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Virtual hybrid test control of sinuous crack

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Abstract

The present study aims at proposing a new generation of experimental protocol for analysing crack propagation in quasi brittle materials. The boundary conditions are controlled in real-time to conform to a predefined crack path. Servo-control is achieved through a full-field measurement technique to determine the pre-set fracture path and a simple predictor model based on linear elastic fracture mechanics to prescribe the boundary conditions on the fly so that the actual crack path follows at best the predefined trajectory. The final goal is to identify, for instance, non-local damage models involving internal lengths. The validation of this novel procedure is performed via a virtual test-case based on an enriched damage model with an internal length scale, a prior chosen sinusoidal crack path and a concrete sample. Notwithstanding the fact that the predictor model selected for monitoring the test is a highly simplified picture of the targeted constitutive law, the proposed protocol exhibits a much improved sensitivity to the sought parameters such as internal lengths as assessed from the comparison with other available experimental tests.

Keywords: A. Crack propagation and arrest. B. Concrete. Crack mechanics. Sensors and actuators. C. Finite element.

2016 MSC: 00-01, 99-00

1. Introduction

Mechanical and civil engineering simulations are based on increasingly complex constitutive models. They enable the behaviour of materials and real structures to be predicted with better accuracy at the expense of more demanding calibration steps. On the one hand, such models have the potential to reduce the need for very expensive large scale tests in service conditions. On the other hand, calibration of the constitutive parameters and assessment of their domain of validity becomes more challenging and requires either new tests (potentially at small scale), or new procedures to exploit at best a richer information. Enhanced sensitivity to model parameters thus becomes a crucial issue in designing optimal experimental tests.

For quasi brittle materials such as concrete, there are different ways of modelling the development of cracking. Smearred crack models were first introduced [1, 2]. Continuum damage mechanics is an alternative route with local and non-local formulations [4, 5, 6, 7, 8, 9]. Cohesive zone models were also proposed to handle initiation and propagation in such materials [10, 11, 12]. In crack band models, the finite width of the process zone is accounted for [13]. Variational formulations can also describe these two different stages of propagation [14]. Discrete descriptions based on lattice calculations are considered to account for multiple cracking [15].

All these models need to be calibrated with possibly discriminating experiments. Stress/strain data are the typical information for calibrating smearred crack and local damage models [16]. For non-local damage models, load/deflection curves of so-called size effect tests can be used [17]. The width of the process zone was shown to be very useful for tuning such models [18]. Point measurements were used by these authors. The process zone width can be revealed via digital image correlation (DIC) [19]. Similarly, the roughness of the fractured surface was also measured and considered for calibration purposes [9]. Conversely, many models only require ultimate strength properties to be known to get first order estimations of their parameters (*e.g.*, see Refs. [8, 20]). From

this analysis it is concluded that very few studies use full-field measurements for identification and validation purposes. DIC was used to monitor complex experiments [21] and calibrate a cohesive zone model [22]. The aim of the present work is to propose such a procedure via virtual testing that explicitly considers
 35 full-field measurements and their uncertainties.

A recent series of crack propagation tests on concrete samples [21] has been performed to achieve complex and discriminating crack patterns (and partly used in an on-going benchmark [23]) by modifying the loading path during the experiment. The mechanical loading was prescribed on the top and bottom part
 40 of the sample by a hexapod [24, 25, 26] (see Figure 1) and the crack tip position was obtained thanks to 2D DIC [27, 28]. First, the results of these tests show that it is possible to manually control the stability and the deflection of a crack in a quasi brittle material using plane loading, namely, a combination of tension, shear and in-plane rotation. Then it has been shown that these complex cracks
 45 with many changes of propagation direction and branching were sensitive to parameters of a state-of-the-art non-local damage model [20].

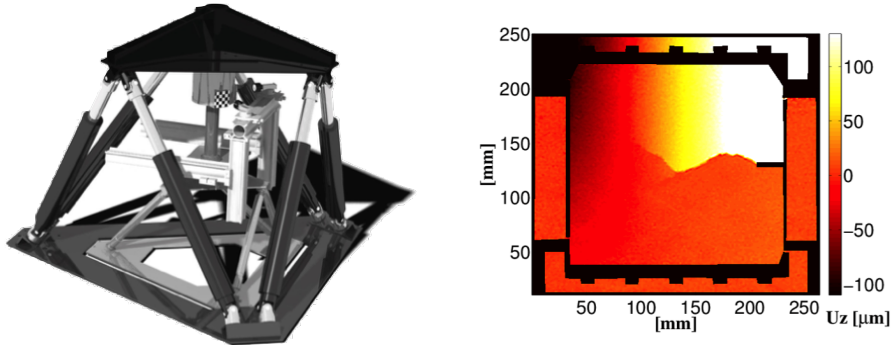


Figure 1: (a) Multi-axial testing machine (hexapod) with six degrees of freedom and (b) vertical displacement field on a concrete sample measured via DIC after having manually monitored the loading so that the crack path successively propagates along predetermined directions [21]

Manual control of the loading path in a multi-axial testing machine to achieve such crack propagation experiment is thus possible, but extremely delicate and definitely non-optimal. Automated load control would be highly desirable. It

50 would allow for a much more reactive feedback on loading directions and magnitudes, hence leading to an enhanced accuracy in following a predetermined crack path, and provide the needed flexibility to reveal parameters that are difficult to calibrate. This, undoubtedly, would pave the way to ‘smart’ and adaptive experiments, a kind of holy Grail in optimised mechanical tests.

55 The design of such control loops is challenging. The first generation of mechanical tests appeared in the late eighteenth century, which were based on a load defined before performing the experiment. The second generation of tests followed when they were controlled by a local and measurable quantity of interest (*e.g.*, strain). This was also true for multiaxial experiments [29, 30, 31]. Such
 60 experimental possibilities now flourish up to a full 3D control, which with 6 degrees of freedom becomes very demanding in terms of servo-control [24, 25, 26]. In spite of this remarkable progress, none of these types of experiments meets the above objective. It is the authors’ belief that the control of experiments via numerical simulations (*e.g.*, finite element computations) updated in real-
 65 time with full-field measurements constitutes a major breakthrough and open new perspectives. As such they can be seen as a sort of ‘*3rd generation experiments.*’ It also enters the framework of dynamic data-driven application systems [32] whose emergence is one critical aspect of simulation-based engineering sciences [33]. Therefore, an interaction between the mechanical loading,
 70 the measurements and the model must be considered, thereby defining the basis of a hybrid testing procedure (Figure 2).

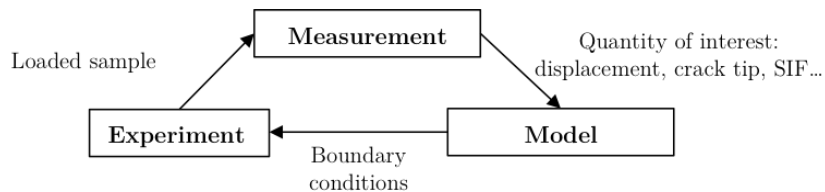


Figure 2: Principle of 3rd generation tests

In the literature, most hybrid experiments reported so far are the so-called

‘sub-structured hybrid tests’ [34, 35, 36, 37]. The latter ones address the dynamic response of generally large-scale structures, and are currently a very active and promising field of research. The spirit of the method is to split the structure into at least two parts. Among them, those that have a simple mechanical behaviour are computationally simulated and referred to as *numerical sub-domains* (or substructures). The other parts, which are critical and complex (*e.g.*, involving non-linearities, irreversibility), the so-called *physical sub-domains*, are kept as substructures actually tested in the laboratory. Pseudo-dynamic testing, continuous pseudo-dynamic testing, fast hybrid testing, real-time substructure testing and real-time dynamic substructure testing [38, 39, 36, 40] are methodologies developed within this hybrid framework and where part of the structure is substituted by computations. On the one hand, these hybrid tests can greatly reduce the overall cost since most of the structure is simulated numerically, while the much smaller key elements are studied experimentally. Moreover this enhanced cost-effectiveness involves no prejudice to the realism of the mechanically tested part. On the other hand, the models used for the numerical sub-domains are to be well-mastered and simple enough so that computations can be performed quickly to perform dynamic tests. In addition, the measurement devices used for feedback are generally poor and frequently reduced to few local strain gauges or LVDTs and often no more than one single actuator is used. These limitations are nothing but the manifestations of fairly recent and novel developments. The main objective is to focus the experiment on a substructure, and substitute the environment — expected to be simple and well-understood — by a model and controlled actuators.

