## **Supporting Information**

## Burgess et al. 10.1073/pnas.1317692111

## SI Text

The calculated weighed mean <sup>206</sup>Pb/<sup>238</sup>U dates from this study are younger than dates on the same ash beds published in ref. 1 by up to 0.2% (Table S1 and Fig. S2). This difference is 7-9 times the uncertainty associated with each weighted mean date. Here we explore possible explanations. To eliminate any potential issues with sample heterogeneity, we used the same mineral separates that were analyzed for ref. 1 and chose morphologically similar, high aspect ratio zircons. Both studies yield a similar distribution of single grain dates with an approximately normal distribution of errors [mean square of weighted deviates  $(MSWD) \cong 1$  when the few outliers interpreted to be the result of inheritance (n = 10/61) are excluded, and it is assumed that chemical abrasion effectively eliminates Pb loss in most cases. We consider it unlikely that the younger weighted mean dates seen in this work are the result of a selection bias or systematic Pb loss in multiple populations of zircon.

The data for ref. 1 were acquired in 2006, in the early stages of the EARTHTIME initiative. Since that time, there have been significant changes in the way U-Pb data are acquired and reduced at Massachusetts Institute of Technology and in other laboratories. These changes include the following. (*i*) New values for the isotopic compositions and purity of U and Pb standards used to calibrate the EARTHTIME tracer solution and new algorithms to determine this composition, which improves the accuracy of the solution calibration relative to the MIT1L calibration by ref. 2 and used in ref. 1. The new calibration reflects the ~5 permil change in the <sup>238</sup>U/<sup>235</sup>U values for CRM112a determined by ref. 3, which leads overall to a decrease in a single <sup>206</sup>Pb/<sup>238</sup>U date of ~0.05%. (*ii*) As a result of tracer calibration, we refined the <sup>18</sup>O/<sup>16</sup>O ratio used for UO<sub>2</sub> measurements, which results in a value ~2.5% greater than that used to reduce the data in ref. 1 and a 0.025% decrease (~60 ka) in a typical

- 1. Shen SZ, et al. (2011) Calibrating the end-Permian mass extinction. *Science* 334(6061): 1367–1372.
- Schoene B, Crowley JL, Condon DJ, Schmitz MD, Bowring SA (2006) Reassessing the uranium decay constants for geochronology using ID-TIMS U–Pb data. Geochim Cosmochim Acta 70(2):426–445.
- Condon DJ, McLean N, Noble SR, Bowring SA (2010) Isotopic composition (238U/235U) of some commonly used uranium reference materials. *Geochim Cosmochim Acta* 74 (24):7127–7143.

single-grain <sup>206</sup>Pb/<sup>238</sup>U date. (iii) Refined estimates of the isotopic composition and dispersion in the laboratory blank, which includes additional measurements and a revised algorithm to calculate composition, indicate that the composition used in ref. 1 was not as accurate as the values used in this study and that the uncertainties were underestimated. For example, applying the composition and uncertainty used by ref. 1 to data from bed 25 generated for this study results in an increase of the weighted mean <sup>206</sup>Pb/<sup>238</sup>Pb date by 35 ka, with a 27% decrease in analytical uncertainty. (iv) New algorithms were used for point by point interference correction on masses 201-205. (v) Point by point fractionation corrections for Pb were used using the EARTHTIME 202-205-233-238 tracer rather than application of a single value for  $\alpha$ -Pb based on long-term monitoring of National Bureau of Standards 981, 982, and synthetic zircon solutions with ET535 added, which was done in ref. 1. We suggest that the fractionation correction used in this study likely reduces scatter in <sup>206</sup>Pb/<sup>238</sup>U dates caused by assuming a constant value and uncertainty. (vi) New algorithms were used for determining and propagating uncertainties into a weighted mean date (4, 5). The dates in ref. 1 cannot simply be recalculated to independently incorporate one or all of the above changes, and thus the relative effects of each cannot be evaluated.

The nonlinear difference between dates also suggests that the subjectivity of data reduction and other factors such as the response of zircon to chemical abrasion and/or subtle, unaccounted for interference corrections, may play a role. Application of these improvements yield significantly improved accuracy and precision on the weighted mean and interpolated dates (Fig. S2 and Table S2). This improvement is particularly evident for bed 33, on which no mean was calculated by ref. 1 due to excess scatter, which is likely due to residual Pb-loss (Fig. S2).

- McLean N, Bowring J, Bowring S (2011) An algorithm for U-Pb isotope dilution data reduction and uncertainty propagation. *Geochem Geophys Geosyst* 12(6):1–26.
- 5. Bowring JF, McLean NM, Bowring SA (2011) Engineering cyber infrastructure for U-Pb geochronology: Tripoli and U-Pb\_Redux. *Geochem Geophys Geosyst* 12(6): 1–19.



Fig. S1. Stratigraphy, geochronology, carbonate carbon isotopic composition, and composite ocean paleotemperature for the extinction interval at the Global Stratotype Section and Point (GSSP), Meishan, China. Stratigraphy and carbonate carbon isotopic composition are from Cao et al. (1). Paleotemperature is from Joachimski et al. (2).

1. Cao C, et al. (2009) Biogeochemical evidence for euxinic oceans and ecological disturbance presaging the end-Permian mass extinction event. *Earth Planet Sci Lett* 281(3-4):188–201. 2. Joachimski MM, et al. (2012) Climate warming in the latest Permian and the Permian-Triassic mass extinction. *Geology* 40(3):195–198.



**Fig. S2.** Comparison of single-grain zircon analysis from beds 22, 25, 28, and 33. Dates from ref. 1 are in dark gray and from this study are in light gray. Each vertical bar represents a single zircon analysis, the height of which is proportional to the  $2\sigma$  analytical uncertainty on that analysis. The thin horizontal bar through the middle of each population of analysis represents the weighted mean calculated date for that bed, which is surrounded by the  $2\sigma$  analytical uncertainty on this date. Thick horizontal lines passing through the diagram are the calculated maximum extinction duration (beds 25–28) and are keyed by color to the respective study.

