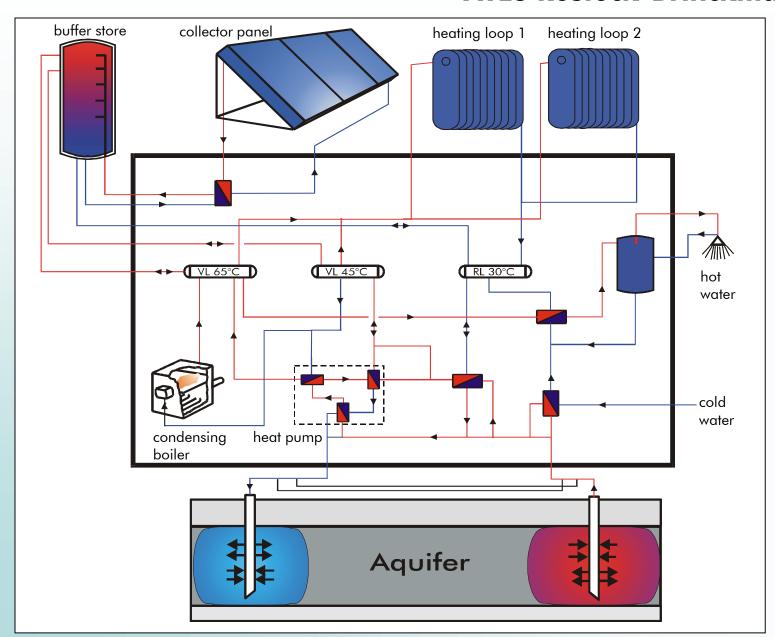




summer winter



Technical concept of solar energy storage







Collector roofs during construction





External view of the warm well cellar



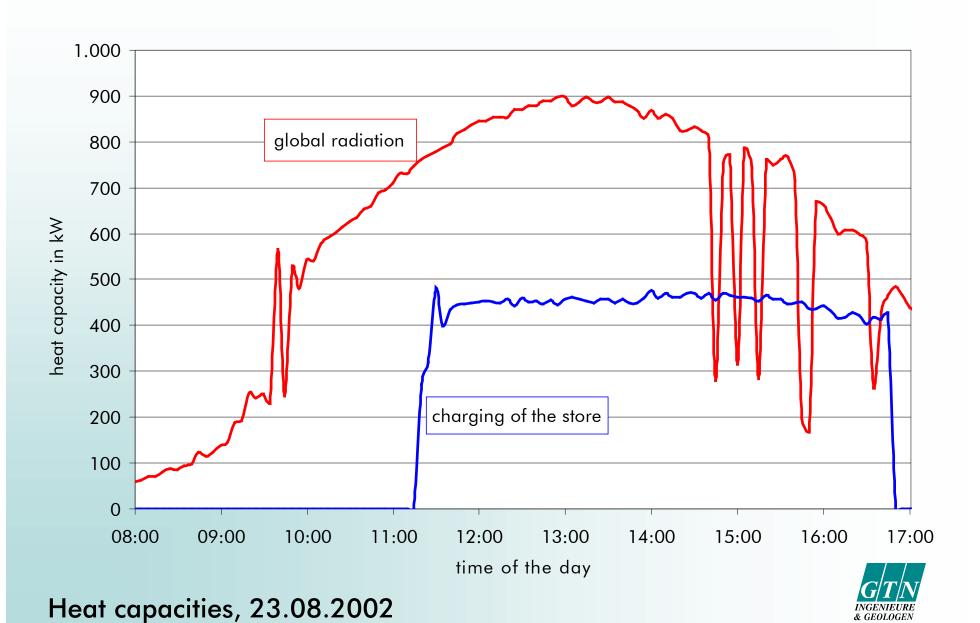


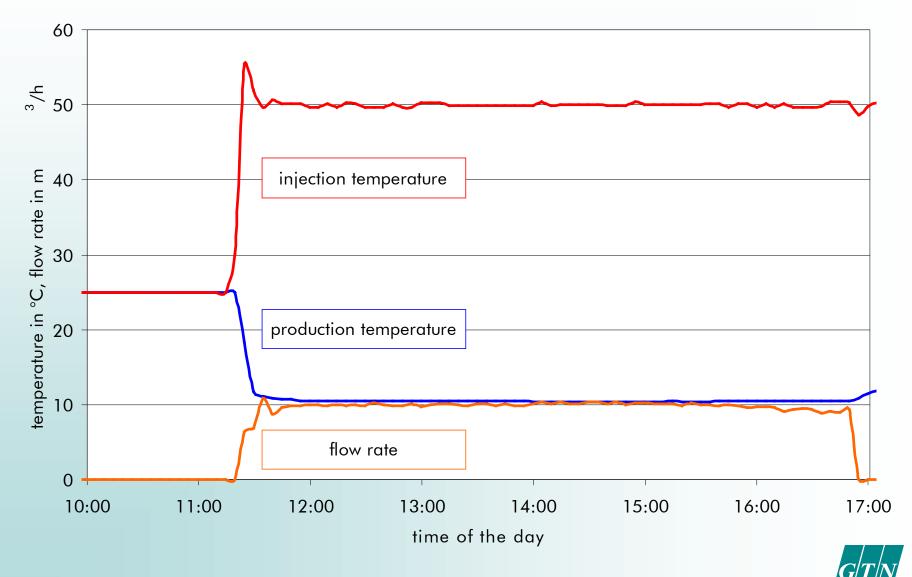
Heat exchangers for charging and discharging (left) and heat pump (right)