In contrast, although the proposed hybrid approach shares a number of common features and tools, it does not rely on a partition of the structure into parts. In the above-mentioned desired monitoring, the tested and simulated structure or material specimen are shared, and perfectly superimposed. Hence, an additional challenge to be faced is that the behaviour is not yet fully determined at the stage where control is to take action.

The proposed strategy is to use a simple predictor model — a.k.a. ‘low-

level' model — that is able to predict (to first-order accuracy) crack propagation
105 and orientation. During the experiment, the quantities of interest (*e.g.*, crack
tip, local displacement, stress intensity factor) are measured on the specimen
and then compared to the set-point values, and the error (*i.e.*, the difference
between the prescribed and current variables) is introduced in the 'low-level'
model that enables the loading condition to be readjusted in order to follow the
110 pre-established target. The use of a simple model is desirable because it allows
for fast computations as needed for real-time control. However, it is legitimate
to wonder whether driving the experiment with a model that is different from
the one to be identified, does not simply impede the sought identification. It will
be argued that, on the contrary, exploiting the discrepancies between designed
115 and achieved crack path, stress intensity factor, or loading history will reveal
extremely powerful.

This method allows, for example, a test to be controlled by quantities of
interest that are not directly accessible (*e.g.*, crack tip, stress intensity factors,
damage fields) but need numerical simulations to be run. The principle of this
120 innovative testing procedure is to establish a continuous (and possibly seamless)
communication between the experiment and the numerical simulation. By nu-
merically solving an inverse problem, the boundary conditions are computed on
the fly to obtain the sought history (*i.e.*, crack path in the present case). Being
able to modify the boundary conditions as functions of the actual behaviour of
125 the specimen enables the loading history to be adapted during the experiment in
order to better control the quantity of interest. This procedure may seem similar
to traditional tests, but here the choice of quantity of interest becomes nearly
unlimited, thereby opening new possibilities for more discriminating tests.

To perform these so-called 3rd generation innovative tests, the hybrid loop
130 is composed of three main parts:

- An experimental loading device (*e.g.*, hexapod) applying multiaxial load-
ing histories to samples enabling cracks to propagate in stable increments
along various directions.

- A measurement technique (*e.g.*, DIC, Integrated-DIC) to determine the position of the crack tip [41, 42, 43] and injecting it in a control algorithm.
- A control algorithm, which is based on a mechanical model, adapting the boundary conditions in order to follow a predefined crack path via numerical simulations.

For obvious security and set-up design reasons, a first step toward a real 3rd generation experiment is the development of a ‘virtual’ test. The present paper discusses such method to control *simulated* quasi static plane crack propagation on a quasi brittle sample and its validation with an identification procedure on a test-case. A ‘high-level’ model thus numerically simulates crack propagation that is considered as a representation of ‘true’ fracture and substitutes a real experimental set-up. Then the crack tip is numerically detected on the simulated experiment and is used in the ‘low-level’ model that will adapt the loading to follow the crack path, which is pre-established (*i.e.*, before the experiment). The virtual test is an important contribution to the development and the optimization of the control technique. Equally important is the assessment, from the virtual test, of the feasibility of various crack paths and their figures of merit for identification purposes.

In the present study, a sinusoidal crack path is chosen as the target. The motivations for this choice are numerous:

- changes in propagation directions bring a wealth of information that a straight path cannot reveal, such as mode mixity, damage ahead of the crack tip, or other physical microscale mechanisms affecting crack propagation may be masked by symmetry,
- the periodicity of the sinusoidal shape allows the repeatability of the experiment to be probed, at least approximatively,
- the mean (large scale) crack direction remains straight and hence the path can be kept distant from boundaries,

- the amplitude and wavelength of the path can be tuned to optimise the test.

The paper is organised as follows. First, the general methodology and composition of the 3rd generation test loop are presented with special attention paid to the control algorithm. Then, a virtual test-case with a sinusoidal crack path is shown. The feasibility of the method and the relevance of the choice of the crack path are the main focus of the present work. Last, an application to parameter identification is proposed.

2. Control Principle of the hybrid test

In this section the content of control part of the hybrid loop (see Figure 3), which can be used for real or virtual hybrid tests, is described.

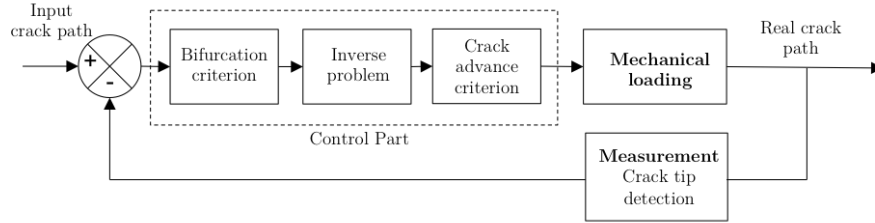


Figure 3: Block diagram of 3rd generation tests

The possible experimental setup is not specified in this work since it could be rather generic, provided that it possesses two important features. First, boundary conditions have to be applied to the specimen using at least two independent degrees of freedom, which influence crack propagation in different ways (otherwise propagation and orientation will not be controlled independently). Second, the measurement of the crack tip position should be possible during crack propagation (otherwise the error calculation will not be possible). For example, a well-instrumented multiaxial testing machine (*e.g.*, hexapod) could

be a suitable candidate to conduct such an experiment [21]. The crack tip measurement may rely on Integrated Digital Image Correlation (I-DIC) using, for example, Williams' series [44, 45, 42], or any other suitable technique.

For a virtual test, the experiment is replaced by a finite element (FE) simulation of crack propagation. In the present case, a non-local damage model is used. The crack tip position is obtained by a damage field analysis, but any other numerical procedure based on, say, FE results could also be considered. The control part is used to find the boundary conditions to obtain the *a priori* chosen crack path, which is established before running the test. It consists of three steps: (1) a deflection angle has to be determined and linked to the stress intensity factors (SIFs), (2) these SIFs have to be converted into boundary conditions, (3) a criterion, which controls the advance of the crack per step, has to be satisfied.

This inverse problem and the evaluation of the SIFs are computed using the 'low-level' model, which is in the present case a Linear Elastic Fracture Mechanics (LEFM) analysis coupled with the geometry updating procedure provided by the eXtended Finite Element Method (X-FEM) [46, 47, 48].

2.1. Crack deflection angle

During mixed-mode propagation, the crack may move away from the chosen path. To correct the path by applying a new loading a deflection angle criterion has to be used. (It is worth noting that this method will not be applicable if the process zone is larger than the crack path curvature, because the crack will not be influenced by the short-term fluctuation of the loading). Let us consider a given crack path and the measured crack propagation, which is simulated by the 'high-level' (*i.e.*, damage) model. In the same spirit as in the field of robotics and automation for a robot following a path [49], a 'look-ahead distance' is chosen. A first idea (Figure 4 (a)) is to look for the intersection between the chosen (input) crack path and a circle of radius dr , which can be considered as a path discretization parameter. This intersection becomes the next target point and the deflection angle is that between the last propagation step and this new

target.

For sufficiently large values of dr it is impossible to describe the full crack path due to its curvature. The shorter dr , the more precise the final crack surface. However, if during the experiment, the ‘real’ crack path happens to be out
 215 of dr circle the procedure may fail. Moreover the smaller dr , the more sensitive to measurement uncertainty, material heterogeneities and propagation fluctuations. Special attention should be paid while choosing dr , namely, smaller than the radius of curvature of the crack path but larger than the process zone.

To address the previous issue, another simpler method is chosen herein. Be-
 220 cause the crack propagation component along the y -axis is small compared with the component along x (*i.e.*, the crack propagates mainly in the x -direction), the circle can be replaced by a straight line parallel to the y -axis, with an offset of $dx \approx dr$. The deflection angle is thus chosen as the angle to reach the intersection between the input crack and the vertical line (see Figure 4 (b)).
 225 The advantage of this simplified procedure is that the algorithm does not fail, even though the determined crack orientation angle is restricted to cracks whose propagation never recedes along the x -axis.