1. Shen SZ, et al. (2011) Calibrating the end-Permian mass extinction. Science 334(6061):1367-1372.

Table S1. Difference in <sup>206</sup> Pb/ <sup>238</sup> U weighted mean dates for Meishan ash beds from this study and from ref	. 1
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Sample	Shen et al. 2011	n; MSWD	Mya*	n; MSWD	∆Date (Mya)
Bed 22-MZ96 (–4.3)	252.50 ± 0.11	(8; 0.8)	252.104 ± 0.060/0.28	(12, 0.50)	0.49 ± 0.125
Bed 25-MBE0203	252.28 ± 0.08	(13; 1.9)	251.941 ± 0.037/0.28	(16; 1.3)	0.34 ± 0.088
Bed 28-MBE0205	252.10 ± 0.06	(7; 1.4)	251.880 ± 0.031/0.28	(13; 0.76)	0.22 ± 0.067
Bed 33-MD99-33u	No age interpretation	Not applicable	251.583 ± 0.086/0.29	(9, 0.86)	None

\*Uncertainty reported is  $2\sigma$  internal (analytical)/external. External uncertainty includes uncertainty associated with tracer calibration and  $^{238}$ U decay constant. Uncertainty on differences is added in quadrature from  $2\sigma$  analytical uncertainty on dated beds.

1. Condon DJ, McLean N, Noble SR, Bowring SA (2010) Isotopic composition (238U/235U) of some commonly used uranium reference materials. Geochim Cosmochim Acta 74:7127-7143.

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Table S2.	U-Pb isot	topic da	ta and si	ngle-grain z	ircon dat	tes												
	Compc	osition					ls	otopic rat	ios						ates (Mya)			
Sample and fraction	Pb* (pg)†	Pbc (pg) <sup>‡</sup>	Th/U§	206Pb/ 204Pb¶	208Pb/ 206Pb <sup>II</sup>	206Pb/ 238U <sup>II</sup>	±2s %	207Pb/ 235U <sup>II</sup>	±2s %	207Pb/ 206Pb <sup>II</sup>	±2s %	Correlation coefficient	206Pb/238U <th>**f</th> <th>±2s absolute<sup>††</sup></th> <th>207Pb/ 235U<sup>‡‡</sup></th> <th>±2s absolute<sup>††</sup></th> <th>Correlation coefficient</th>	**f	±2s absolute <sup>††</sup>	207Pb/ 235U <sup>‡‡</sup>	±2s absolute <sup>††</sup>	Correlation coefficient
MD99-33u (bed 33)		, ,	7				7		, ,				C L C	1 1 1 1				
17	117.01	510.0	0./42	100.051	CC7.0	0.040	0.1	0.204	007.1	70.0	007.	0.240	610.107	C/7.0	100.007	070.2	0.240	
z2	9.475	0.839	0.592	679.826	0.187	0.040	0.125	0.283	1.351	0.052	1.329	0.221	251.630	0.309	252.952	3.025	0.221	
z4	9.275	0.663	0.827	790.601	0.262	0.040	0.102	0.281	1.164	0.051	1.145	0.226	251.684	0.252	251.842	2.595	0.226	
z5	5.586	0.552	0.644	603.426	0.204	0.040	0.135	0.280	1.531	0.051	1.505	0.238	251.513	0.334	251.029	3.406	0.238	
z6	5.995	0.617	0.730	568.289	0.231	0.040	0.139	0.281	1.631	0.051	1.606	0.221	251.607	0.344	251.619	3.636	0.221	
29	12.836	0.523	0.717	1411.322	0.227	0.040	0.065	0.282	0.644	0.051	0.631	0.244	251.486	0.159	252.017	1.437	0.244	
z11	8.236	0.745	0.655	655.293	0.207	0.040	0.128	0.284	1.392	0.052	1.370	0.221	251.705	0.315	253.751	3.126	0.221	
z16	8.950	0.567	0.683	922.383	0.216	0.040	0.086	0.283	0.984	0.052	0.967	0.231	251.741	0.212	253.161	2.204	0.231	
z17	7.186	0.762	0.733	551.292	0.232	0.040	0.144	0.279	1.689	0.051	1.658	0.253	251.371	0.356	249.986	3.743	0.253	
MBE0205 (hed 28)																		
z1	95.822	0.313	0.478	18513.842	0.151	0.040	0.051	0.282	0.085	0.051	0.059	0.709	251.956	0.126	251.993	0.190	0.709	
z4	12.658	0.442	0.723	1641.269	0.228	0.040	0.059	0.282	0.558	0.051	0.548	0.220	251.886	0.147	252.277	1.247	0.220	
z6	18.890	0.958	0.592	1172.719	0.187	0.040	0.071	0.282	0.776	0.051	0.763	0.226	251.823	0.176	251.903	1.730	0.226	
z8	37.429	0.562	0.607	3904.118	0.192	0.040	0.037	0.282	0.237	0.051	0.232	0.216	251.862	0.091	251.996	0.530	0.216	
z11	27.572	0.530	0.684	2997.531	0.216	0.040	0.036	0.281	0.305	0.051	0.299	0.208	251.875	0.089	251.842	0.680	0.208	
z12	11.461	0.574	0.731	1147.501	0.231	0.040	0.075	0.281	0.796	0.051	0.781	0.248	251.762	0.186	251.586	1.774	0.248	
z13	17.787	0.983	0.465	1114.532	0.147	0.040	0.077	0.281	0.821	0.051	0.808	0.213	251.838	0.190	251.845	1.830	0.213	
z16	23.831	0.578	0.548	2460.545	0.173	0.040	0.041	0.282	0.368	0.051	0.361	0.204	251.948	0.101	252.389	0.822	0.204	
z17	26.153	0.529	0.500	2987.040	0.158	0.040	0.039	0.282	0.302	0.051	0.299	0.149	251.955	0.096	252.295	0.676	0.149	
z18	19.001	0.388	0.660	2840.031	0.209	0.040	0.040	0.282	0.322	0.051	0.316	0.216	251.848	0.098	252.266	0.720	0.216	
z21	23.401	0.415	0.524	3382.454	0.166	0.040	0.035	0.282	0.269	0.051	0.263	0.218	251.861	0.087	252.137	0.600	0.218	
z23	41.944	1.133	0.629	2165.926	0.199	0.040	0.047	0.282	0.419	0.051	0.411	0.225	251.852	0.116	252.206	0.936	0.225	
z25	22.163	0.528	0.526	2521.836	0.166	0.040	0.041	0.282	0.363	0.051	0.355	0.256	251.857	0.102	251.936	0.810	0.256	
MBE0203 (bed 25)																		
z5	11.974	0.520	0.626	1355.706	0.198	0.040	0.062	0.283	0.670	0.052	0.658	0.226	252.038	0.153	253.146	1.500	0.226	
z6	16.591	0.579	0.680	1659.969	0.215	0.040	0.057	0.282	0.546	0.051	0.537	0.215	251.976	0.140	252.106	1.220	0.215	
z7	35.158	0.894	0.594	2321.304	0.188	0.040	0.047	0.282	0.390	0.051	0.381	0.236	251.947	0.117	252.501	0.872	0.236	
z8	24.082	0.584	0.647	2398.111	0.205	0.040	0.055	0.282	0.384	0.051	0.374	0.244	251.917	0.137	252.477	0.859	0.244	
z11	24.813	0.413	0.634	3503.291	0.201	0.040	0.040	0.282	0.263	0.051	0.256	0.232	251.936	0.099	252.195	0.588	0.232	
z12	22.225	1.046	0.663	1240.030	0.210	0.040	0.066	0.283	0.727	0.051	0.716	0.220	252.009	0.163	252.744	1.627	0.220	
z14	12.232	0.424	0.608	1700.375	0.192	0.040	0.115	0.281	0.563	0.051	0.535	0.336	251.748	0.284	251.503	1.254	0.336	
z16	30.500	0.469	0.596	3822.666	0.189	0.040	0.047	0.281	0.256	0.051	0.246	0.295	251.907	0.116	251.733	0.571	0.295	