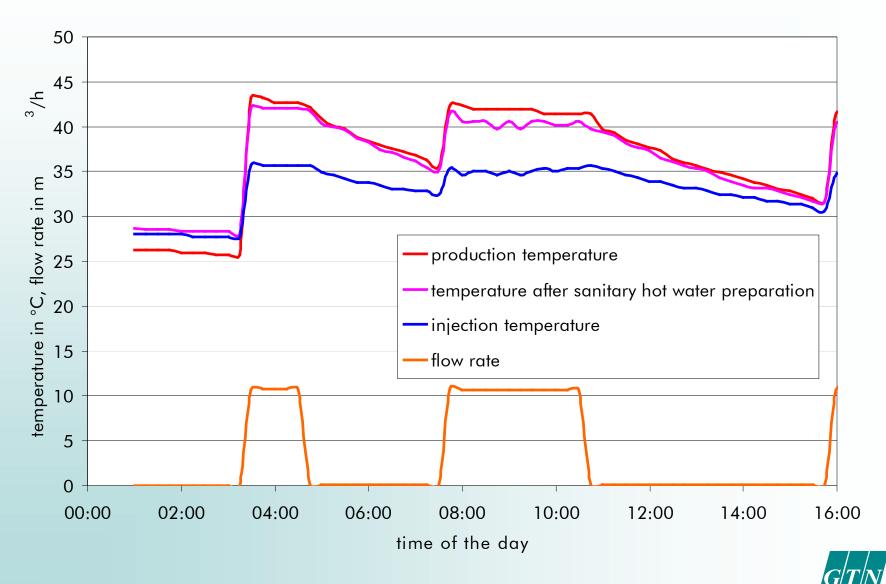
Well head during construction



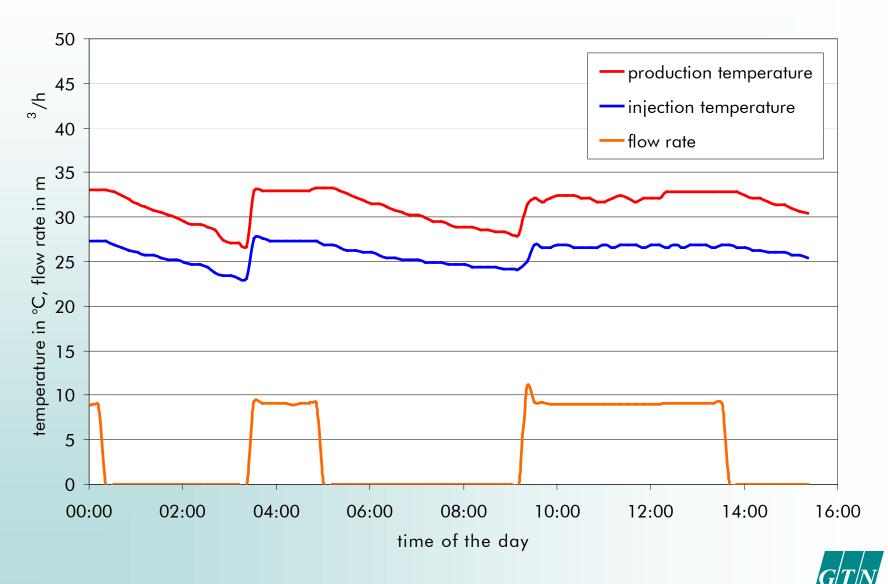




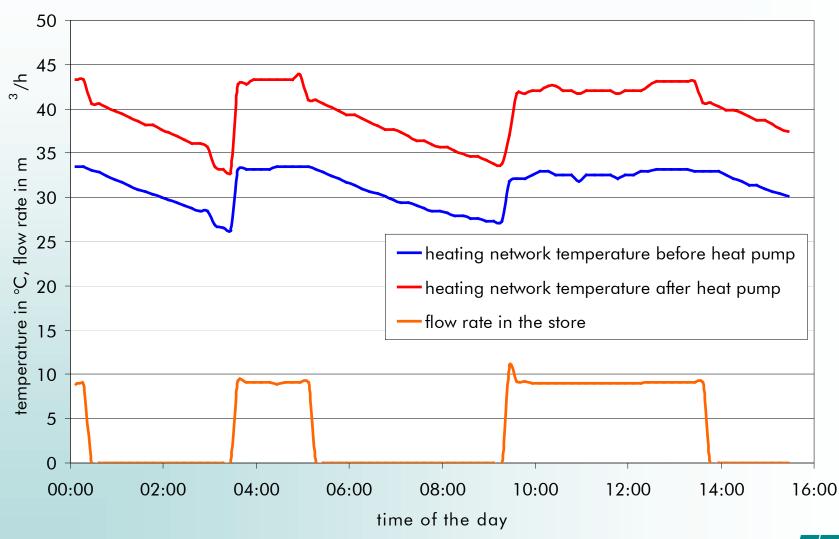
Storage loop parameters, charging, 23.08.2002



Storage loop parameters, discharging, 1.9.2002

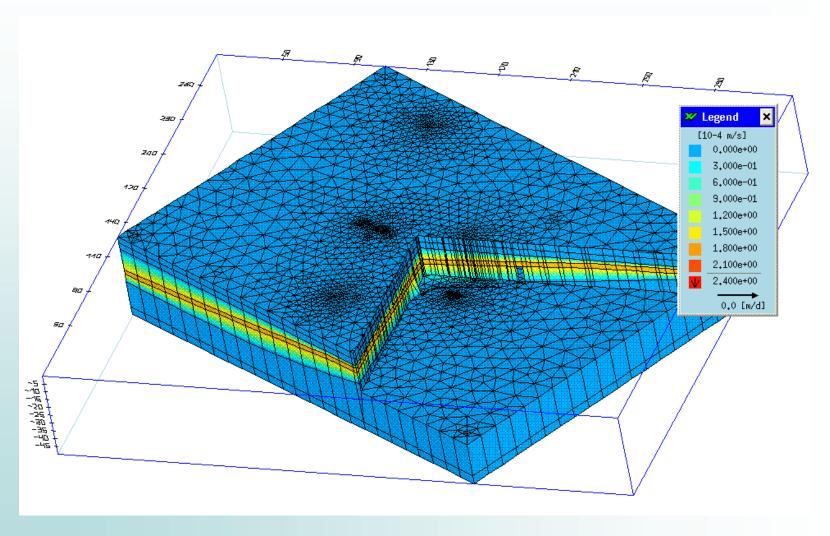


Storage loop parameters, discharging, 27.11.2002

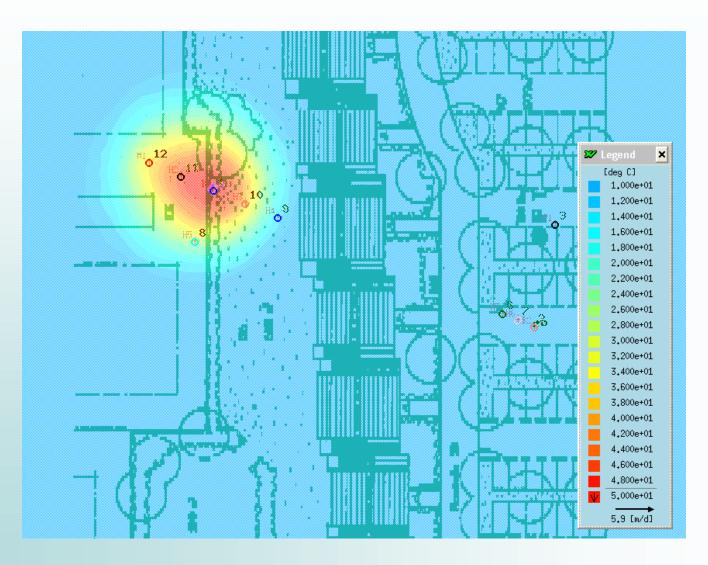


Parameters at the heat pump condenser, discharging, 27.11.2002



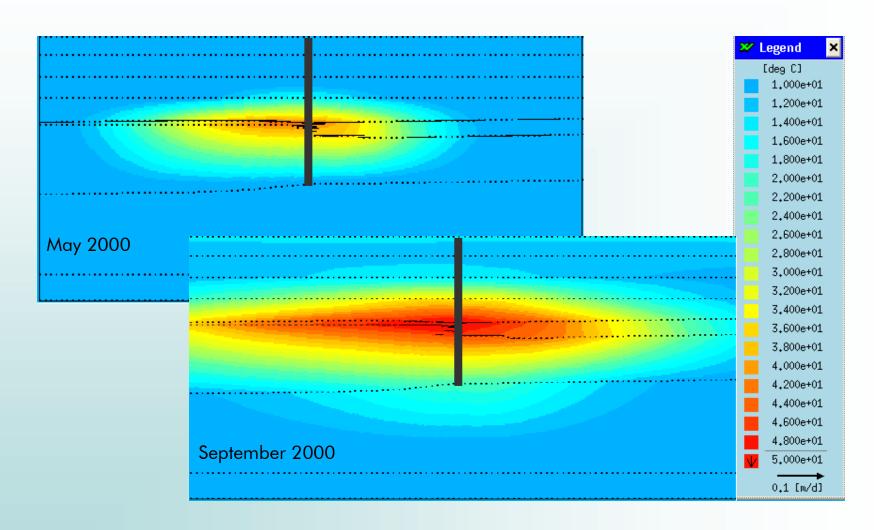






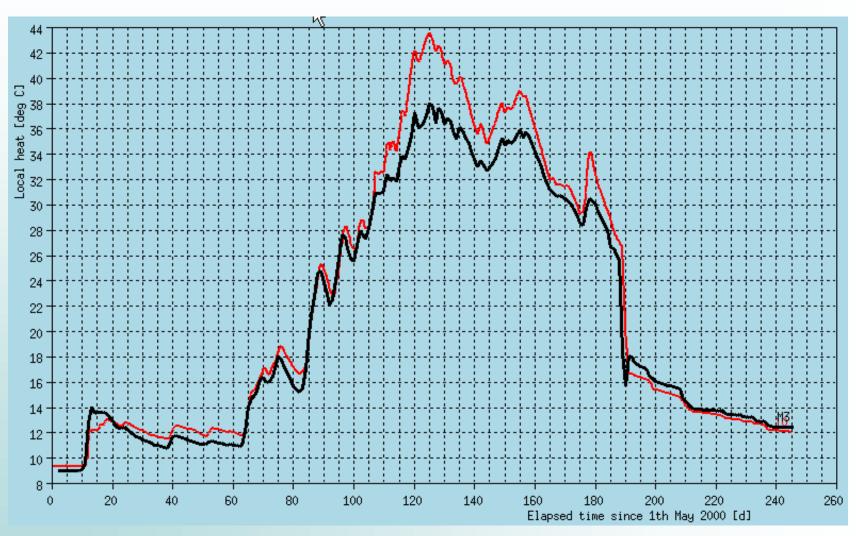
Simulated temperature distribution when charging at a depth of 17 m, early September 2000