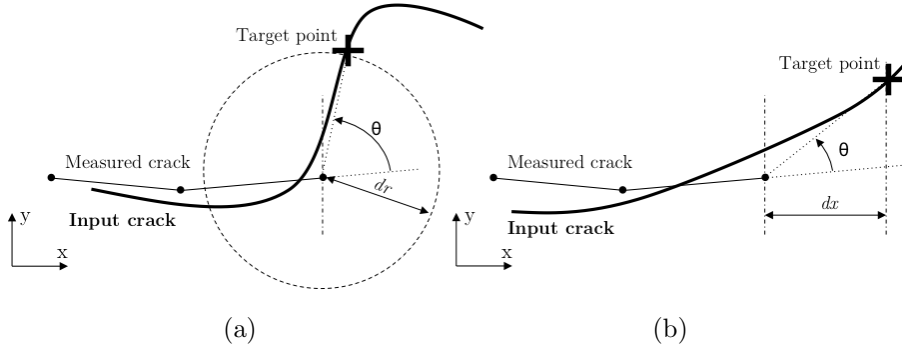


Figure 4: Target point with the two proposed methods, (a) at a distance dr from the previous measured point, and (b) at a projected distance dx on the x -axis

With the chosen procedure and dr set, the predetermined crack path may not be reached if the propagation step is shorter than dr or if the deflection angle reaches its maximum threshold value. Consequently, the crack will follow
 230

in the best case a path that will be called the *command crack path*, namely, the discretised version of the initial input path.

2.2. Inverse problem

In the previous section, an algorithm has been proposed, which allows the
235 deflection angle of the next step to be selected once the crack tip is detected. The purpose is then to get the boundary conditions that generate this angle for further loading. LEFM is assumed to yield a reasonable approximation for small crack propagation increments. Within this theory, in-plane cracks are fully described by two SIFs K_I and K_{II} . Let us stress that such is not the case
240 for what is here considered as the ground truth because of the non-locality of damage. However, in the limit when the internal length scale of the model tends to 0, it is expected that LEFM is recovered.

In the following test-case with a hexapod, three degrees of freedom are used to keep the experiment without significant out-of-plane motion. The other three
245 degrees of freedom correspond to in-plane motions, namely, tension, shear and in-plane rotation applied to the upper part of the sample. However, the latter degrees of freedom are not directly those on which the control conditions are expressed. Rather, the target is to tune the boundary conditions to produce a given SIF pair, which is an inverse problem. However, the two SIFs that control
250 crack propagation are linearly dependent on the sample boundary conditions, and can be bijectively related to two degrees of freedom. One last degree of freedom remains available, and it can be made orthogonal to the previous ones, so that it preserves the SIF pair objective, and the planar character of the test. It is proposed to use this last degree of freedom in order to ensure *stable* crack
255 propagation.

Many methods were developed in the past for crack stability control, starting from the simple SIF gradient or principal stresses analysis, going to more complex force-displacement snap-back identification to finally end up with highly non-linear Rayleigh quotient minimization problem. As a first approximation we limit ourselves to linear elasticity and hence introduce the stability criterion

as some general linear constraint on three in-plane motion amplitudes. The advantage of such description is that the whole relationships remain linear and read as a 3×3 system ($\{\mathbf{k}\} = [\mathbf{S}]\{\mathbf{b}\}$)

$$\begin{Bmatrix} K_I \\ K_{II} \\ \kappa \end{Bmatrix} = \begin{bmatrix} S_I^1 & S_I^2 & S_I^3 \\ S_{II}^1 & S_{II}^2 & S_{II}^3 \\ S_\kappa^1 & S_\kappa^2 & S_\kappa^3 \end{bmatrix} \begin{Bmatrix} b_1 \\ b_2 \\ b_3 \end{Bmatrix} \quad (1)$$

where K_I , K_{II} are the total SIFs that control crack propagation, S_I^i and S_{II}^i the sensitivity matrix elements, *i.e.*, SIFs generated by elementary boundary loadings b_i (*e.g.*, kinematic (translation and rotation), static (force and torque) components), and S_κ^i a set of parameters that defines the stabilising motion constraint

$$\kappa = S_\kappa^1 b_1 + S_\kappa^2 b_2 + S_\kappa^3 b_3 \quad (2)$$

where S_κ^i parameters could be either set during the whole experiment or may vary depending on the crack tip position. The easy way to establish all sensitivity matrix elements $S_{I,II}^i$ is to perform numerical simulations to assess the influence of each elementary loading on the SIFs. To summarise, in order to inverse and solve this system (Equation (1)), three main ingredients are needed, namely, deflection, arrest and stability criteria:

- **Deflection criterion.** Within the LEFM framework it is commonly assumed that, first, the SIF amplitude sets the crack propagation threshold, and second, the SIF ratio K_{II}/K_I influences the crack deflection angle. While many different deflection criteria exist (*e.g.*, maximum normal stress criterion [50], local symmetry criterion [51, 52]), in order to simplify the analysis the deflection angle is given by an implicit function of SIF ratio

$$f(\theta) = \frac{K_{II}}{K_I} \quad (3)$$

- **Arrest criterion.** With the ratio of load amplitude b_i , $i = 1-3$, set by the deflection angle and K_I gradient, a proportional loading is applied until the crack increment length reaches dr . The advantage of this *iterative*

265 *methodology* is that it is directly controlled by the measured quantity
of interest, *i.e.*, the crack length. In another class of possible strategies
(*e.g.*, *prediction method*) the missing equation needed to get the boundary
conditions should be provided. For example, the boundary amplitude may
be chosen to satisfy the LEFM propagation criterion $K_I = K_{Ic}$. One
270 of these additional equations described above is an arrest criterion on
the proportional boundary conditions that controls the incremental crack
advance.

- **Stability criterion.** The stability of the crack is an essential feature
to be taken into account. Ideally (*i.e.*, for a rigid testing machine), it is
275 based on the change of the elastic energy with crack advance [53]. Such
an assumption will be made in the following. In a real test, the rigidity of
the testing machine may have to be taken into account to avoid unstable
crack propagation [54]. Based on experience from real experiments [21],
in our application case, the stabilising condition is set to be the rota-
280 tional loading. The idea is to obtain the crack to open by edge rotation
about the crack tip centre, which creates a relative compression zone in
front of the crack thereby penalising its subsequent sudden propagation
(Figure 5). This empirical procedure helps avoiding the crack to become
unstable and to instantaneously propagate through the ligament. The
285 corresponding loading is a rotation about a moving centre, which should
be close to the crack tip. Represented as a superposition of tension and
fixed centre rotation it could be written within a single linear constraint
(Equation (2)).

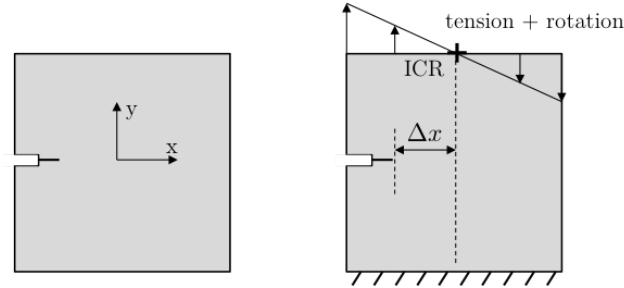


Figure 5: Example of a rotational loading stabilising crack propagation. The distance Δx between the crack tip and the projected instantaneous centre of rotation (ICR) is introduced in the studied case

In the present case, the SIFs related to each boundary condition are computed with an LEFM model and the cracked geometry is updated using the X-FEM framework. The finite element model is enriched by adding degrees of freedom to the concerned elements, which take into account the displacement discontinuities through the crack faces and the stress field singularity in the vicinity of the crack tip. In this study, computations are performed by coupling X-FEM with a level set propagation technique. One of the advantages of such an approach is that the computations are carried out only using the sound mesh.