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				Isc	otopic ratio	SC					-	Dates (Mya)			
2 su/d.	206Pb/ 204Pb <sup>¶</sup>	208Pb/ 206Pb <sup>II</sup>	206Pb/ 238U <sup>II</sup>	±2s %	207Pb/ 235U <sup>II</sup>	±2s %	207Pb/ 206Pb <sup>II</sup>	±2s %	Correlation coefficient	206Pb/238U <th>**f</th> <th>±2s absolute<sup>††</sup></th> <th>207Pb/ 235U<sup>‡‡</sup></th> <th>±2s absolute<sup>††</sup></th> <th>Correlation coefficient</th>	**f	±2s absolute <sup>††</sup>	207Pb/ 235U <sup>‡‡</sup>	±2s absolute <sup>††</sup>	Correlation coefficient
.564 1	1766.638	0.178	0.040	0.067	0.282	0.517	0.051	0.508	0.208	251.776	0.165	251.913	1.154	0.208	
.718 2	2433.824	0.227	0.040	0.065	0.283	0.409	0.052	0.399	0.222	252.005	0.161	253.275	0.916	0.222	
.831 3	3763.472	0.263	0.040	0.064	0.282	0.277	0.051	0.267	0.265	252.045	0.160	252.109	0.619	0.265	
.502 6	3363.726	0.159	0.040	0.091	0.282	0.193	0.051	0.164	0.527	251.833	0.225	252.184	0.432	0.527	
.604 1	1870.738	0.191	0.040	0.064	0.282	0.490	0.051	0.479	0.234	252.105	0.158	252.142	1.095	0.234	
.619 1	276.525	0.196	0.040	0.086	0.282	0.754	0.051	0.736	0.257	251.904	0.212	252.468	1.685	0.257	
.651 3	3742.086	0.206	0.040	0.053	0.284	0.276	0.052	0.265	0.283	252.766	0.131	253.648	0.619	0.283	
.687 2	2041.178	0.217	0.040	0.079	0.282	0.473	0.051	0.464	0.190	252.717	0.195	252.501	1.056	0.190	
0.656 2	543.477	0.207	0.040	0.057	0.282	0.375	0.051	0.368	0.185	251.904	0.141	252.193	0.837	0.185	
.535 1	986.473	0.169	0.040	0.068	0.282	0.484	0.051	0.477	0.182	251.820	0.167	252.533	1.083	0.182	
1.649 1	203.960	0.205	0.040	0.095	0.283	0.821	0.051	0.803	0.246	252.534	0.234	252.923	1.839	0.246	
.507	991.047	0.160	0.040	0.084	0.287	0.920	0.052	0.903	0.236	254.321	0.208	256.400	2.084	0.236	
.423 2	2397.833	0.134	0.040	0.045	0.283	0.377	0.051	0.372	0.165	252.107	0.112	252.959	0.844	0.165	
.504	839.435	0.159	0.040	0.102	0.283	1.088	0.052	1.069	0.229	252.151	0.253	253.409	2.440	0.229	
.502 1	146.177	0.158	0.052	0.074	0.385	0.767	0.054	0.757	0.175	326.432	0.237	330.723	2.164	0.175	
.570	727.912	0.180	0.040	0.098	0.282	1.253	0.051	1.245	0.119	252.010	0.241	252.274	2.799	0.119	
0.416	759.359	0.131	0.040	0.125	0.282	1.214	0.051	1.192	0.231	251.927	0.310	252.314	2.713	0.231	
.751	648.381	0.237	0.040	0.158	0.281	1.462	0.051	1.420	0.313	252.044	0.391	251.080	3.252	0.313	
0.448 2	2042.101	0.137	0.148	0.198	1.455	0.386	0.071	0.325	0.538	889.717	1.648	912.127	2.322	0.538	
.458	857.181	0.145	0.040	060.0	0.283	1.063	0.052	1.045	0.236	252.063	0.222	253.086	2.381	0.236	
.549 1	103.944	0.174	0.040	0.081	0.278	0.860	0.051	0.838	0.307	252.013	0.200	249.129	1.899	0.307	
0.630 2	241.185	0.199	0.040	0.072	0.282	0.456	0.051	0.438	0.318	252.150	0.179	252.035	1.017	0.318	
0.191 1	1763.883	0.061	0.040	0.084	0.282	0.615	0.051	0.589	0.369	252.132	0.208	252.225	1.373	0.369	
0.497 2	2154.042	0.157	0.040	0.071	0.282	0.446	0.051	0.443	0.128	252.172	0.176	252.478	0.998	0.128	
0.543 3	3390.630	0.171	0.059	0.091	0.446	0.377	0.055	0.357	0.323	370.678	0.329	374.652	1.180	0.323	
.516	870.075	0.163	0.040	0.128	0.281	1.110	0.051	1.086	0.238	252.066	0.316	251.214	2.469	0.238	
0.677	759.931	0.214	0.040	0.123	0.284	1.207	0.052	1.191	0.180	252.287	0.305	253.836	2.711	0.180	
0.676 4	1037.644	0.214	0.040	0.099	0.281	0.263	0.051	0.237	0.432	251.435	0.245	251.822	0.586	0.432	
0.672	474.147	0.212	0.040	0.185	0.283	2.025	0.052	1.973	0.320	251.662	0.455	253.362	4.540	0.320	
0.672 1	404.695	0.212	0.040	0.168	0.281	0.693	0.051	0.661	0.304	251.421	0.415	251.567	1.544	0.304	
.689 3	3974.906	0.218	0.040	0.066	0.281	0.260	0.051	0.247	0.311	251.478	0.164	251.385	0.579	0.311	
.662 3	3207.811	0.209	0.040	0.054	0.281	0.309	0.051	0.296	0.322	251.497	0.133	251.582	0.688	0.322	
	02     70     70       70     84     84     85       93     93     93     71       16     44     1     1       77     7     1     6       889     31     2     1       17     6     2     1     2	02 1146.177   70 727.912   16 759.359   51 648.381   58 648.381   58 857.181   58 857.181   49 1103.944   30 2241.185   91 1763.883   97 2154.042   43 3390.630   16 870.075   77 759.931   76 4037.644   77 759.931   78 3374.906   62 3207.811	02 1146.177 0.158   70 727.912 0.131   51 648.381 0.237   48 2042.101 0.137   58 857.181 0.137   58 857.181 0.137   59 2241.185 0.199   91 1763.883 0.061   91 1763.883 0.061   92 2241.185 0.157   93 2241.185 0.163   91 1763.883 0.061   92 2154.042 0.171   93 3390.633 0.171   16 870.075 0.163   77 759.931 0.214   76 4037.644 0.212   77 759.931 0.212   78 3397.4.906 0.212   89 3397.4.906 0.212   82 3207.811 0.209	02     1146.177     0.158     0.052       70     727.912     0.180     0.040       51     648.381     0.237     0.040       53     648.381     0.237     0.040       548     857.181     0.137     0.148       58     857.181     0.137     0.148       58     857.181     0.145     0.040       49     1103.944     0.174     0.040       30     2241.185     0.199     0.040       91     1763.883     0.061     0.040       92     2241.185     0.171     0.040       93     2241.185     0.157     0.040       91     1763.883     0.061     0.040       93     3390.630     0.171     0.040       46     870.075     0.163     0.040       77     759.931     0.214     0.040       76     4037.644     0.212     0.040       77     759.931     0.212     0.040       72     1404.695	02     1146.177     0.158     0.052     0.074       70     727.912     0.180     0.040     0.158       648.381     0.237     0.040     0.158       648.381     0.237     0.040     0.158       648.381     0.137     0.148     0.198       648.381     0.137     0.148     0.198       648.381     0.137     0.148     0.198       648.383     0.145     0.040     0.051       91     1103.944     0.174     0.040     0.072       91     1763.883     0.061     0.040     0.072       91     1763.883     0.061     0.040     0.072       91     1763.883     0.061     0.040     0.071       91     1763.883     0.0171     0.040     0.072       91     2154.042     0.157     0.040     