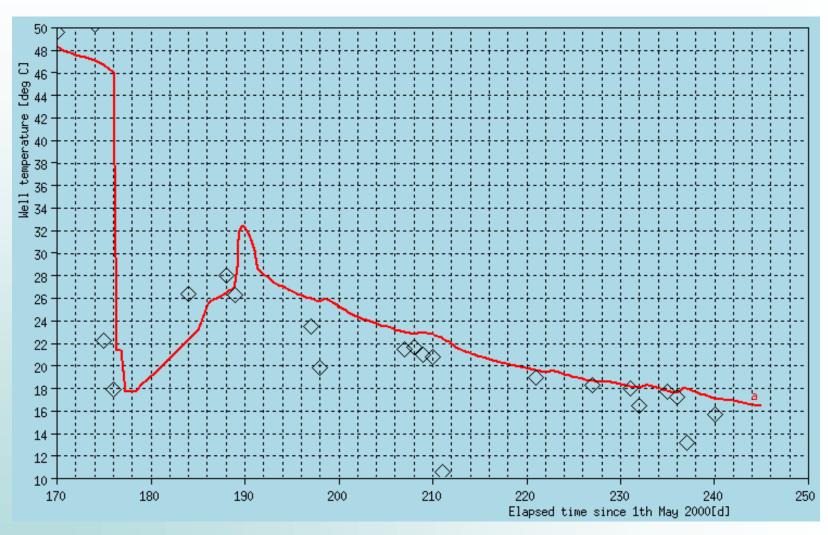
Calculated temperature, model layers and velocity arrows along the track of intersection





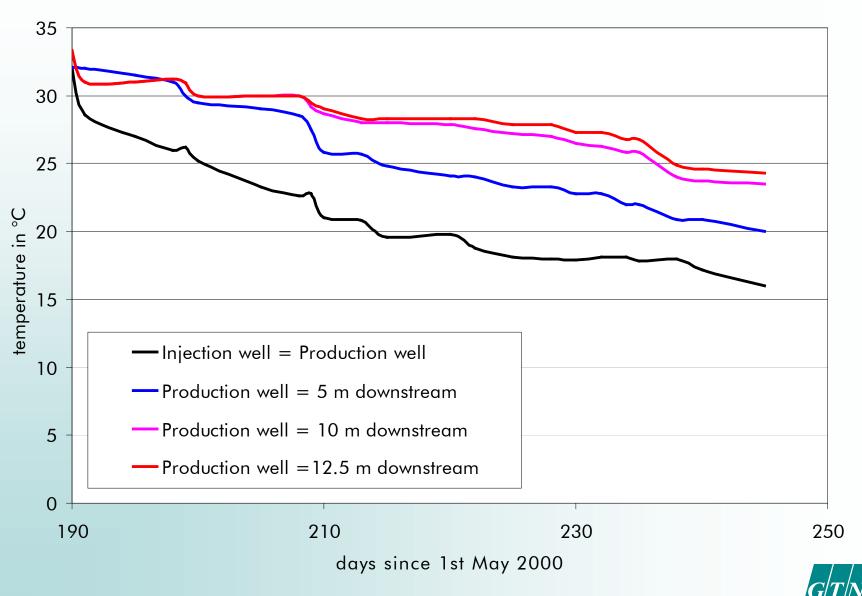
Calculated (red) and measured (black) temperature behaviour at the measuring-lance M3 in 2000



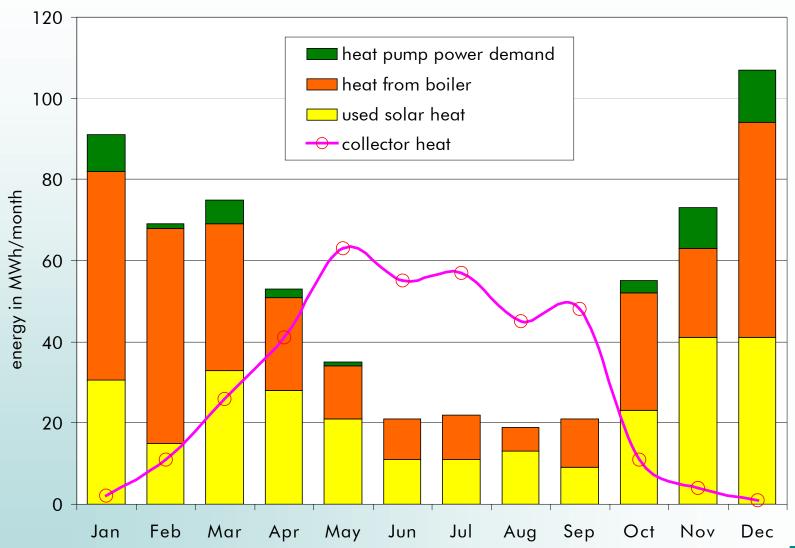


Calculated (red) and measured (black rhombs) discharging temperature, end of 2000 (days since 1st May)



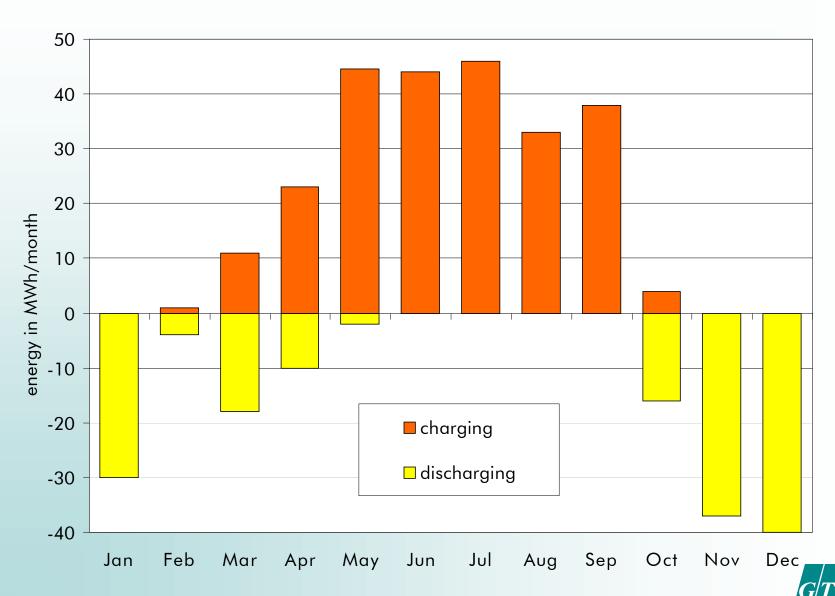


Dependency of the discharging temperature on the well site

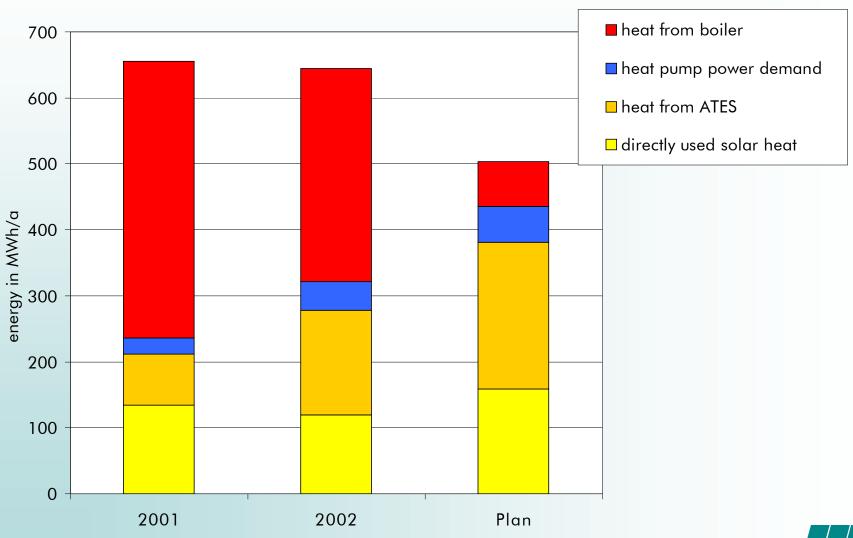


Monthly heat balance of the system (2002)