In summary, the procedure consists of the following steps:

1. From the current and targeted crack path, compute the incremental crack direction, and hence the ratio K_{II}/K_I .
2. Compute $[\mathbf{S}]$ matrix using a low-level model. Exploiting linearity and hence the superposition principle one computation of $\{\mathbf{k}\}$ is needed for each b_i .
3. The desired direction of propagation and the stability heuristic rule provide a direction for vector $\{\mathbf{k}\}$, from which a direction for the loading $\{\mathbf{b}\}$ is derived. (One may choose $K_I = K_{Ic}$ to use a convention that can hold for the entire experiment, although it has no consequence.)
4. Until the crack has propagated by dx , apply the loading $\lambda(t)\{\mathbf{k}\}$ where $\lambda(t)$ is the magnitude of the loading along the direction $\{\mathbf{k}\}$, which is

slowly increased with time.

310 5. Repeat steps 1-4 until the crack has propagated over the desired length.

3. Proof of concept

3.1. Test-case

To show the feasibility of the new method and the identification procedure, the test-case of a concrete sample with a sinusoidal crack path is considered. This test-case is based on the multiple crack deflection experiments presented
315 in Ref. [21]. In these tests, concrete samples have been loaded in a hexapod using tension, shear and in-plane rotation as control variables. The cracks that initiated at the notch propagated slowly while the boundary conditions were manually changed in order to reorient the crack towards the desired angle. The
320 result of such test is a *Z*-shaped (*i.e.*, zigzagged) cracked surface with multiple controlled turns. The following virtual experiment is proposed in the same spirit. Identical specimen geometry and type of loading will be used hereafter. The boundary conditions are applied on the upper face while the lower face is motionless. The kinematic loadings correspond to in-plane rigid body motions, namely, global tension (*i.e.*, translation along *y*), global shear (*i.e.*, translation
325 along *x*) and in-plane rotation.

The specimen is a $200 \times 200 \times 50$ mm³ concrete parallelepiped with a 5×25 mm² notch (see Figure 6).

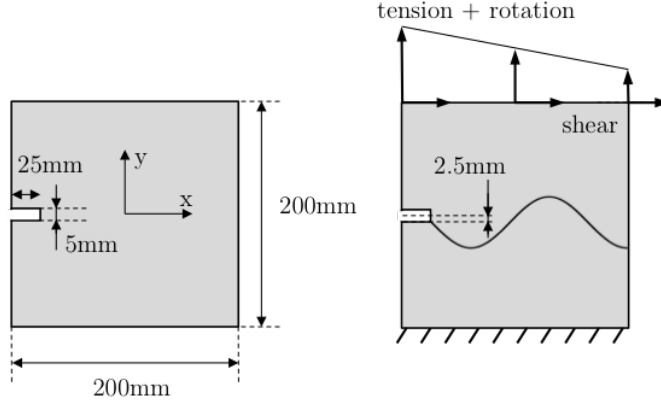


Figure 6: Test-case geometry and possible loading for the sinusoidal crack path

For this virtual test the chosen mechanical parameters are close to real concrete data [21]. The Young's modulus is set to $E = 21$ GPa, the Poisson's ratio to $\nu = 0.2$, the tensile strength to $\alpha = 3.9$ MPa, the compressive strength to $\beta = 8.5$ MPa, the shear strength to $\gamma = 3.25$ MPa, and the Griffith energy to $G_f = 100$ J/m². The input crack path $y_{\text{input}}(x)$ is a sinusoidal function with 1.25 period and an amplitude of 15 mm with an offset of -2.5 mm in order to start in the corner of the notch

$$y_{\text{input}}(x) = -15 \sin \left[2\pi \frac{1.25}{175} (x + 75) \right] - 2.5 \quad (4)$$

The virtual test follows the same principle (see Figure 7) as the real one, namely, the numerical control is the same as used in real tests, the experimental loading device is replaced by a numerical simulation performed using a damage model in order to obtain realistic responses. The assessment of the crack tip is also performed by numerical means. For each iteration i , the crack propagates because of the i -th loading and the final i -th position of the tip is the input in the control part for iteration $i + 1$. Finally the sample is unloaded and the boundary conditions are computed for the next iteration.

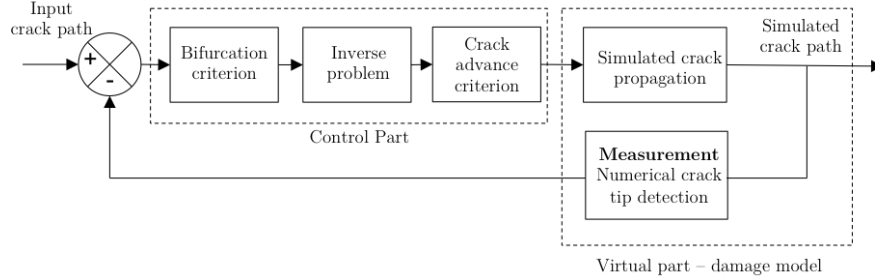


Figure 7: Block diagram of *virtual* 3rd generation tests

Because crack propagation is simulated with a damage model, the crack tip position is numerically found by analysing damage field contours. For a virtual test, the testing machine, the specimen and the measurement can be seen as a
 340 black box where boundary conditions are sent in and a crack path is obtained.

3.2. Deflection criterion

In the following, the simulated crack path and its position will be considered as a true representation of crack tip propagation and the numerical results as experimental reference. The chosen deflection criterion is the maximum normal stress. The crack tip is assumed to turn in the direction where the normal stress ($\sigma_{\theta\theta}$ in a local crack frame) is maximum. The local SIF ratio that has to be applied to the specimen is thus given by (see Equation (3))

$$\frac{K_{II}}{K_I} = \frac{\sin(\theta)}{1 - 3 \cos(\theta)} \quad (5)$$

3.3. Inverse problem

The linear system that uses the boundary conditions to deflect, propagate and stabilise the crack is presented. The three needed boundary conditions are
 345 on the upper face tension b_1 , shear b_2 and a plane rotation about the upper face centre b_3 . In this test-case, the stabilization of the crack path is controlled with a moving Instantaneous Centre of Rotation (ICR) at a determined x position. The x position of the centroid, which depends on tension and rotation, enables

tensile and compressive zones to be created in the sample. In order to stabilise
 350 crack propagation, the ICR has been located at a horizontal distance Δx from
 the crack tip. This distance has to be chosen with caution. It is bounded by

- the prediction of models (*i.e.*, with LEFM, $\Delta x \in [0, \infty]$ to ensure $K_I > 0$
 at the current crack tip)
- the real experimental behaviour (*e.g.*, intermittent propagation of the
 355 crack, heterogeneity)
- the capacity of the machine (*i.e.*, the maximum level of tension, compression
 and torque the hexapod is able to perform)
- the material behaviour in other parts of the sample (*i.e.*, damage on the
 compressive zone and on the edges)

From previous experience [21], it has been chosen to set this horizontal distance
 from the crack tip $\Delta x = 58$ mm. The position $\ell(i)$ of the ICR is thus
 updated for each crack propagation by $\ell(i) = C(i) + \Delta x$ where $C(i)$ is the horizontal
 crack position for the corresponding time step, and $\ell(0) = -16.5$ mm.
 This condition is rewritten as

$$b_1 + \ell(i)b_3 = 0 \tag{6}$$

The linear system (7) that has to be inverted to find the value of the boundary
 conditions reads

$$\begin{Bmatrix} K_I \\ K_{II} \\ 0 \end{Bmatrix} = \begin{bmatrix} S_I^1 & S_I^2 & S_I^3 \\ S_{II}^1 & S_{II}^2 & S_{II}^3 \\ 1 & 0 & \ell(i) \end{bmatrix} \begin{Bmatrix} b_1 \\ b_2 \\ b_3 \end{Bmatrix} \tag{7}$$

When inverting and solving the system with Equation (7), the sought ratio of boundary conditions is obtained

$$\left\{ \begin{array}{l} \left\{ \begin{array}{l} K_I \\ K_{II} \\ 0 \end{array} \right\} = \begin{bmatrix} S_I^1 & S_I^2 & S_I^3 \\ S_{II}^1 & S_{II}^2 & S_{II}^3 \\ 1 & 0 & \ell(i) \end{bmatrix} \left\{ \begin{array}{l} b_1 \\ b_2 \\ b_3 \end{array} \right\} \\ \frac{K_{II}}{K_I} = \frac{\sin(\theta)}{1 - 3 \cos(\theta)} \\ \text{Arrest criterion (e.g., iterative methodology, deflection criterion [50])} \end{array} \right. \quad \begin{array}{l} \text{Inverse problem (7)} \\ \text{Deflection criterion (5)} \\ \text{Arrest criterion (e.g., iterative methodology, deflection criterion [50])} \end{array} \quad (8)$$

360 In the following test-case, the advance of the crack has been set according to the arrest criterion. This corresponds to an advance of the crack by $dx = 6.6$ mm per step $C(n) = C(0) + n \times dx$. A graphical representation of the system is shown in Figure 8 in the (K_I, K_{II}) plane when normalised by the toughness K_{Ic} . The influence of the two boundary conditions is different and complementary,
 365 and a linear combination has to be chosen to get the adequate SIF ratio.