0.123       91     3390.630     0.171     0.040     0.123       77     759.931     0.214     0.040     0.123       76 <td>02     1146.177     0.158     0.052     0.074     0.385       70     727.912     0.180     0.040     0.038     0.282       648.381     0.237     0.040     0.125     0.282       648.381     0.237     0.040     0.198     0.281       648.381     0.237     0.040     0.198     0.281       648.381     0.137     0.148     0.198     1.455       68     857.181     0.145     0.040     0.283       49     1103.944     0.174     0.090     0.283       91     1763.883     0.061     0.040     0.071     0.282       91     1763.883     0.061     0.040     0.071     0.282       91     1763.883     0.061     0.071     0.282       930.630     0.171     0.059     0.091     0.446       17     759.931     0.214     0.040     0.123     0.284       77     759.931     0.214     0.040     0.123     0.284       76&lt;</td> <td>02     1146.177     0.158     0.052     0.074     0.385     0.767       70     727.912     0.180     0.040     0.098     0.282     1.214       61     759.359     0.131     0.040     0.125     0.282     1.214       61     759.359     0.131     0.040     0.125     0.282     1.214       648.381     0.237     0.040     0.198     1.455     0.386       68     857.181     0.145     0.040     0.090     0.283     1.063       69     1103.944     0.174     0.040     0.091     0.282     0.456       91     1763.883     0.061     0.040     0.072     0.282     0.466       91     1763.883     0.061     0.040     0.071     0.282     0.466       91     1763.883     0.061     0.040     0.071     0.282     0.466       91     3390.630     0.171     0.059     0.091     0.446     0.377       16     870.075     0.163</td> <td>02     1146.177     0.158     0.062     0.074     0.385     0.767     0.054       16     729.359     0.131     0.040     0.038     0.282     1.214     0.051       16     759.359     0.131     0.040     0.158     0.282     1.214     0.051       16     759.359     0.131     0.040     0.158     0.282     1.214     0.051       51     648.381     0.237     0.040     0.158     0.282     1.214     0.051       58     857.181     0.145     0.040     0.090     0.283     1.063     0.051       58     857.181     0.145     0.040     0.072     0.282     1.063     0.051       50     2241.185     0.145     0.040     0.071     0.282     0.446     0.051       51     1763.883     0.061     0.040     0.071     0.282     0.615     0.051       51     1763.883     0.061     0.040     0.0123     0.282     0.446     0.051       <t< td=""><td>02     1146.177     0.158     0.062     0.074     0.385     0.767     0.054     0.757       16     729.359     0.131     0.040     0.125     0.282     1.245     0.051     1.426       16     759.359     0.131     0.040     0.158     0.282     1.245     0.051     1.420       16     759.359     0.131     0.148     0.198     1.455     0.051     1.420       58     857.181     0.137     0.148     0.198     1.455     0.386     0.071     0.325       58     857.181     0.145     0.040     0.072     0.283     1.065     0.336       49     1103.944     0.174     0.040     0.071     0.282     0.446     0.531     0.438       3106.630     0.171     0.059     0.071     0.282     0.446     0.561     0.438       3390.630     0.171     0.059     0.071     0.282     0.446     0.561     0.443       77     759.931     0.214     0.282</td><td>1146.177     0.158     0.052     0.074     0.385     0.767     0.054     0.757     0.175       16     759.359     0.131     0.040     0.038     0.282     1.237     0.051     1.192     0.313       16     759.359     0.131     0.040     0.158     0.282     1.245     0.031     1.192     0.231       16     759.359     0.131     0.040     0.158     0.283     1.465     0.051     1.420     0.313       16     759.351     0.137     0.148     0.198     1.455     0.386     0.071     0.325     0.236       16     857.181     0.145     0.040     0.072     0.283     1.063     0.355     0.365     0.313       17     0.145     0.040     0.071     0.282     0.446     0.743     0.128       16     877.035     0.161     0.040     0.071     0.282     0.361     0.326       17     163.883     0.061     0.040     0.123     0.281     0.136</td><td>1146.117     0.158     0.052     0.074     0.385     0.767     0.054     0.757     0.175     336.432       16     759.359     0.131     0.040     0.098     0.282     1.214     0.051     1.245     0.119     252.010       16     759.359     0.131     0.040     0.158     0.281     1.462     0.051     1.425     0.313     252.044       8     57.181     0.145     0.040     0.158     0.283     1.063     0.051     1.420     0.313     252.043       8     857.181     0.145     0.040     0.051     0.283     1.063     0.307     252.013       8     857.181     0.144     0.040     0.081     0.278     0.860     0.736     0.367     252.063       9     1103.944     0.174     0.040     0.081     0.278     0.860     0.745     0.236     252.166       9     241.165     0.191     0.281     0.281     0.281     0.561     252.135       1763.383     <t< td=""><td>1146.177     0.158     0.052     0.074     0.355     0.767     0.054     0.757     0.175     326.432     0.237       1     757.912     0.180     0.040     0.088     0.282     1.231     0.019     252.010     0.241       16     759.359     0.131     0.040     0.158     0.282     1.245     0.313     252.043     0.313       16     759.359     0.131     0.148     0.198     1.455     0.386     0.071     0.335     0.331     252.043     0.391       17     648.381     0.144     0.198     1.455     0.386     0.071     0.325     0.234     0.331       103.944     0.114     0.149     0.282     0.446     0.377     0.438     0.330     0.22413     0.176       176.3883     0.061     0.040     0.281     1.165     0.361     0.436     0.236     0.234       176.3883     0.061     0.040     0.281     1.110     0.238     0.307     0.178     0.22132     0.176<td>D     1146.177     0.158     