Monthly heat balance of the ATES (2002)

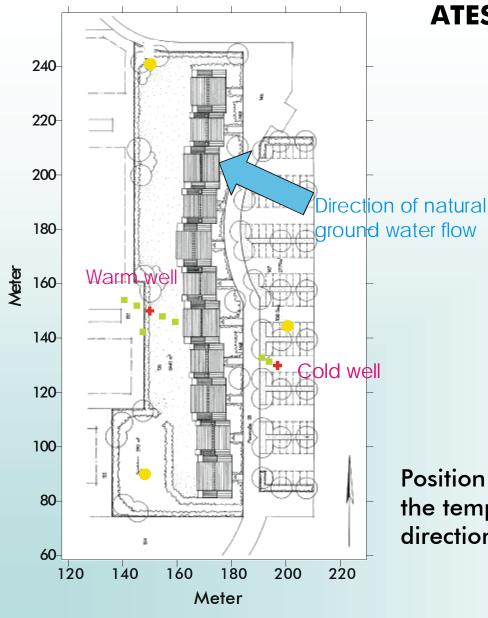


Heat balances in 2001 and 2002



	2001	2002	2004
•Solar fraction	32 %	43 %	49 %
•ATES recovery factor	36.5 %	64.5 %	48,5 %
•COP of heat pump	4.1	4.3	4,5

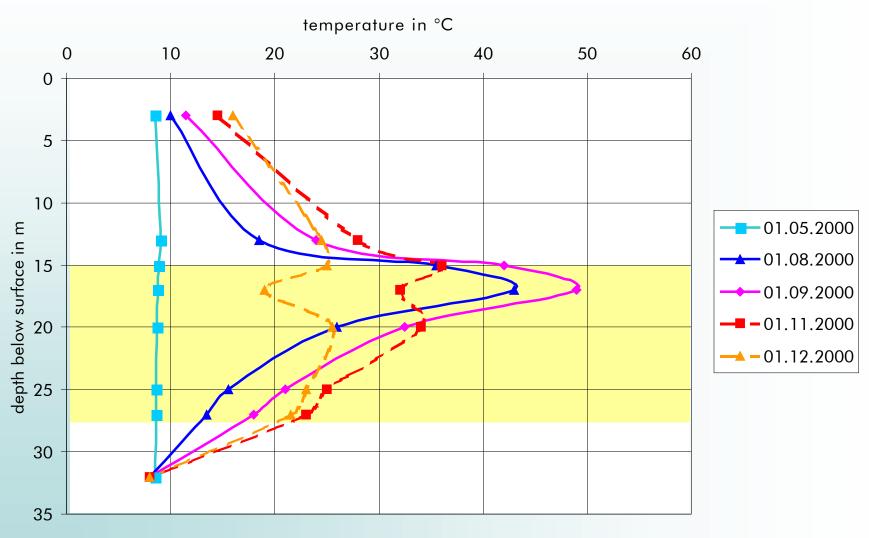




Position of the wells, the temperature measuring-lances and direction of natural groundwater flow

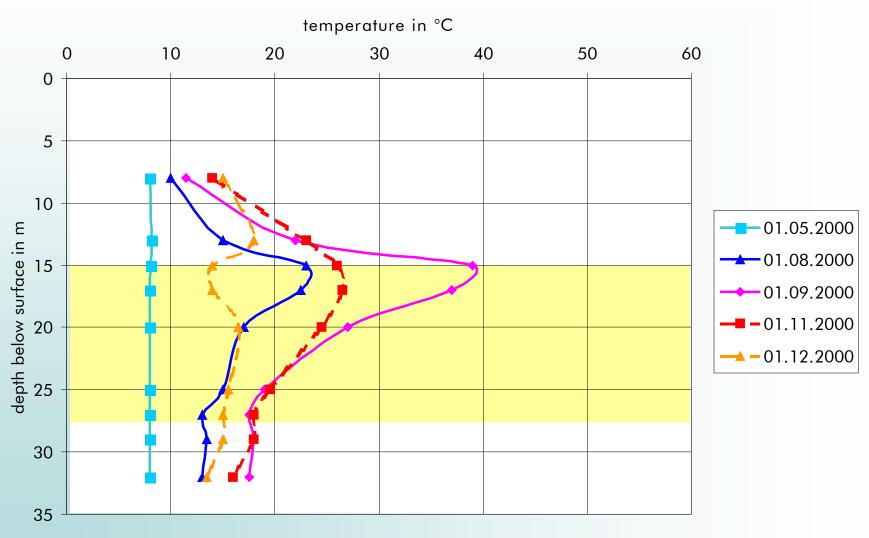
- Observation well
- Temperature measuring lances





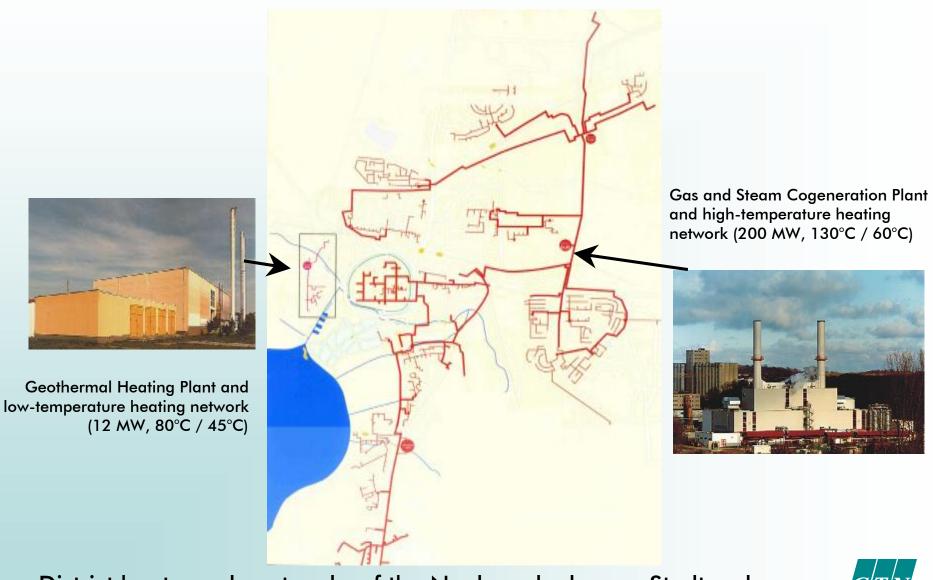
Temperature profiles at measuring-lance M2, 5 m downstream of the warm well





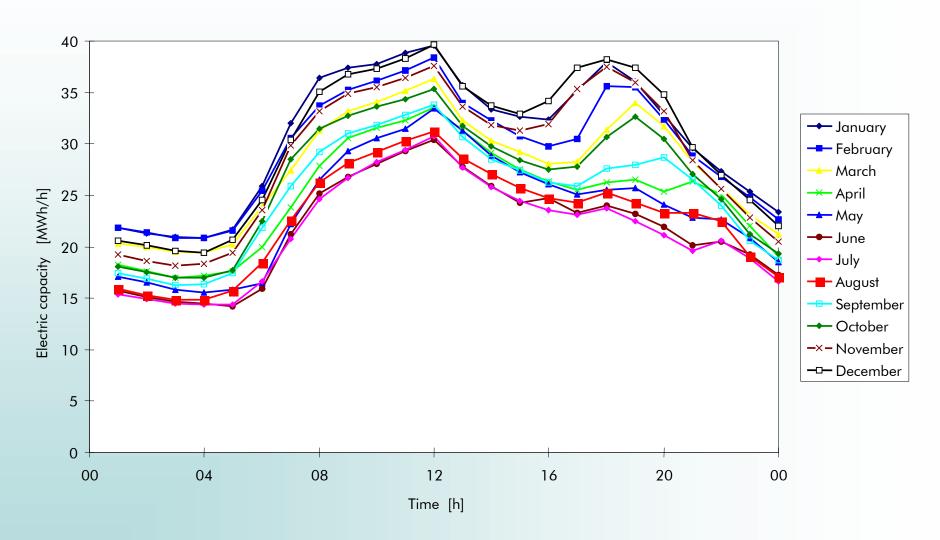
Temperature profiles at measuring-lance M3, 5 m upstream of the warm well