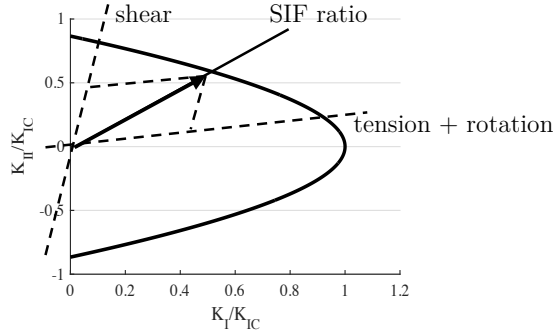


Figure 8: Fracture threshold (maximum normal stress criterion [50]) and influence of the boundary conditions

3.4. Mechanical loading and measurement

For the considered virtual test, a damage model simulates crack propagation. The computation is performed with a non-local damage model [8, 55] suitable for quasi brittle materials like concrete. The model considers the growth of

370 damage as an irreversible process, differentiates compressive/tensile responses, and does not take into account crack closure in the current formulation.

Damage is described by a scalar field $a(\mathbf{x})$ defined on the entire sample, $a = 0$ corresponding to sound material and $a = 1$ to a fully damaged state. With the increase in damage the stiffness of the material, $A(a)$, decreases (*i.e.*, $A(0) = 1$ and $A(1) = 0$). The stress/strain relationship takes into account stiffness loss

$$\boldsymbol{\sigma} = A(a)\mathbf{E} : \boldsymbol{\epsilon} \quad (9)$$

where \mathbf{E} is the stiffness tensor. The following potential functional is used to describe the material state

$$\Phi(\boldsymbol{\epsilon}, a) = A(a)\Gamma(\boldsymbol{\epsilon}) + ka + \frac{c}{2}(\nabla a)^2 \quad (10)$$

where $\boldsymbol{\epsilon}$ is the infinitesimal strain tensor, ka the dissipated energy, and c the parameter that controls the size of the damage localization zone D . The 1D analytical solution [55] opens the way for the parameters k and c to be identified, which can be linked to Griffith energy G_f by

$$k = \frac{3}{4} \frac{G_f}{D} \quad c = \frac{3}{8} DG_f \quad (11)$$

The Γ function is expressed as

$$\Gamma(\boldsymbol{\epsilon}) = \left(c_T \text{tr}(\boldsymbol{\epsilon}) + \sqrt{c_H \text{tr}^2(\boldsymbol{\epsilon}) + c_S \frac{3}{2} \boldsymbol{\epsilon}^{dev} : \boldsymbol{\epsilon}^{dev}} \right)^2 \quad (12)$$

where c_H , c_T and c_S are numerical parameters that can be identified from three physical measurements, namely, the triplet of tensile strength, compressive strength and shear strength.

The yield surface is obtained by deriving the functional Φ with respect to the damage field $a(\mathbf{x})$

$$f(\boldsymbol{\epsilon}, a) = -\frac{\partial \Phi}{\partial a} \quad (13)$$

The consistency (Kuhn-Tucker) conditions read

$$f \leq 0, \quad \dot{a} \geq 0, \quad \dot{a}f = 0 \quad (14)$$

375 The elastic domain $f(\epsilon, 0) = 0$ is an ellipsoid of revolution defined by $\Gamma(\epsilon) =$ constant. The real yield surface [56] of concrete is described in the tension-shear domain by adjusting the model parameters (Figure 9)

$$\begin{aligned}
 c_T &= \sqrt{\frac{E}{2}} \frac{\alpha}{1-2\nu} \left(\frac{1}{2\alpha} - \frac{1}{2\beta} \right) \\
 c_H &= \frac{\alpha^2 E}{(1-2\nu)^2} \left[\left(\frac{1}{2\alpha} - \frac{1}{2\beta} \right)^2 - \frac{1}{3\gamma^2} \right] \\
 c_S &= \frac{E\alpha^2}{6\gamma^2(1+\nu)^2}
 \end{aligned} \tag{15}$$

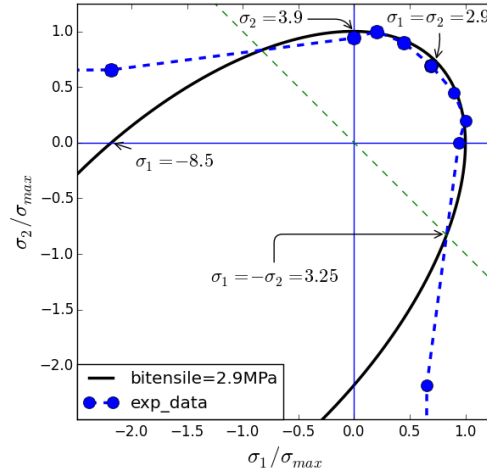


Figure 9: Elastic domain (plane stress) shape in the bitensile quadrant of the experimental data for concrete [56]

Last, the stiffness loss function $A(a)$ defines the post-peak behaviour of the material. It is written by using two parameters

$$A(a) = \frac{(1-a)^2}{(1-a)^2 + ma(1+pa)} \tag{16}$$

where m defines the initial damage rate

$$m = \frac{3EG_f}{2D\alpha^2} \tag{17}$$

The parameter p is more important as it influences the size of the process zone. The identification of the latter is very challenging for classical fracture
380 experiments. That is why the identification presented in the next section will deal with this scalar parameter.

For the computations, the numerical parameter D has to be adapted to the size of the mesh to cover at least 3 elements inside the damaged zone of size $2 \times D$ (*i.e.*, finer meshes are not needed as the results converge quickly to a
385 cohesive zone response [55]). In the current study D is set to 1 mm and the length scale p to 1.5. The mesh is composed of 31,296 6-noded triangular (T6) elements with an average size equal to 1 mm.

The damage model is implemented in Code_Aster [57]. The measurement of the crack tip is obtained at each step from the damage field with the Code_Aster
390 module Post_Endo_Fiss [58]. With this method, the crack path is detected when the damage level is greater than a characteristic threshold. During each iteration, the new crack tip is detected and injected in the control part. Consequently the crack geometry has to be updated after each propagation increment. The threshold on the damage variable to detect the crack is set to $a = 0.1$.

In this study with a numerical simulation of the crack path, the arrest cri-
395 terion is an iterative method based on a certain amount of damage increase per increment. This is possible to obtain since a numerical simulation is used and coupled with the damage control continuation method implemented in Code_Aster [59]. This functionality is very convenient since the position of
400 the crack tip cannot be known on the fly during loading with the FE code. The crack tip position and the damage level are strongly linked with the crack propagation length per iteration, as will be shown in the next section.

3.5. Results

Once the 33 reorientation iteration steps have converged, the last thin lig-
405 ament tends to break in an unstable manner and can no longer be controlled. The result obtained after all 33 steps is shown for the horizontal and vertical displacement fields in Figure 10 and the crack propagation path in Figure 11.