0.002     0.004     0.385     0.767     0.057     0.057     0.363     330.733       7     773-912     0.188     0.040     0.098     0.282     1.214     0.011     251.927     0.310     252.148       16     759.383     0.131     0.146     0.282     1.214     0.051     1.245     0.313     252.044     0.391     251.010       16     759.343     0.137     0.146     0.283     1.462     0.051     1.420     0.313     252.043     0.391     251.018     251.018     251.018     251.018     251.018     251.018     252.018     <td< td=""><td>1146.177     0.158     0.005     0.007     0.385     0.576     0.057     0.175     0.3373     2.164       7     759359     0.131     0.040     0.098     0.282     1.233     0.051     1.462     0.391     25.010     0.241     2.739     2.164       7     59359     0.131     0.040     0.128     0.282     1.214     0.051     1.442     0.331     25.1921     2.331     2.739       8     574.181     0.145     0.146     0.146     0.146     0.381     0.331     2.51.06     0.241     239       8     105344     0.147     0.040     0.081     0.283     0.061     0.383     0.381     2321     23106     2321     231       9     103344     0.174     0.040     0.081     0.282     0.051     0.383     0.391     251.08     2321.08     2321.08     1017       9     105344     0.146     0.051     0.446     0.051     0.443     0.128     252.013     0.117</td></td<></td></td></t<></td></t<></td>	02     1146.177     0.158     0.052     0.074     0.385       70     727.912     0.180     0.040     0.038     0.282       648.381     0.237     0.040     0.125     0.282       648.381     0.237     0.040     0.198     0.281       648.381     0.237     0.040     0.198     0.281       648.381     0.137     0.148     0.198     1.455       68     857.181     0.145     0.040     0.283       49     1103.944     0.174     0.090     0.283       91     1763.883     0.061     0.040     0.071     0.282       91     1763.883     0.061     0.040     0.071     0.282       91     1763.883     0.061     0.071     0.282       930.630     0.171     0.059     0.091     0.446       17     759.931     0.214     0.040     0.123     0.284       77     759.931     0.214     0.040     0.123     0.284       76<	02     1146.177     0.158     0.052     0.074     0.385     0.767       70     727.912     0.180     0.040     0.098     0.282     1.214       61     759.359     0.131     0.040     0.125     0.282     1.214       61     759.359     0.131     0.040     0.125     0.282     1.214       648.381     0.237     0.040     0.198     1.455     0.386       68     857.181     0.145     0.040     0.090     0.283     1.063       69     1103.944     0.174     0.040     0.091     0.282     0.456       91     1763.883     0.061     0.040     0.072     0.282     0.466       91     1763.883     0.061     0.040     0.071     0.282     0.466       91     1763.883     0.061     0.040     0.071     0.282     0.466       91     3390.630     0.171     0.059     0.091     0.446     0.377       16     870.075     0.163	02     1146.177     0.158     0.062     0.074     0.385     0.767     0.054       16     729.359     0.131     0.040     0.038     0.282     1.214     0.051       16     759.359     0.131     0.040     0.158     0.282     1.214     0.051       16     759.359     0.131     0.040     0.158     0.282     1.214     0.051       51     648.381     0.237     0.040     0.158     0.282     1.214     0.051       58     857.181     0.145     0.040     0.090     0.283     1.063     0.051       58     857.181     0.145     0.040     0.072     0.282     1.063     0.051       50     2241.185     0.145     0.040     0.071     0.282     0.446     0.051       51     1763.883     0.061     0.040     0.071     0.282     0.615     0.051       51     1763.883     0.061     0.040     0.0123     0.282     0.446     0.051 <t< td=""><td>02     1146.177     0.158     0.062     0.074     0.385     0.767     0.054     0.757       16     729.359     0.131     0.040     0.125     0.282     1.245     0.051     1.426       16     759.359     0.131     0.040     0.158     0.282     1.245     0.051     1.420       16     759.359     0.131     0.148     0.198     1.455     0.051     1.420       58     857.181     0.137     0.148     0.198     1.455     0.386     0.071     0.325       58     857.181     0.145     0.040     0.072     0.283     1.065     0.336       49     1103.944     0.174     0.040     0.071     0.282     0.446     0.531     0.438       3106.630     0.171     0.059     0.071     0.282     0.446     0.561     0.438       3390.630     0.171     0.059     0.071     0.282     0.446     0.561     0.443       77     759.931     0.214     0.282</td><td>1146.177     0.158     0.052     0.074     0.385     0.767     0.054     0.757     0.175       16     759.359     0.131     0.040     0.038     0.282     1.237     0.051     1.192     0.313       16     759.359     0.131     0.040     0.158     0.282     1.245     0.031     1.192     0.231       16     759.359     0.131     0.040     0.158     0.283     1.465     0.051     1.420     0.313       16     759.351     0.137     0.148     0.198     1.455     0.386     0.071     0.325     0.236       16     857.181     0.145     0.040     0.072     0.283     1.063     0.355     0.365     0.313       17     0.145     0.040     0.071     0.282     0.446     0.743     0.128       16     877.035     0.161     0.040     0.071     0.282     0.361     0.326       17     163.883     0.061     0.040     0.123     0.281     0.136</td><td>1146.117     0.158     0.052     0.074     0.385     0.767     0.054     0.757     0.175     336.432       16     759.359     0.131     0.040     0.098     0.282     1.214     0.051     1.245     0.119     252.010       16     759.359     0.131     0.040     0.158     0.281     1.462     0.051     1.425     0.313     252.044       8     57.181     0.145     0.040     0.158     0.283     1.063     0.051     1.420     0.313     252.043       8     857.181     0.145     