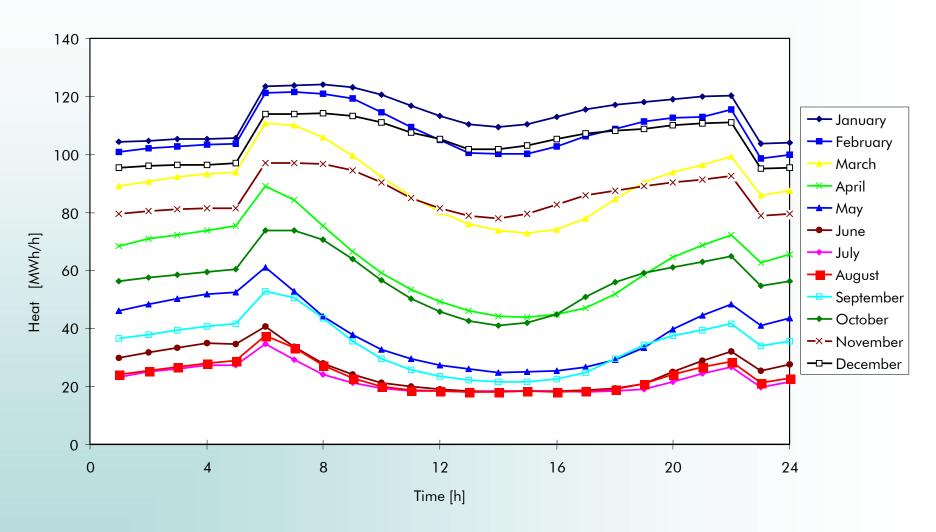
District heat supply networks of the Neubrandenburger Stadtwerke GmbH (Public Utilities)





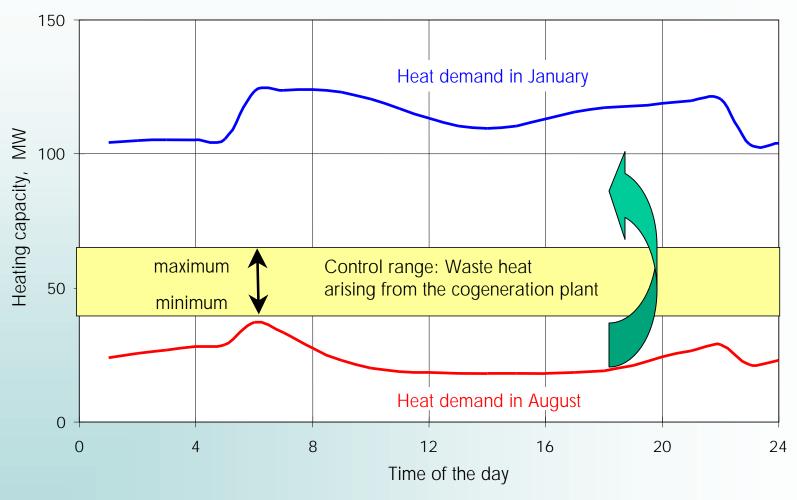


Characteristics of the power demand of the town of Neubrandenburg

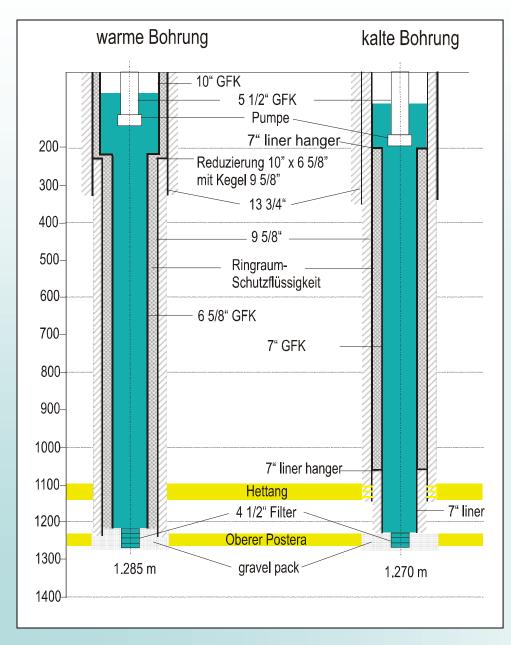


Characteristics of the heat demand of the town of Neubrandenburg











well construction

Production horizons: Hettangian and

Upper Postera

• Depth: 1,105 m – 1,172 m

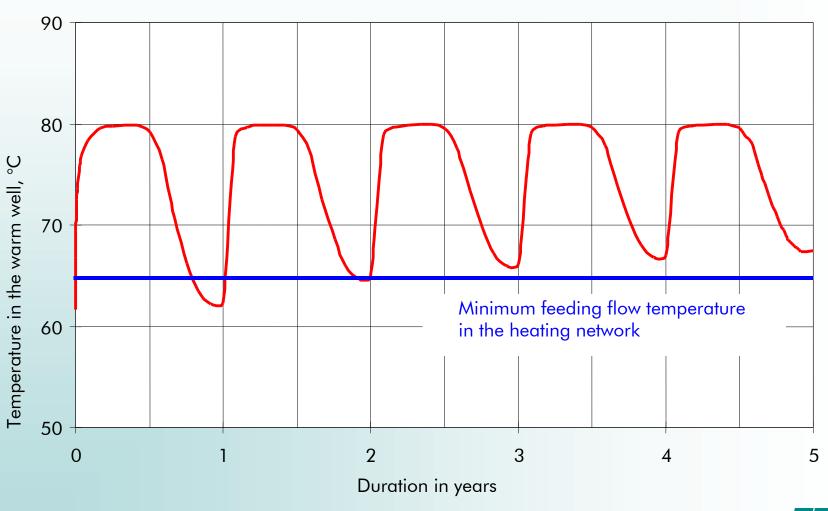
1,237 m – 1,271 m

• Flowrate: 200 m³/h

• Production temperature: 50 °C and 54 °C

•Mineralisation: 118 g/l and 133 g/l

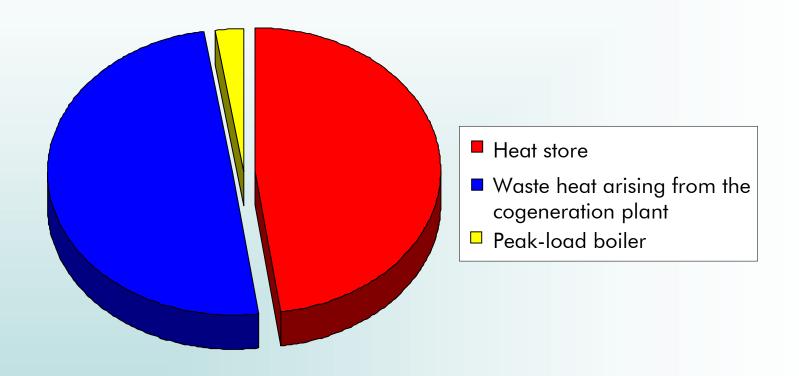






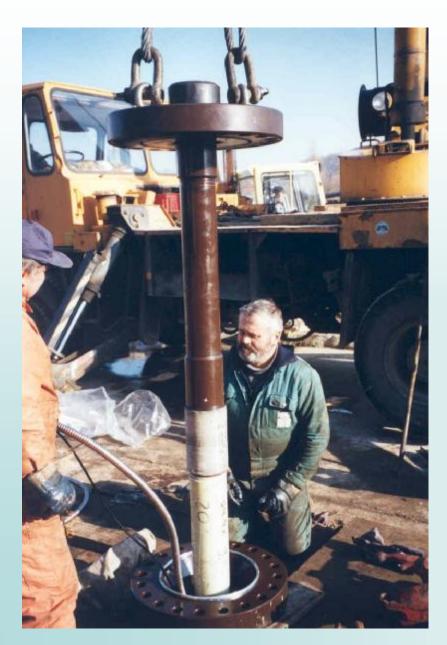






Balance of generation in the district heat supply network "Rostock Street"