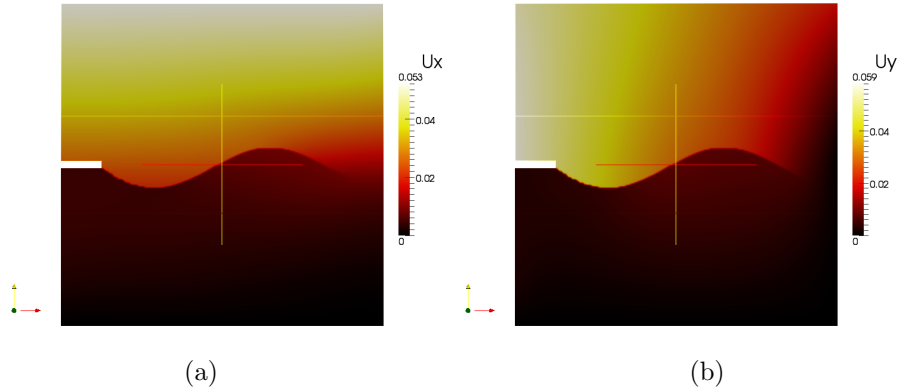


Figure 10: Displacement field at the end of the virtual sine test. (a) Horizontal (x -axis), and (b) vertical (y -axis) components

In Figure 11, the target crack path and that obtained by the simulated procedure (red circle) are compared. Even if there is a visible deviation between
 410 both crack paths, it is observed that the simulated path is close to the target. The mean relative error is 6.3 %, which is deemed acceptable.

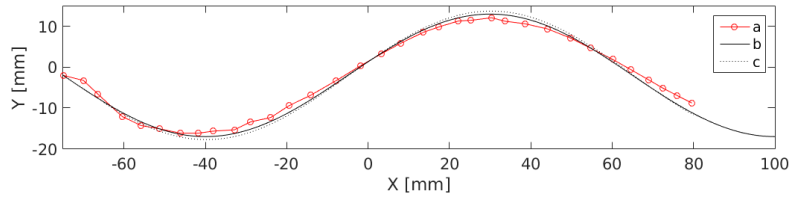


Figure 11: Comparison between (a) the measured crack path, (b) the target crack path, and (c) the input crack (never reached because of the step discretization)

The maximum displacement of the top left and right corners of the sample applied for each increment before unloading is reported in Figure 12. Even if a global sinusoidal shape can be seen on the shear boundary conditions, the
 415 precise loading history is not trivial and hence not easily guessed *a priori*.

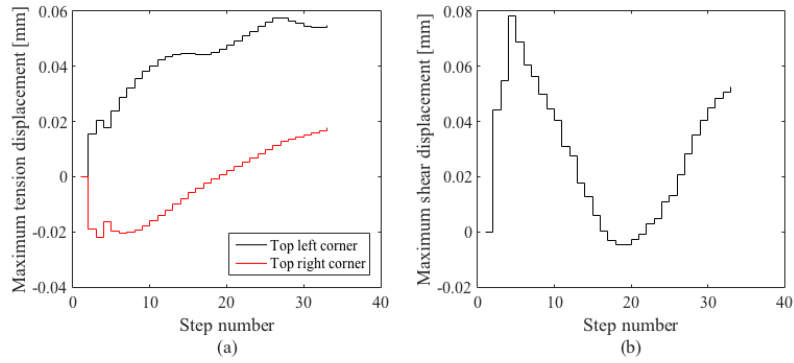


Figure 12: Maximum applied displacement at the top left and right corners of the sample vs. step number. (a) Tension on the top left corner (positive values) and on the top right corner, and (b) shear (uniform)

The crack length for each iteration is plotted in Figure 13. The increase of the crack length and the variation of boundary conditions mean that the crack continuously turns during the experiment.

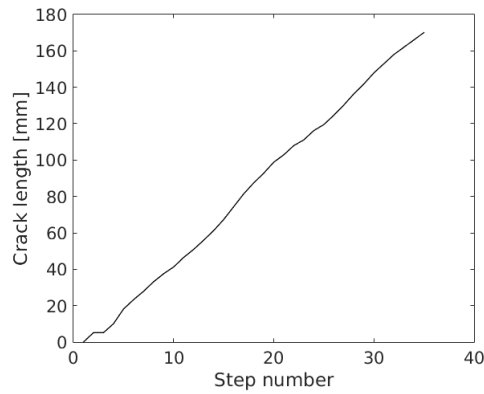


Figure 13: Total crack length vs. step number

The length of the crack vs. the number of increments is close to a linear curve.
 420 The mean crack advance is found to be ≈ 5 mm per iteration. This length does not exactly correspond to the advance of the ICR (≈ 6.6 mm). Even if the tensile

gradient slightly decreases during the test, it is still important to stabilise the crack. During propagation, the mean absolute value of the deflection angle is $\langle |\theta| \rangle = 6^\circ$, *i.e.*, the crack does not rotate much for each iteration because of
425 small propagation increments and the rather smooth prescribed crack path.

With the help of the iterative procedure the inverse damage problem is solved recursively, *i.e.*, the boundary conditions (Figure 12) could be directly applied to the sample from the start until the end (*i.e.*, 33rd step) to obtain the desired sinusoidal path if the behaviour of the machine and the specimen were exactly
430 those of the numerical simulation.

The question of the relationship between the ‘low-level’ and ‘high-level’ models is worth mentioning. In the present case, it is natural to observe that if the internal length scale of the model is much smaller than all characteristic sizes of the problem (here the smallest crack path radius of curvature), the high-
435 level model becomes identical to the low-level one, that is LEFM. Hence a very good control is expected, unless precisely when the internal length scale plays a significant role, and hence the present approach naturally provides a very discriminating tool to reveal such model enrichment as explored in the following subsection.

440 However, one may wonder whether a cruder ‘low-level’ model may still provide a viable route to experimentally control such a sinuous crack path. To this end, a very poor version of the ‘low level’ model has been used to test the control principle. Instead of an LEFM prediction, a simple proportional-integral (PI) controller with incremental change of the shear stress and a constantly growing
445 tension/rotation permits us to drive the crack as desired during the first 12 steps. However the inaccuracies of this low level model produce spurious damage patterns from which a secondary crack may branch whenever the main crack path reaches some unfavourable direction. More details are shown in Appendix A. The feasibility of the iterative control of a crack propagation, even though
450 limited, is proved.

4. Application to identification

The aim of the testing procedure is to be sensitive enough to the model parameters to enable for their identification. A rough estimate of the sensitivity to the length scale can be directly obtained from the analysis of the crack path trajectory with respect to the studied parameter variation. As shown in Figure 14 the crack path is sensitive to the length scale parameter p , but it is difficult to assess its best fit value, as its variation is really important (*i.e.*, a factor of 3).

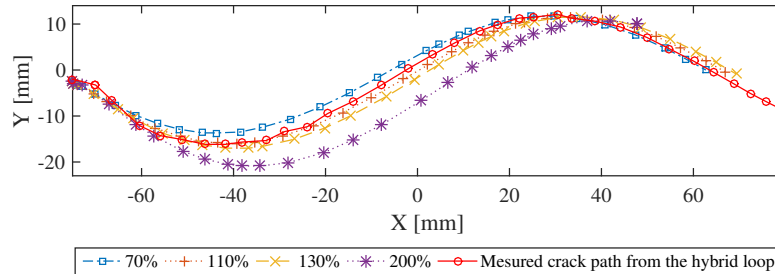


Figure 14: Crack path sensitivity to the length scale parameter p

For a more quantitative analysis, an identification procedure must be performed. The previous test-case will be used for identification purposes with artificial noise added in order to prove its robustness.

4.1. Global DIC

In practice, a global DIC approach [60] will be used to measure the displacement field for identification purposes [61]. It consists of the registration of an image $f(\mathbf{x})$ in the reference configuration and a series of pictures $g(\mathbf{x}, t)$ in the deformed configuration indexed by time t . The correlation code minimises

the sum of squared differences between the deformed image corrected by the measured displacement $\mathbf{u}(\mathbf{x}, t)$ and the reference image

$$\chi_f^2(t) = \frac{1}{2\gamma_f^2|\Omega|} \sum_{\Omega} ((g(\mathbf{x} + \mathbf{u}(\mathbf{x}, t), t) - f(\mathbf{x}))^2 \quad (18)$$

with respect to the nodal displacement vector $\{\mathbf{u}_m\}$ of a finite element mesh defined by the shape functions Φ_i and unknown degree of freedom u_i such that
465 $\mathbf{u}(\mathbf{x}, t) = \sum_i \Phi_i(\mathbf{x})u_i(t)$, where $\mathbf{x} \in \Omega$ is any considered pixel, Ω the Region Of Interest (ROI) and γ_f the standard deviation (expressed in grey levels) of the Gaussian white noise assumed to affect each image independently (including the reference one, which is responsible for the factor 2).