0.040     0.051     0.283     1.063     0.307     252.013       8     857.181     0.144     0.040     0.081     0.278     0.860     0.736     0.367     252.063       9     1103.944     0.174     0.040     0.081     0.278     0.860     0.745     0.236     252.166       9     241.165     0.191     0.281     0.281     0.281     0.561     252.135       1763.383     <t< td=""><td>1146.177     0.158     0.052     0.074     0.355     0.767     0.054     0.757     0.175     326.432     0.237       1     757.912     0.180     0.040     0.088     0.282     1.231     0.019     252.010     0.241       16     759.359     0.131     0.040     0.158     0.282     1.245     0.313     252.043     0.313       16     759.359     0.131     0.148     0.198     1.455     0.386     0.071     0.335     0.331     252.043     0.391       17     648.381     0.144     0.198     1.455     0.386     0.071     0.325     0.234     0.331       103.944     0.114     0.149     0.282     0.446     0.377     0.438     0.330     0.22413     0.176       176.3883     0.061     0.040     0.281     1.165     0.361     0.436     0.236     0.234       176.3883     0.061     0.040     0.281     1.110     0.238     0.307     0.178     0.22132     0.176<td>D     1146.177     0.158     0.002     0.004     0.385     0.767     0.057     0.057     0.363     330.733       7     773-912     0.188     0.040     0.098     0.282     1.214     0.011     251.927     0.310     252.148       16     759.383     0.131     0.146     0.282     1.214     0.051     1.245     0.313     252.044     0.391     251.010       16     759.343     0.137     0.146     0.283     1.462     0.051     1.420     0.313     252.043     0.391     251.018     251.018     251.018     251.018     251.018     251.018     252.018     <td< td=""><td>1146.177     0.158     0.005     0.007     0.385     0.576     0.057     0.175     0.3373     2.164       7     759359     0.131     0.040     0.098     0.282     1.233     0.051     1.462     0.391     25.010     0.241     2.739     2.164       7     59359     0.131     0.040     0.128     0.282     1.214     0.051     1.442     0.331     25.1921     2.331     2.739       8     574.181     0.145     0.146     0.146     0.146     0.381     0.331     2.51.06     0.241     239       8     105344     0.147     0.040     0.081     0.283     0.061     0.383     0.381     2321     23106     2321     231       9     103344     0.174     0.040     0.081     0.282     0.051     0.383     0.391     251.08     2321.08     2321.08     1017       9     105344     0.146     0.051     0.446     0.051     0.443     0.128     252.013     0.117</td></td<></td></td></t<></td></t<>	02     1146.177     0.158     0.062     0.074     0.385     0.767     0.054     0.757       16     729.359     0.131     0.040     0.125     0.282     1.245     0.051     1.426       16     759.359     0.131     0.040     0.158     0.282     1.245     0.051     1.420       16     759.359     0.131     0.148     0.198     1.455     0.051     1.420       58     857.181     0.137     0.148     0.198     1.455     0.386     0.071     0.325       58     857.181     0.145     0.040     0.072     0.283     1.065     0.336       49     1103.944     0.174     0.040     0.071     0.282     0.446     0.531     0.438       3106.630     0.171     0.059     0.071     0.282     0.446     0.561     0.438       3390.630     0.171     0.059     0.071     0.282     0.446     0.561     0.443       77     759.931     0.214     0.282	1146.177     0.158     0.052     0.074     0.385     0.767     0.054     0.757     0.175       16     759.359     0.131     0.040     0.038     0.282     1.237     0.051     1.192     0.313       16     759.359     0.131     0.040     0.158     0.282     1.245     0.031     1.192     0.231       16     759.359     0.131     0.040     0.158     0.283     1.465     0.051     1.420     0.313       16     759.351     0.137     0.148     0.198     1.455     0.386     0.071     0.325     0.236       16     857.181     0.145     0.040     0.072     0.283     1.063     0.355     0.365     0.313       17     0.145     0.040     0.071     0.282     0.446     0.743     0.128       16     877.035     0.161     0.040     0.071     0.282     0.361     0.326       17     163.883     0.061     0.040     0.123     0.281     0.136	1146.117     0.158     0.052     0.074     0.385     0.767     0.054     0.757     0.175     336.432       16     759.359     0.131     0.040     0.098     0.282     1.214     0.051     1.245     0.119     252.010       16     759.359     0.131     0.040     0.158     0.281     1.462     0.051     1.425     0.313     252.044       8     57.181     0.145     0.040     0.158     0.283     1.063     0.051     1.420     0.313     252.043       8     857.181     0.145     0.040     0.051     0.283     1.063     0.307     252.013       8     857.181     0.144     0.040     0.081     0.278     0.860     0.736     0.367     252.063       9     1103.944     0.174     0.040     0.081     0.278     0.860     0.745     0.236     252.166       9     241.165     0.191     0.281     0.281     0.281     0.561     252.135       1763.383 <t< td=""><td>1146.177     0.158     0.052     0.074     0.355     0.767     0.054     0.757     0.175     326.432     0.237       1     757.912     0.180     0.040     0.088     0.282     1.231     0.019     252.010     0.241       16     759.359     0.131     0.040     0.158     0.282     1.245     0.313     252.043     0.313       16     759.359     0.131     0.148     0.198     1.455     0.386     0.071     0.335     0.331     252.043     0.391       17     648.381     0.144     0.198     1.455     0.386     0.071     0.325     0.234     0.331       103.944     0.114     0.149     0.282     0.446     0.377     0.438     0.330     0.22413     0.176       176.3883     0.061     0.040     0.281     1.165     0.361     0.436     0.236     0.234       176.3883     0.061     0.040     0.281     1.110     0.238     0.307     