Installation of the submersible pump in the well Gt N 4/86 in 2002









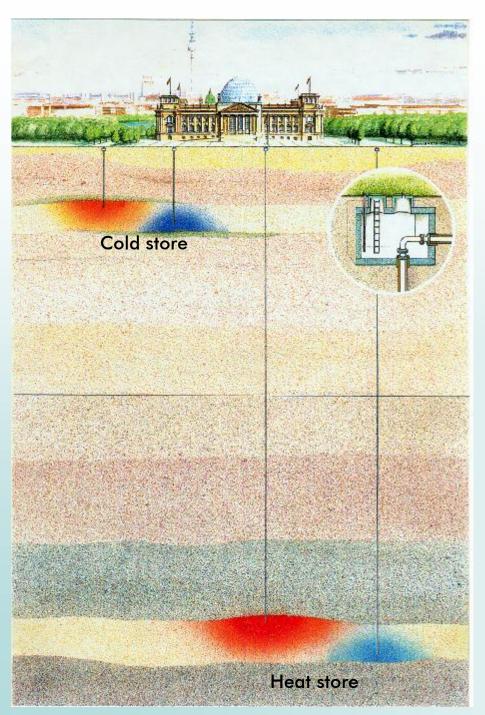














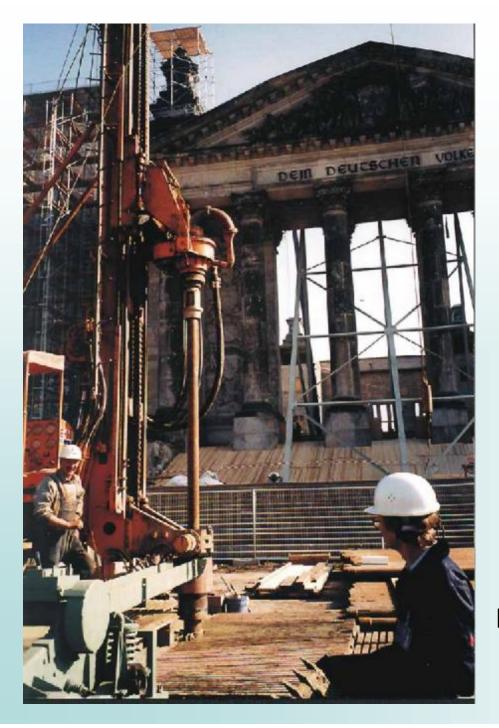


Parliament buildings supplied by ATES



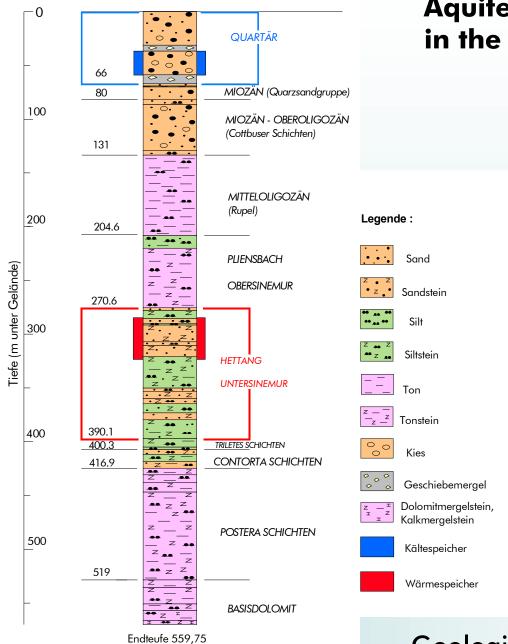






Drilling of a heat store well







• Geological formation: Hettangian

• Depth: 285 m- 315 m

•Store temperature: 19 °C

•Mineralisation: 29 g/l

• Porosity: 30.4 %

• Permeability: $2.8-4.2 \mu m^2$

Number of wells:

•Internal distance: 400 m

• Production/injection flowrate: 100 m³/h

•Injection temperature: 70 °C



Geological formation: Quaternary

• Depth: 30 m- 60 m

•Store temperature: 10 °C

• Porosity: ~30 %

• Permeability: $> 1 \mu m^2$

Number of wells:12 in 2 groups

•Internal distance: 400 m

• Production / injection flowrate: 300 m³/h

•Injection temperature:

in winter 5 °C

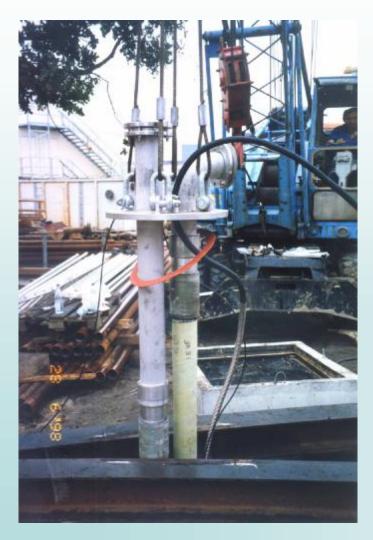
in summer 28 °C









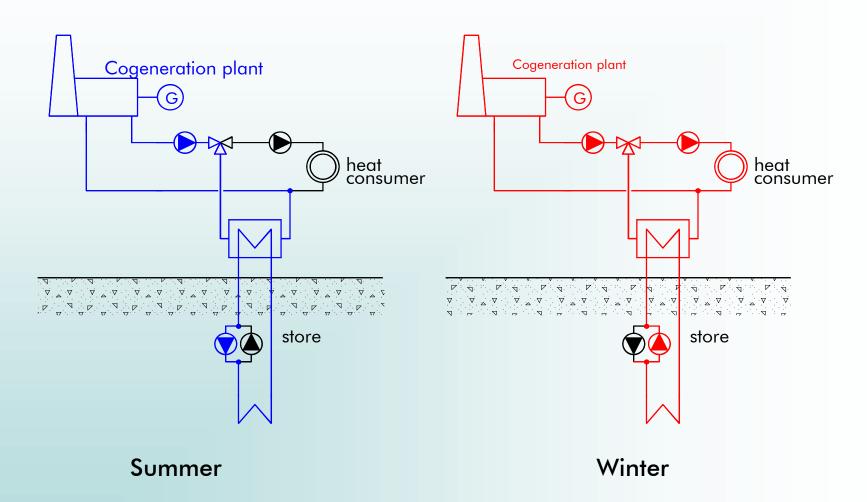




Heat store well chamber

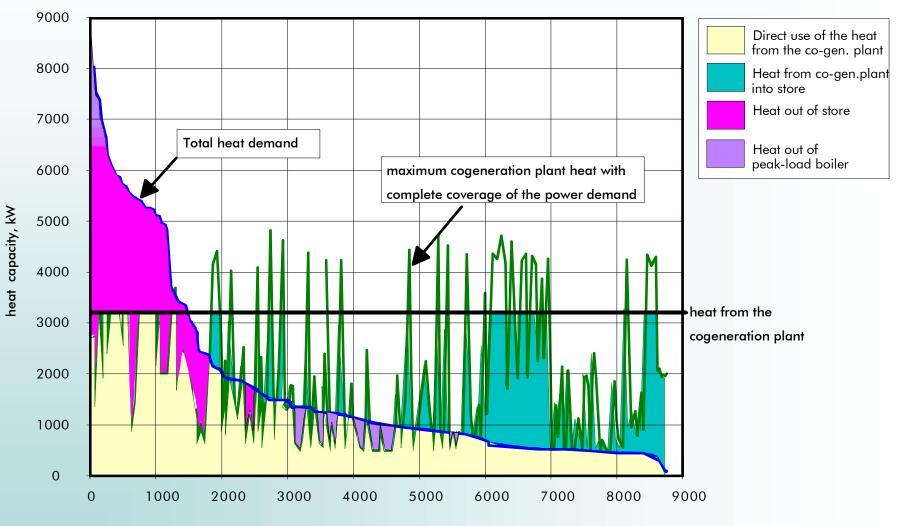






Technical concept of the storage of waste heat arising from a cogeneration plant

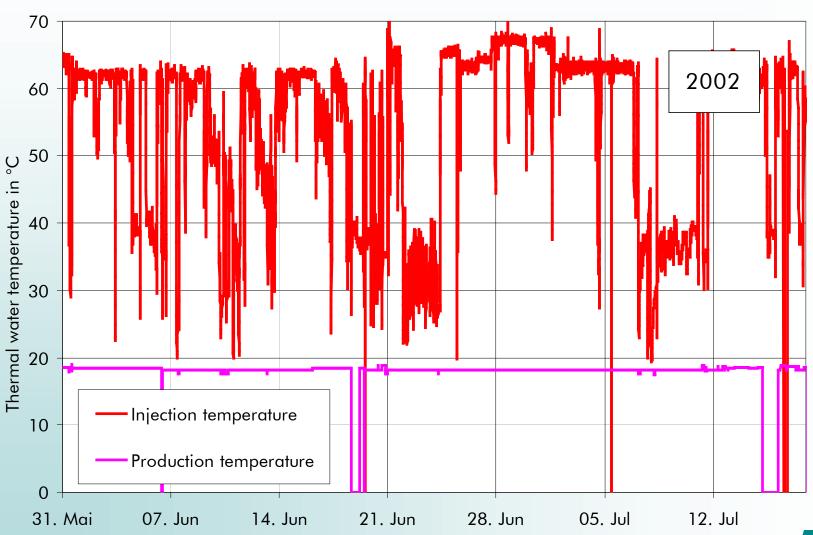




duration, h/a



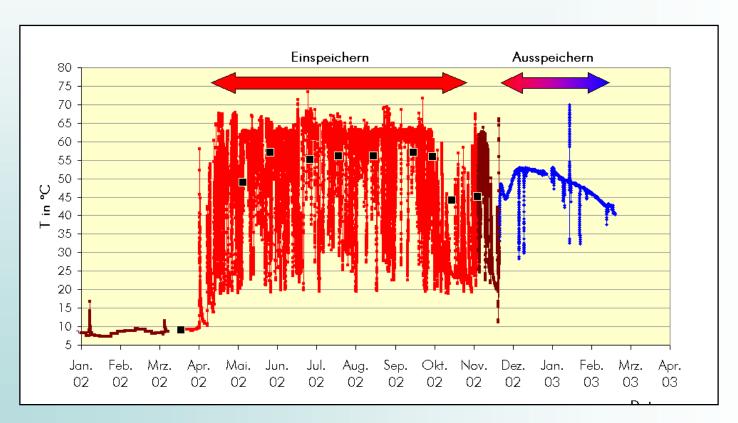






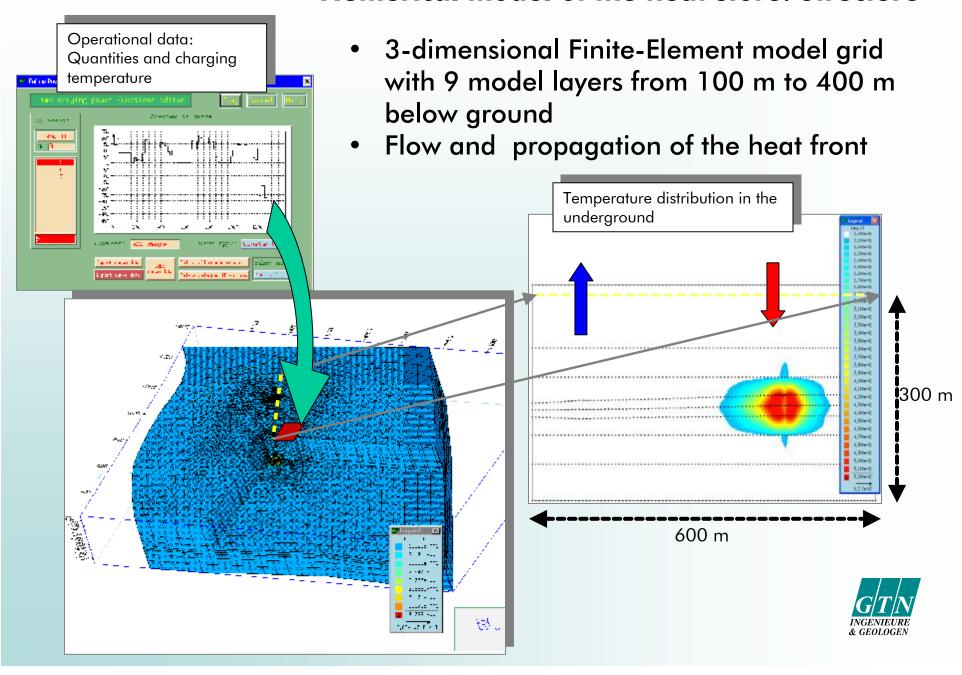


- Until autumn 2002: Charging only
- First regular annual cycle: Completed by discharging in winter 2002/2003