The minimization of this functional is solved by successive linearisations and corrections using modified Gauss-Newton scheme [62]

$$[\mathbf{M}]\{\delta\mathbf{u}_m\} = \{\mathbf{b}\} \quad (19)$$

where $[\mathbf{M}]$ is the DIC matrix, $\{\delta\mathbf{u}_m\}$ the vector gathering all corrections to the measured degrees of freedom, and $\{\mathbf{b}\}$ the residual column vector, which cancels out when the grey level conservation is satisfied everywhere. Since the measured displacement field is corrupted by noise, the DIC matrix is related to the covariance matrix $[\mathbf{C}_u]$ of the measured degrees of freedom by [60]

$$[\mathbf{C}_u] = 2\gamma_f^2[\mathbf{M}]^{-1} \quad (20)$$

Once a discretization has been chosen for displacement field measurements,
470 and the level of acquisition noise is known, this derivation gives access to the sensitivity of the measured degrees of freedom to acquisition noise [62].

4.2. Weighted FEMU

Several identification methods have been adapted or developed to quantitatively use full field measurement results to calibrate material parameter [63, 61].
475 The most used method is Finite Element Model Updating (FEMU), which is based on the minimization of the differences between the measured quantities (*i.e.*, forces \mathbf{F}_m and displacement fields \mathbf{u}_m) and the corresponding computed

quantities from a numerical simulation, namely, \mathbf{F}_c and \mathbf{u}_c . This simulation, which utilises a constitutive model, is performed with Dirichlet boundary conditions extracted from, say, DIC analyses.

Weighted displacement-based FEMU (*i.e.*, FEMU-U) consists in computing the set of (dimensionless) constitutive parameters $\{\mathbf{p}\}$ that minimises the functional χ_u^2 [62]

$$\chi_U^2 = \frac{1}{N_u} \{\mathbf{u}_m - \mathbf{u}_c\} [\mathbf{C}_u]^{-1} \{\mathbf{u}_m - \mathbf{u}_c\} \quad (21)$$

where χ_U^2 is the weighted squared difference between the measured and calculated displacements, and N_u the total number of kinematic degrees of freedom. The weighted chi-squared error therefore refers to the $[\mathbf{M}]$ -norm associated with the DIC matrix (up to a constant prefactor $1/(2\gamma_f^2)$).

The reaction forces may also be measured and computed. Thus, the same approach is followed with the reaction forces for which χ_F^2 is minimised (FEMU-F) [62]

$$\chi_F^2 = \frac{1}{N_F} \{\mathbf{F}_m - \mathbf{F}_c\} [\mathbf{C}_F]^{-1} \{\mathbf{F}_m - \mathbf{F}_c\} \quad (22)$$

where N_F is the number of load measurements and $[\mathbf{C}_F]$ the covariance matrix of the measured load (in the present case it is assumed that the load measurements are uncorrelated so that $[\mathbf{C}_F] = \gamma_F^2 [\mathbf{I}]$, with γ_F the standard load uncertainty and $[\mathbf{I}]$ the identity matrix).

The identification based on the combined displacement field and reaction force (FEMU-UF) [64] is achieved by minimising the global functional χ_{UF}^2 in a Bayesian framework [62]

$$\chi_{UF}^2 = \frac{N_u}{N_u + N_F} \chi_u^2 + \frac{N_F}{N_u + N_F} \chi_F^2 \quad (23)$$

4.3. Comparison of two different tests

The so-called Nooru-Mohammed tests [65] have become a reference for mixed mode propagation of cracks in quasi brittle samples. One of these crack paths will be chosen to be compared with the sinusoidal path obtained with the present method. The input data for identification purposes are the measured boundary

conditions of the sample (*i.e.*, force and displacement field). These bound-
495 ary conditions applied to the top and bottom surface are known for a Nooru-
Mohammed test. The material and behaviour are the same as in the sinusoidal
test-case. A double notched sample is analysed. The most used crack path of
all Nooru-Mohammed tests is the number 5. As in the real Nooru-Mohammed
test, the load starts with shear up to 10 kN, then the sample is loaded with a
500 tensile displacement while maintaining constant the shear force. This load leads
to a curved crack path in mixed mode I and II.

Table 1: Parameter values

Parameter	p	ν	β	G_f	E	γ	α
Units	–	–	(MPa)	(J/m ²)	(GPa)	(MPa)	(MPa)
Value	1.05-3	0.2	8.5	100	20	3.25	3.9
Number	1	2	3	4	5	6	7

The predicted behaviour is simulated with the non-local damage law presented previously. In the following the most difficult parameter to identify, namely, the length scale p that controls the size of the process zone, is studied. The other parameters (*i.e.*, E , ν , α , β , γ and G_f), which can be more easily identified with standard tests are assumed to be known. The values of the parameters are reported in Table 1. Even though the experiment has not been performed yet, it is possible to analyse its sensitivity to various quantities (*e.g.*, material parameters, sample geometry, loading path). The sensitivity analysis can be performed on any of the three identification residuals (*i.e.*, χ_u^2 , χ_F^2 , χ_{uF}^2 , see Refs. [66, 67]). In the present case, the dimensionless Hessian is computed when only kinematic data are considered

$$[\mathbf{H}_u] = [\mathbf{S}_u]^t [\mathbf{C}_u]^{-1} [\mathbf{S}_u] \quad (24)$$

with

$$\{\mathbf{S}_u\}_i = \{\mathbf{u}_c(p_i + \delta p)\} - \{\mathbf{u}_c(p_i)\} \quad (25)$$

where $\{\mathbf{S}_u\}_i$ denotes the column vector of displacement sensitivities with respect to the i -th material parameter when δp is equal to 10% of p_i . The eigenvalues

of $[\mathbf{H}_u]$ are very helpful to probe the sensitivity of a given experimental con-
 505 figuration to the chosen parameters $\{\mathbf{p}\}$ [66]. If only the length of the process
 zone parameter (*i.e.*, p) is studied, the diagonal component p of the dimension-
 less Hessian $[\mathbf{H}_u]$ is to be compared. In the present case, its level is equal to
 1.5×10^{-3} for the Nooru-Mohammed test, and 9.0×10^{-2} for the proposed
 experiment. The norm of the sensitivity for the length scale parameter is 59
 510 times higher for the sinusoidal test, which proves the interest of such test.

More globally, the spectrum of eigenvalues associated with the dimensionless
 Hessian $[\mathbf{H}_u]$ can be compared to probe the global sensitivity of the two exper-
 iments to the whole set of material parameters for the chosen damage model
 (*i.e.*, the higher any eigenvalue, the more sensitive the experiment). Figure 15
 515 shows the spectrum for the two configurations. On average there is a two or-
 der of magnitude difference in favour of the new configuration. These results
 show that the new configuration is significantly more sensitive to the material
 parameters.

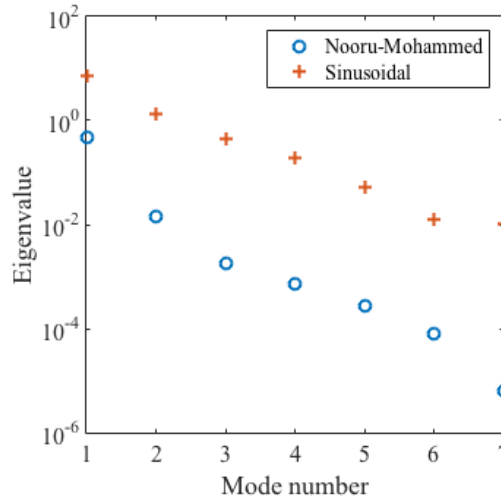


Figure 15: Comparison of the 7 eigenvalues of $[\mathbf{H}_u]$ with a sinusoidal test and Nooru-Mohammed test

The coupling between the parameters is analysed with the covariance nor-

malised by the diagonal terms. The corresponding correlation matrix is formed (with no index summation)

$$[\tilde{H}_u^{-1}]_{ij} = \frac{[H_u^{-1}]_{ij}}{\sqrt{[H_u^{-1}]_{ii}}\sqrt{[H_u^{-1}]_{jj}}} \quad (26)$$

For the sinusoidal crack path the correlation matrix shows an anti-correlation
 520 between the Poisson's ratio and the scale parameter p . The correlation matrix for the Nooru-Mohammed test (obtained with the same mesh) appears to be strongly coupled whereas the sinusoidal experiment is less coupled (Figure 16).