0.178     0.22132     0.176<td>D     1146.177     0.158     0.002     0.004     0.385     0.767     0.057     0.057     0.363     330.733       7     773-912     0.188     0.040     0.098     0.282     1.214     0.011     251.927     0.310     252.148       16     759.383     0.131     0.146     0.282     1.214     0.051     1.245     0.313     252.044     0.391     251.010       16     759.343     0.137     0.146     0.283     1.462     0.051     1.420     0.313     252.043     0.391     251.018     251.018     251.018     251.018     251.018     251.018     252.018     <td< td=""><td>1146.177     0.158     0.005     0.007     0.385     0.576     0.057     0.175     0.3373     2.164       7     759359     0.131     0.040     0.098     0.282     1.233     0.051     1.462     0.391     25.010     0.241     2.739     2.164       7     59359     0.131     0.040     0.128     0.282     1.214     0.051     1.442     0.331     25.1921     2.331     2.739       8     574.181     0.145     0.146     0.146     0.146     0.381     0.331     2.51.06     0.241     239       8     105344     0.147     0.040     0.081     0.283     0.061     0.383     0.381     2321     23106     2321     231       9     103344     0.174     0.040     0.081     0.282     0.051     0.383     0.391     251.08     2321.08     2321.08     1017       9     105344     0.146     0.051     0.446     0.051     0.443     0.128     252.013     0.117</td></td<></td></td></t<>	1146.177     0.158     0.052     0.074     0.355     0.767     0.054     0.757     0.175     326.432     0.237       1     757.912     0.180     0.040     0.088     0.282     1.231     0.019     252.010     0.241       16     759.359     0.131     0.040     0.158     0.282     1.245     0.313     252.043     0.313       16     759.359     0.131     0.148     0.198     1.455     0.386     0.071     0.335     0.331     252.043     0.391       17     648.381     0.144     0.198     1.455     0.386     0.071     0.325     0.234     0.331       103.944     0.114     0.149     0.282     0.446     0.377     0.438     0.330     0.22413     0.176       176.3883     0.061     0.040     0.281     1.165     0.361     0.436     0.236     0.234       176.3883     0.061     0.040     0.281     1.110     0.238     0.307     0.178     0.22132     0.176 <td>D     1146.177     0.158     0.002     0.004     0.385     0.767     0.057     0.057     0.363     330.733       7     773-912     0.188     0.040     0.098     0.282     1.214     0.011     251.927     0.310     252.148       16     759.383     0.131     0.146     0.282     1.214     0.051     1.245     0.313     252.044     0.391     251.010       16     759.343     0.137     0.146     0.283     1.462     0.051     1.420     0.313     252.043     0.391     251.018     251.018     251.018     251.018     251.018     251.018     252.018     <td< td=""><td>1146.177     0.158     0.005     0.007     0.385     0.576     0.057     0.175     0.3373     2.164       7     759359     0.131     0.040     0.098     0.282     1.233     0.051     1.462     0.391     25.010     0.241     2.739     2.164       7     59359     0.131     0.040     0.128     0.282     1.214     0.051     1.442     0.331     25.1921     2.331     2.739       8     574.181     0.145     0.146     0.146     0.146     0.381     0.331     2.51.06     0.241     239       8     105344     0.147     0.040     0.081     0.283     0.061     0.383     0.381     2321     23106     2321     231       9     103344     0.174     0.040     0.081     0.282     0.051     0.383     0.391     251.08     2321.08     2321.08     1017       9     105344     0.146     0.051     0.446     0.051     0.443     0.128     252.013     0.117</td></td<></td>	D     1146.177     0.158     0.002     0.004     0.385     0.767     0.057     0.057     0.363     330.733       7     773-912     0.188     0.040     0.098     0.282     1.214     0.011     251.927     0.310     252.148       16     759.383     0.131     0.146     0.282     1.214     0.051     1.245     0.313     252.044     0.391     251.010       16     759.343     0.137     0.146     0.283     1.462     0.051     1.420     0.313     252.043     0.391     251.018     251.018     251.018     251.018     251.018     251.018     252.018 <td< td=""><td>1146.177     0.158     0.005     0.007     0.385     0.576     0.057     0.175     0.3373     2.164       7     759359     0.131     0.040     0.098     0.282     1.233     0.051     1.462     0.391     25.010     0.241     2.739     2.164       7     59359     0.131     0.040     0.128     0.282     1.214     0.051     1.442     0.331     25.1921     2.331     2.739       8     574.181     0.145     0.146     0.146     0.146     0.381     0.331     2.51.06     0.241     239       8     105344     0.147     0.040     0.081     0.283     0.061     0.383     0.381     2321     23106     2321     231       9     103344     0.174     0.040     0.081     0.282     0.051     0.383     0.391     251.08     2321.08     2321.08     1017       9     105344     0.146     0.051     0.446     0.051     0.443     0.128     252.013     0.117</td></td<>	1146.177     0.158     0.005     0.007     0.385     0.576     0.057     0.175     0.3373     2.164       7     759359     0.131     0.040     0.098     0.282     1.233     0.051     1.462     0.391     25.010     0.241     2.739     2.164       7     59359     0.131     0.040     0.128     0.282     1.214     0.051     1.442     0.331     25.1921     2.331     2.739       8     574.181     0.145     0.146     0.146     0.146     0.381     0.331     2.51.06     0.241     239       8     105344     0.147     0.040     0.081     0.283     0.061     0.383     0.381     2321     23106     2321     231       9     103344     0.174     0.040     0.081     0.282     0.051     0.383     0.391     251.08     2321.08     2321.08     1017       9     105344     0.146     0.051     0.446     0.051     0.443     0.128     252.013     0.117	