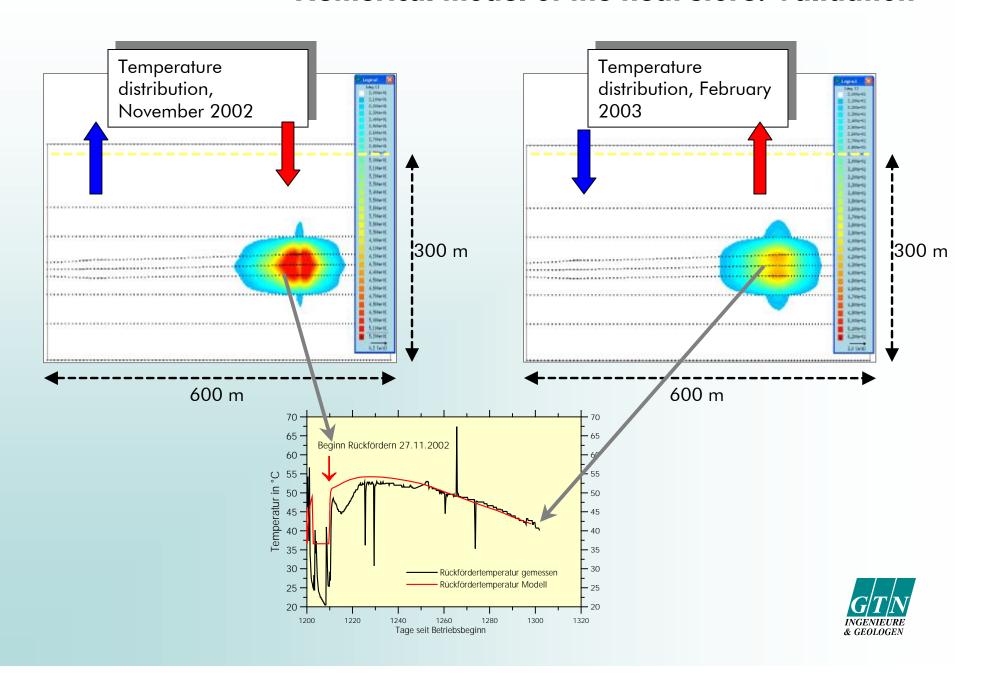


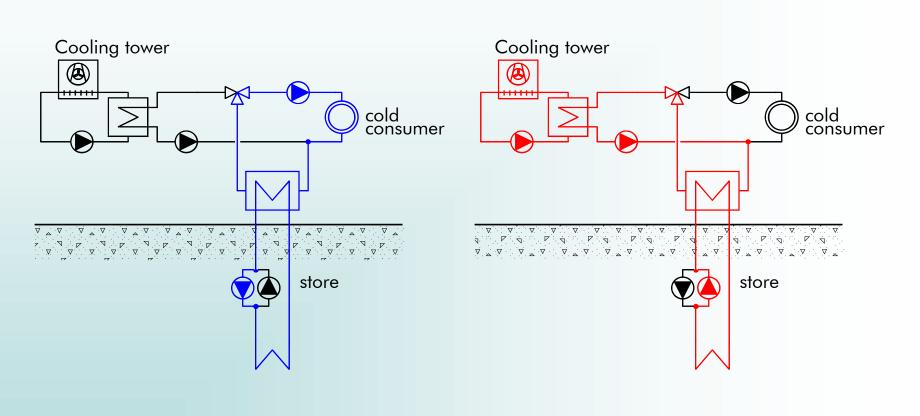


Numerical model of the heat store: Structure



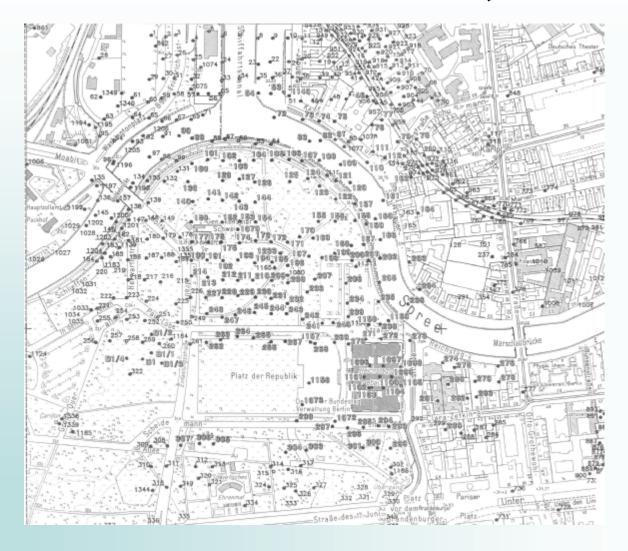
Numerical model of the heat store: Validation



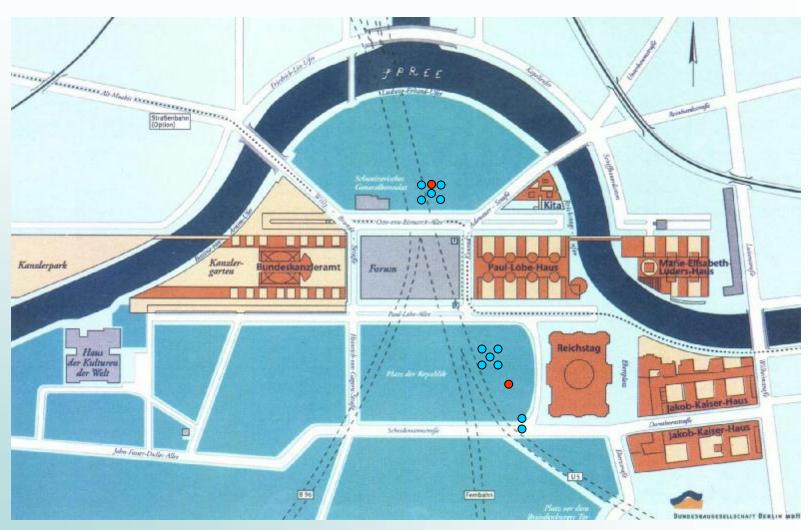


Summer Winter





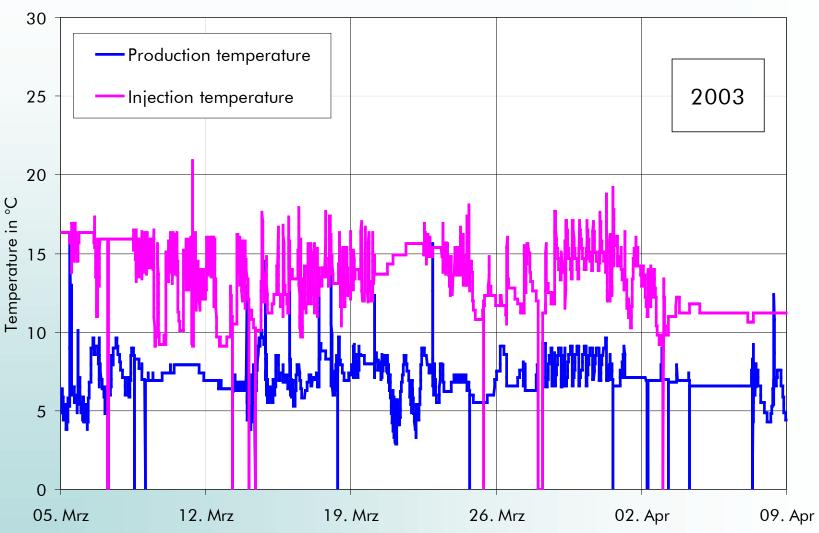


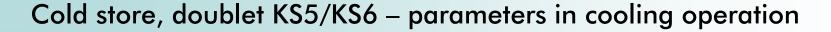




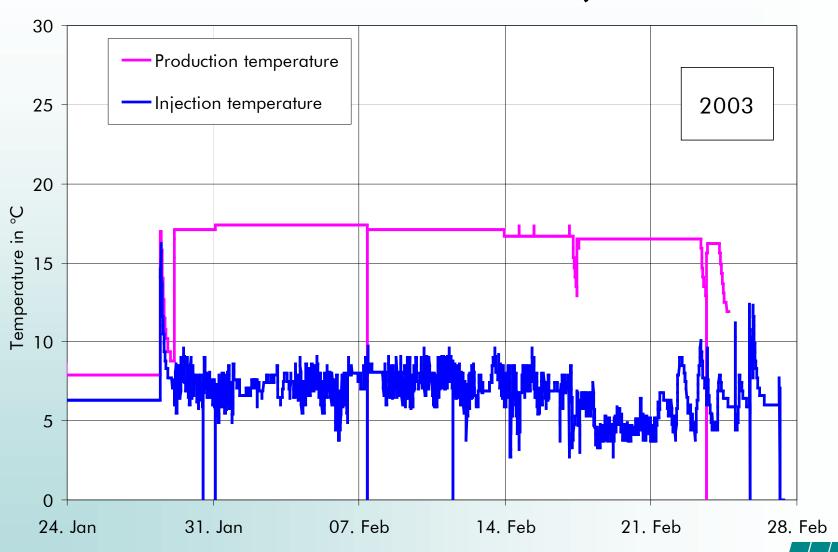
Heat store







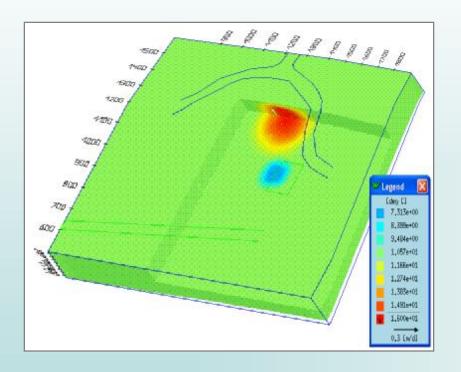




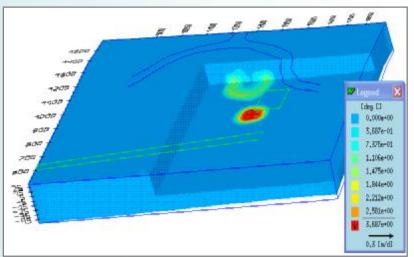
Cold store, doublet KS2/KS3 - parameters during regeneration

Numerical model of the heat store

Simulated temperature distribution, March 2003



Simulated cooling-down since March 2002







Cold store well head



Heat store well head





Surface loop of the cold store



Surface loop of the heat store





Filter in the cold store loop



Heat exchanger in the cold store loop