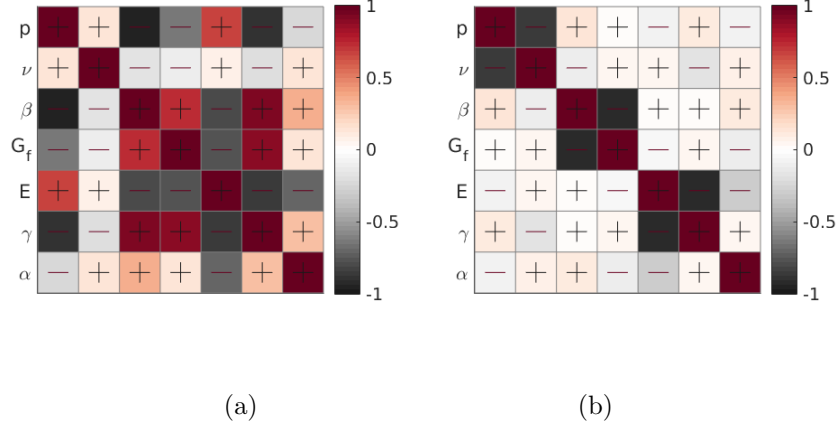


Figure 16: Correlation matrix for (a) the Nooru-Mohammed test (b) the sinusoidal experiment

To probe the noise sensitivity of the proposed identification procedure with the sinusoidal test-case, displacement uncertainties η_u and force uncertainties
 525 η_F have been added to the numerical noiseless results prior to the identification step. For the displacement field, a DIC computation of a reference image representative of the proposed test (extracted from a real test [21]) is run with the same image for which white Gaussian grey level noise is added. The grey level noise has a standard deviation γ_f equal to 0.6 % of the dynamic range
 530 (*i.e.*, difference between maximum and minimum grey levels) of the reference image. The corresponding nodal displacement due to acquisition noise $\{\eta_u\}$ is added to the 'measured' displacement field $\{u_c\}$. To summarise, the displace-

ment error is obtained with the normalised quadratic difference between the reference displacement field considered as the measured one (with parameter p and corrupted by the noise) and the computed field (with $p + \delta p$).
535

For the force uncertainty, γ_F is assumed to be proportional to the magnitude of the load level with a coefficient ρ_1^2 [68]. A minimum uncertainty for the load cells is included whose variance ρ_0^2 is independent of the load level so that the load uncertainty reads

$$\gamma_F^2 = \rho_1^2 |F|^2 + \rho_0^2 \quad (27)$$

where the parameters, which are representative of nowadays cameras and load cells, are given in Table 2.

Table 2: Parameters for the analysis of noise sensitivity

γ_f	ρ_1	ρ_0
0.6% of 8-bit images = 2 grey levels	4×10^{-4}	30 N

For different values of the parameter p ranging from 70% to 200% of the initial reference value (*i.e.*, $p = 1.5$), the FEMU-UF functional is plotted in
540 Figure 17. The shape of the functional for the sinusoidal path is much steeper than for Nooru-Mohammed’s case. This means that the sinusoidal crack path is more sensitive to the length scale p and less to noise. Hence the identification procedure will converge more precisely and faster [69].

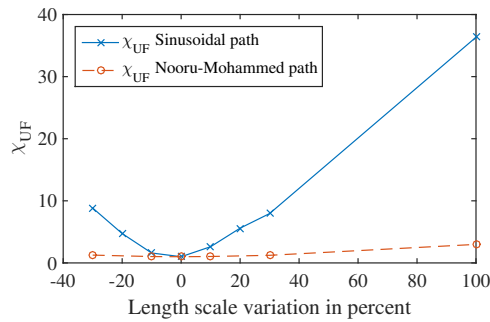


Figure 17: Weighted norm of the error χ_{UF} as a function of the length of the process zone for the two test configurations

5. Conclusion

545 This paper presented an experimental procedure to perform tests with new quantities of interest (*e.g.*, SIF, crack tip position) in order to validate models and calibrate their parameters. A virtual test-case has shown the feasibility of the described method by following a sinusoidal crack path on a concrete sample. The loading was in tension, shear and in-plane rotation and crack propagation 550 was simulated with a non-local damage model. The extracted boundary conditions enable the sensitivity of this crack path to be assessed relative to a more standard crack path for mixed mode crack propagation in quasi brittle materials. It has been shown that the crack path obtained with the proposed method was about two orders of magnitude more sensitive especially for the length scale 555 identification.

The sinusoidal shape has been arbitrarily selected and was not optimised for identification purposes. The use of the proposed virtual method allows different crack paths to be analysed very quickly. An optimization step of the crack path for the identification of a specific parameter can be performed based on the 560 presented framework [66]. Last, achieving real 3rd generation tests is the next step of the present study to calibrate internal length scales of damage models, which are very difficult to estimate with current tests and procedures.

Acknowledgement

The support of CNRS (French National Centre for Scientific Research) for 565 the CONCRET project is gratefully acknowledged.

Appendix A

To go along the same lines as Section 3 but exploring yet a cruder example of low level prediction, a poor version of the control model has been tested in the same spirit as the manual tests performed by Carpiuc *et al.* [21]. Instead of 570 working with an LEFM prediction, the control was performed by an incremental

change of the shear component U_s and a constantly increasing tensile/rotation component (Figure 18).

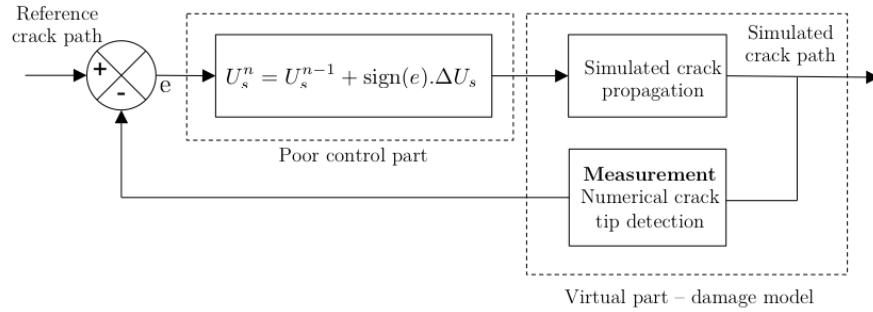


Figure 18: Control loop of the crack path with a low level (PI) control model. U_s is the shear displacement boundary condition, which is mainly responsible for the deflection of the crack, and ΔU_s an elementary variation of the shear component

The results are that the deflection of the crack is less smooth and creates bifurcation zones. However, for small increments, the control of the 'high level
 575 model' was performed by a simple proportional integral (PI) corrector (as a qualitative illustration, see Figure 19). Such a control strategy provides an acceptable response for the main crack up to an inflection point of the trajectory.

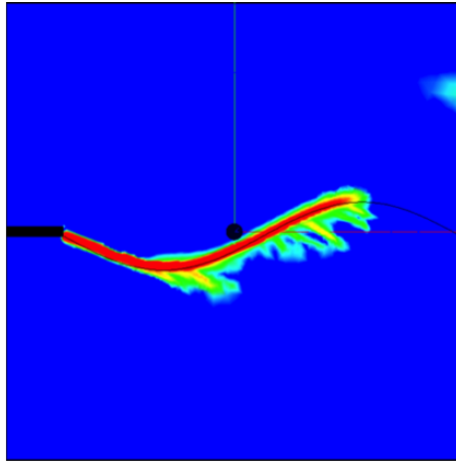


Figure 19: Damage field (red is for the damage variable greater than 0.95) with multiple branching zones for a crack controlled with the 'low level' (PI control) model

However, because of the distance to the actual physics of the problem, more damage accumulates on the concave side of the crack. Past the inflection point
 580 for the main crack trajectory, these damaged zones act as secondary branching points, and thus prevent us from controlling the crack path until its very end. This result illustrates the benefit of having a low level model that is close enough to the expected ground truth.

Last, let us note that for the inversion of a non-linear control model, the
 585 implementation of a Gauss-Newton routine, for example, may solve the problem with successive updated sensitivities on the boundary conditions.

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