DNAS

DNAS DNAS

Table S2. (	Cont.													
	Compo	sition					<u>.</u>	sotopic ra <sup>.</sup>	tios					
Sample and	Pb*	Pbc		206Pb/	208Pb/	206Pb/		207Pb/		207Pb/		Correlation	206Pb/238	
fraction	(bd)⁺	t(bd)	Th/U§	204Pb <sup>¶</sup>	206Pb <sup>II</sup>	238U <sup>II</sup>	±2s %	235U <sup>II</sup>	±2s %	206Pb <sup>II</sup>	±2s %	coefficient	<th>**f</th>	**f
z15	17.101	1.216	0.666	826.874	0.211	0.040	0.113	0.282	1.150	0.051	1.114	0.364	251.620	
z16	7.036	0.607	0.735	672.915	0.232	0.040	0.115	0.281	1.386	0.051	1.363	0.240	251.577	
z17	10.339	0.356	0.680	1679.481	0.215	0.040	0.064	0.282	0.574	0.051	0.565	0.195	251.796	

Correlation coefficient

Dates (Mya)

207Pb/ 235U<sup>##</sup> 252.266

±2s

Pb/238U

absolute<sup>††</sup> ±2s

> absolute<sup>††</sup> 0.279

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DNAC

0.364 0.240

3.090 2.569

251.759

0.284

0.195 0.238 0.252 0.225 0.216 0.243

1.282 1.143 1.214 1.288 2.973 2.609 1.215

251.968

0.159

252.339

0.135 0.175

251.738

0.238 0.252

0.501

0.051 0.051 0.051 0.051 0.051 0.051

0.512

0.282

0.055

0.040

0.218 0.204 0.218 0.240

1822.853

0.688

0.421

13.277 9.031

z18 z21 251.742

0.193

0.225 0.216 0.243

> 1.313 1.148

251.540 252.072 252.107

0.300

0.255

251.435 251.482

0.154

0.203

0.535

0.544

0.282

0.282

0.104

0.194

785.193

705.476

5.638 10.546

z24 z25

8.823

z22

1598.787

0.281

0.078 0.121

0.040 0.040 0.040

252.671

252.199 251.502 251.471

0.529 0.565

0.543 0.578 1.334 1.169

0.283 0.281

0.071

0.040

1738.759

0.646 0.691 0.758 0.613

0.303 0.319 0.461 0.801 0.203

Analyses highlighted in gray are not included in the weighted mean calculation 0.062 0.040 0.209 1704.160 0.661 0.439 12.856 z26

Total mass of radiogenic Pb.

<sup>+</sup>Total mass of common Pb.

 $^{3}$ Th contents calculated from radiogenic  $^{208}$ Pb and the  $^{207}$ Pb/ $^{206}$ Pb date of the sample, assuming concordance between U-Th and Pb systems.

Ratio of radiogenic Pb (including <sup>208</sup>Pb) to common Pb.

Measured ratio corrected for fractionation and spike contribution only.

\*Measured ratios corrected for fractionation, tracer, and blank.

<sup>+1</sup>/sotopic dates calculated using the decay constants  $\lambda^{238} = 1.55125E-10$  and  $\lambda^{235} = 9.8485E-10$  (1). <sup>++</sup>Corrected for initial Th/U disequilibrium using radiogenic 208Pb and Th/U[magma] = 3.00000.

1. Jaffey A, Flynn K, Glendenin L, Bentley W, Essling A (1971) Precision measurement of half-lives and specific activities of <sup>235</sup>U and <sup>238</sup>U. Phys Rev C Nucl Phys 4:1889–1906.